

LECTURE 6

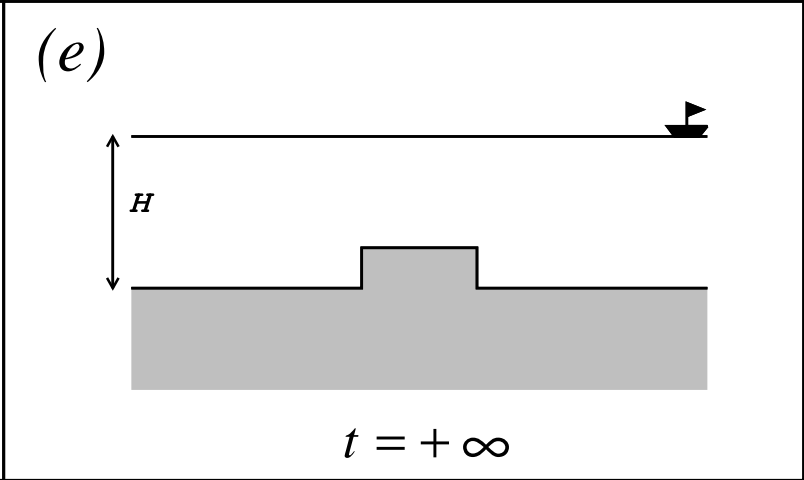
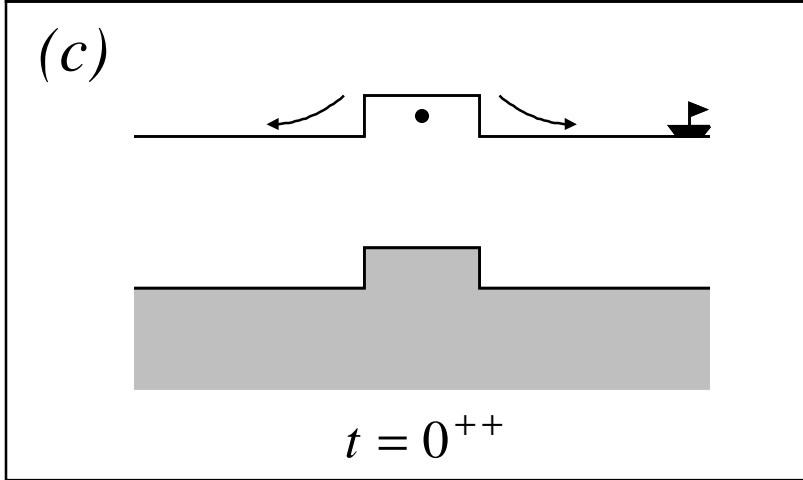
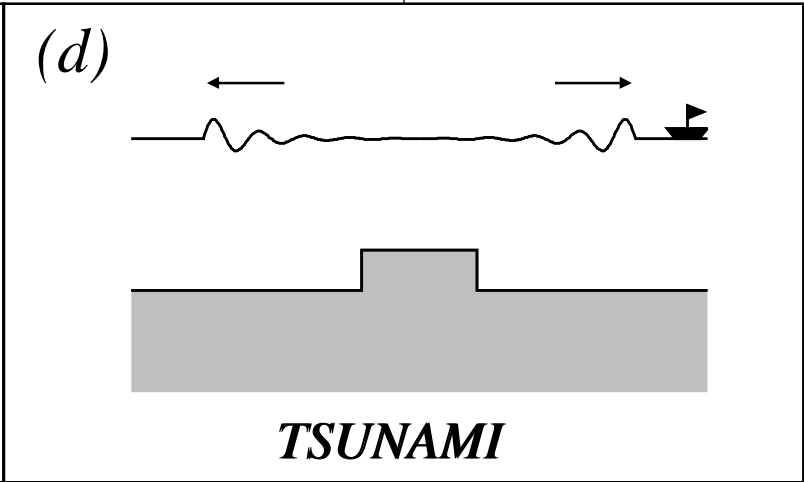
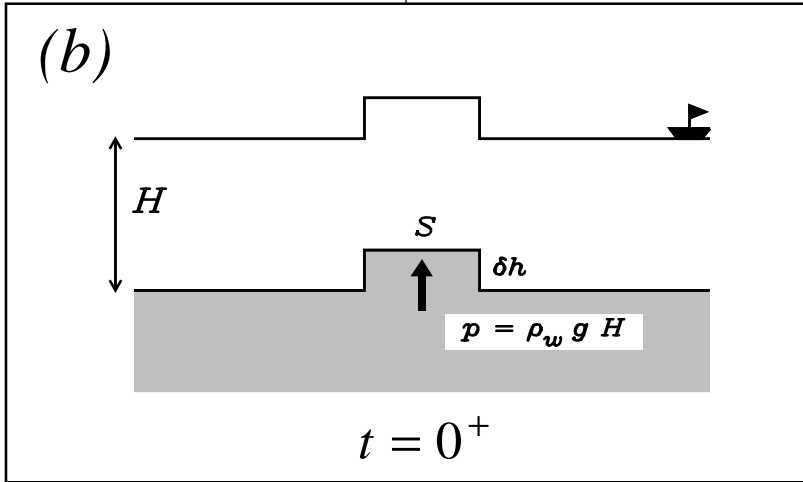
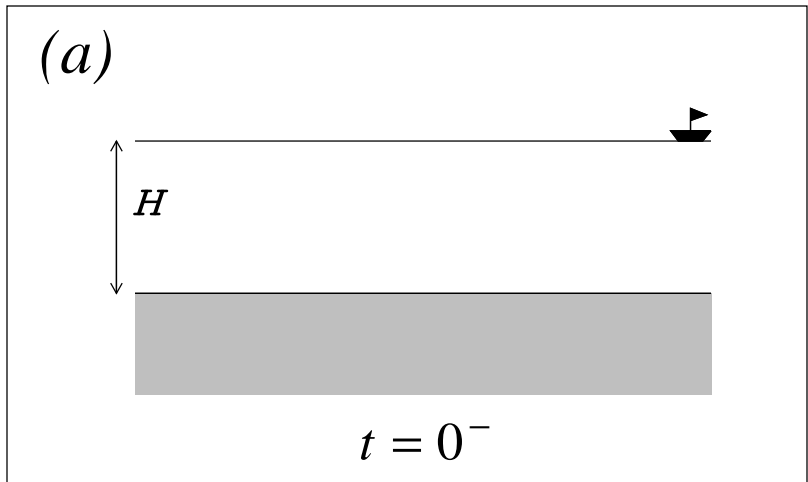
MODELING EARTHQUAKES AS TSUNAMI SOURCES

PRINCIPLES of HYDRODYNAMIC SIMULATIONS

CLASSICAL APPROACH

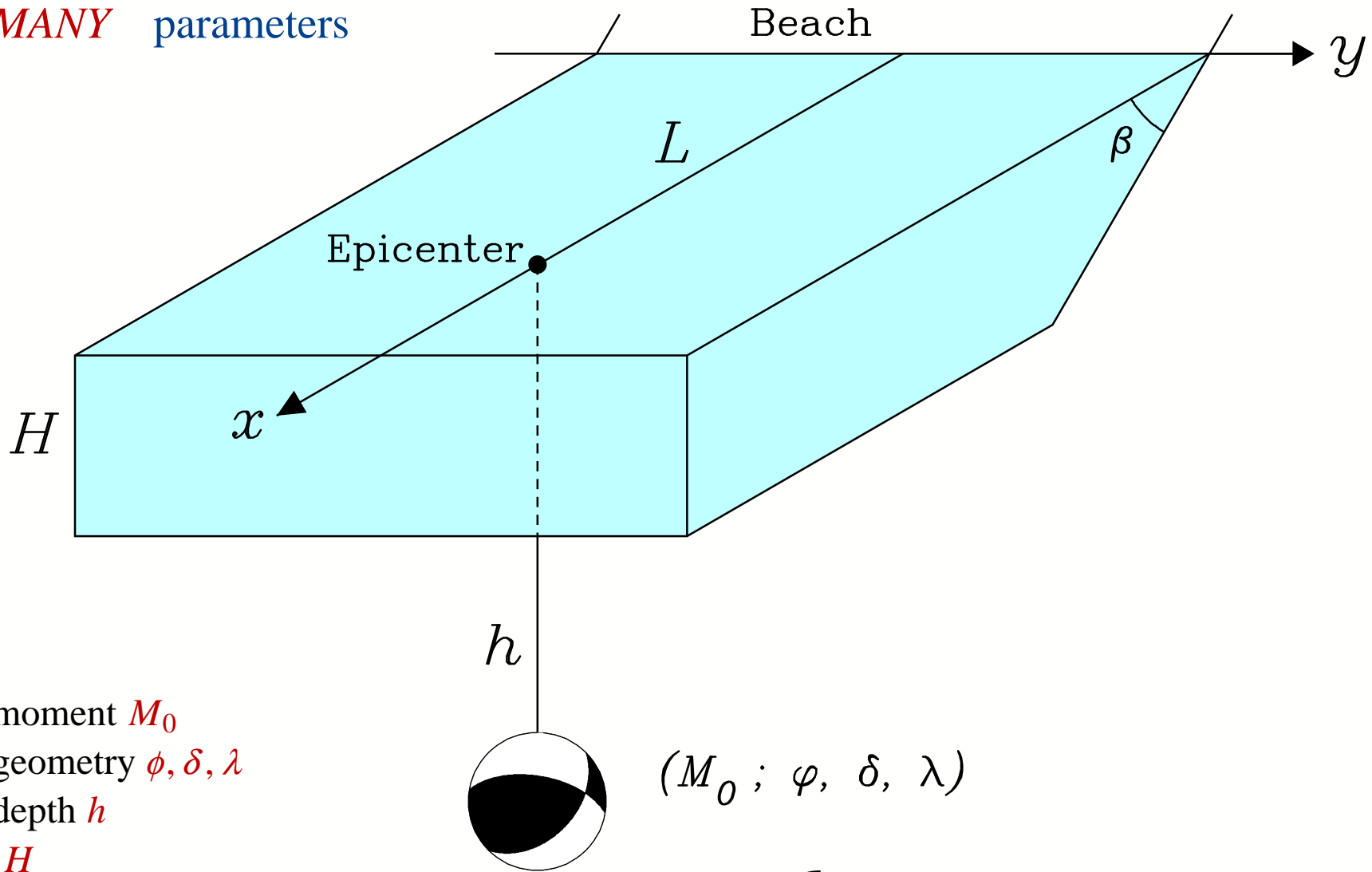
1. Obtain model of Earthquake Rupture
2. Compute Static Deformation of Ocean Bottom
3. Use as Initial Conditions of
Vertical Surface Displacement with Zero Initial Velocity
4. Run Hydrodynamic Model (*e.g.*, **MOST**)
5. Propagate, up to and including
INUNDATION of Receiving Shore

CLASSICAL
APPROACH



GENERIC EARTHQUAKE DISLOCATION

Involves *MANY* parameters



Earthquake moment M_0

Earthquake geometry ϕ, δ, λ

Earthquake depth h

Water depth H

Epicentral distance to shore L

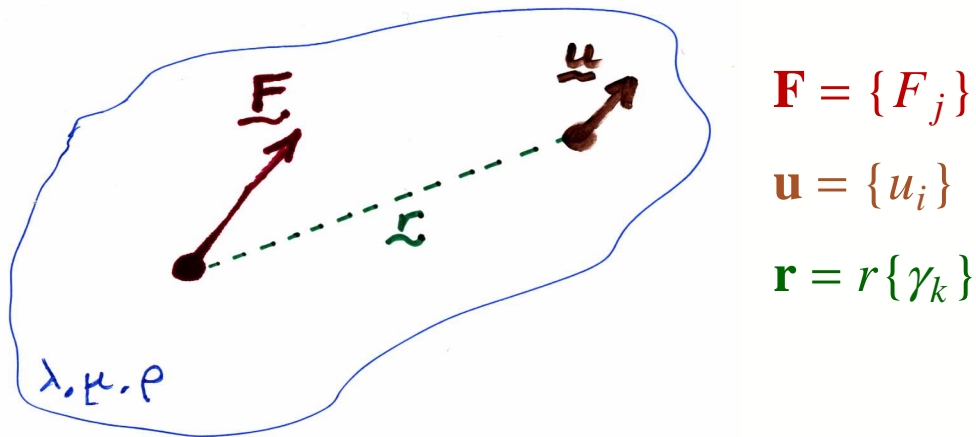
Beach slope β

$(M_0 ; \varphi, \delta, \lambda)$

$M_0 : \left\{ \begin{array}{l} \text{Fault Length } L_F \\ \text{Fault width } W \\ \text{Slip on Fault } \Delta u \end{array} \right.$

FIRST STEP

- Position a point force \mathbf{F} in an infinite homogeneous elastic medium



- Obtain the *Dynamic* displacement field of the deformation

Then for a point force $X_0(t)$ in the x_j -direction at the origin, we have

$$\begin{aligned}
 u_i(\mathbf{x}, t) &= X_0 * G_{ij} \quad (\text{in the notation of Chapter 3}) \\
 &= \frac{1}{4\pi\rho} (3\gamma_i\gamma_j - \delta_{ij}) \frac{1}{r^3} \int_{r/\alpha}^{r/\beta} \tau X_0(t - \tau) d\tau \\
 &\quad + \frac{1}{4\pi\rho\alpha^2} \gamma_i\gamma_j \frac{1}{r} X_0\left(t - \frac{r}{\alpha}\right) \\
 &\quad - \frac{1}{4\pi\rho\beta^2} (\gamma_i\gamma_j - \delta_{ij}) \frac{1}{r} X_0\left(t - \frac{r}{\beta}\right). \tag{4.23}
 \end{aligned}$$

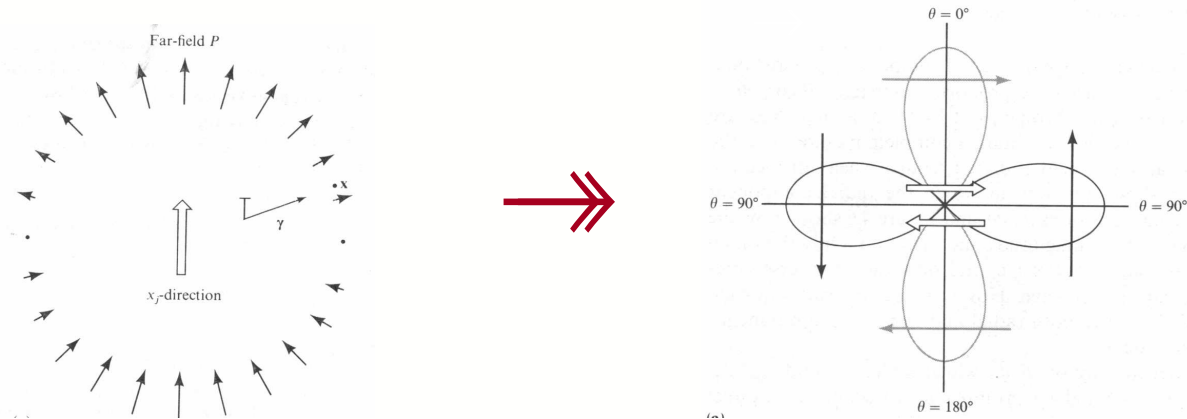
[Aki and Richards, 1980; p. 73, Eqn. (4.23)]

- The *STATIC* displacement is simply obtained by putting $t \rightarrow \infty$.

[This expression is known as the Somigliana Tensor]

SECOND STEP

- Replace Single Force by Double-Couple



→ Simply use Somigliana's tensor as a Green's function and take appropriate derivatives.

NEAR FIELD

NEAR FIELD

NEAR FIELD

[Far Field]

→ Note that these are the *P* and *S* waves of the near [and far] field[s].

$$\begin{aligned}
 M_{pq} * G_{np,q} = & \left(\frac{15\gamma_n\gamma_p\gamma_q - 3\gamma_n\delta_{pq} - 3\gamma_p\delta_{nq} - 3\gamma_q\delta_{np}}{4\pi\rho} \right) \frac{1}{r^4} \int_{r/\alpha}^{r/\beta} \tau M_{pq}(t - \tau) d\tau \\
 & + \left(\frac{6\gamma_n\gamma_p\gamma_q - \gamma_n\delta_{pq} - \gamma_p\delta_{nq} - \gamma_q\delta_{np}}{4\pi\rho\alpha^2} \right) \frac{1}{r^2} M_{pq} \left(t - \frac{r}{\alpha} \right) \\
 & - \left(\frac{6\gamma_n\gamma_p\gamma_q - \gamma_n\delta_{pq} - \gamma_p\delta_{nq} - 2\gamma_q\delta_{np}}{4\pi\rho\beta^2} \right) \frac{1}{r^2} M_{pq} \left(t - \frac{r}{\beta} \right) \\
 & + \frac{\gamma_n\gamma_p\gamma_q}{4\pi\rho\alpha^3} \frac{1}{r} \dot{M}_{pq} \left(t - \frac{r}{\alpha} \right) \\
 & - \left(\frac{\gamma_n\gamma_p - \delta_{np}}{4\pi\rho\beta^3} \right) \gamma_q \frac{1}{r} \dot{M}_{pq} \left(t - \frac{r}{\beta} \right). \tag{4.29}
 \end{aligned}$$

[Aki and Richards, 1980; p. 79; Eqn. (4.29)]

THIRD STEP

- Include effect of free surface

(Combine with "reflection" of equivalent P and S waves)

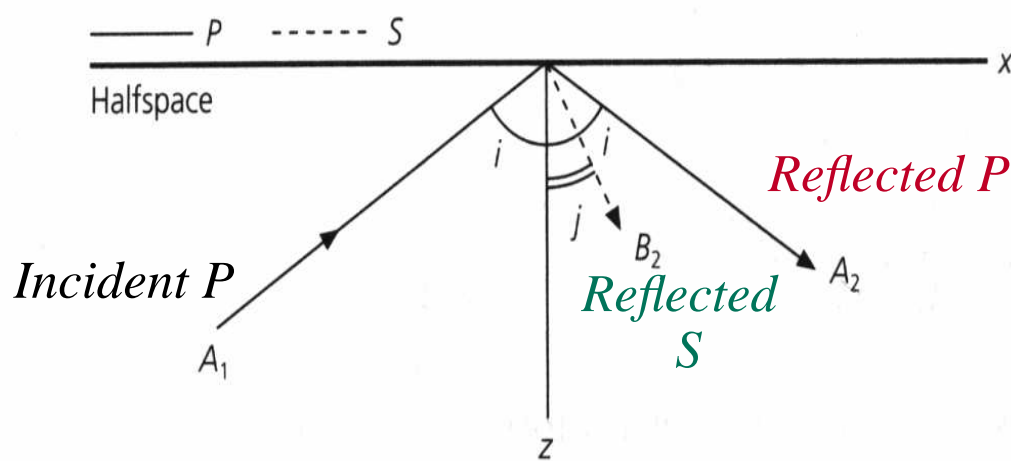


Fig. 2.6-6 Geometry for a P wave in a halfspace incident upon a free surface. A_1 , A_2 , and B_2 are the amplitudes of the incident P, reflected P, and reflected SV waves.

[Stein and Wyession, 2002]

- Integrate over finite area of faulting

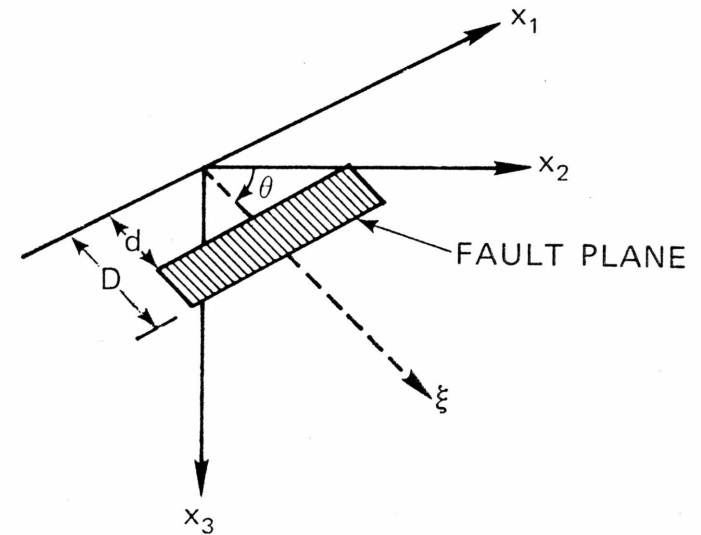


FIG. 1. Fault geometry and coordinate system.

The problem has an analytical solution

TWO equivalent algorithms

Mansinha and Smylie [1971]

Okada [1985]

Only difference: Okada allows for
tensile crack
(non-double-couple solution).

STATIC DEFORMATION OF OCEAN BOTTOM

Straightforward, if somewhat arcane analytical formulæ

[Mansinha and Smylie, 1971; Okada, 1985]

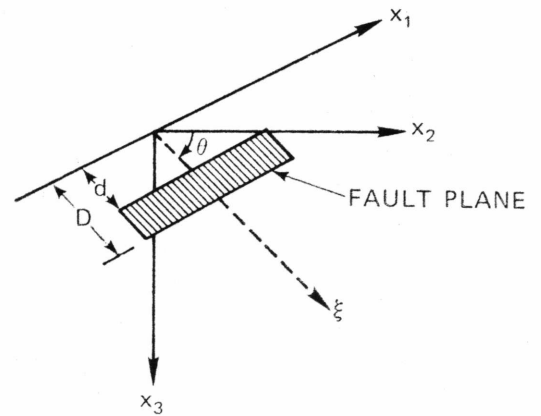
(1) Displacements

For strike-slip

$$\begin{cases} u_x = -\frac{U_1}{2\pi} \left[\frac{\xi q}{R(R + \eta)} + \tan^{-1} \frac{\xi \eta}{qR} + I_1 \sin \delta \right] \\ u_y = -\frac{U_1}{2\pi} \left[\frac{\hat{y} q}{R(R + \eta)} + \frac{q \cos \delta}{R + \eta} + I_2 \sin \delta \right] \\ u_z = -\frac{U_1}{2\pi} \left[\frac{\hat{d} q}{R(R + \eta)} + \frac{q \sin \delta}{R + \eta} + I_4 \sin \delta \right] \end{cases} .$$

For dip-slip

$$\begin{cases} u_x = -\frac{U_2}{2\pi} \left[\frac{q}{R} - I_3 \sin \delta \cos \delta \right] \\ u_y = -\frac{U_2}{2\pi} \left[\frac{\hat{y} q}{R(R + \xi)} + \cos \delta \tan^{-1} \frac{\xi \eta}{qR} - I_1 \sin \delta \cos \delta \right] \\ u_z = -\frac{U_2}{2\pi} \left[\frac{\hat{d} q}{R(R + \xi)} + \sin \delta \tan^{-1} \frac{\xi \eta}{qR} - I_5 \sin \delta \cos \delta \right] \end{cases} .$$



where

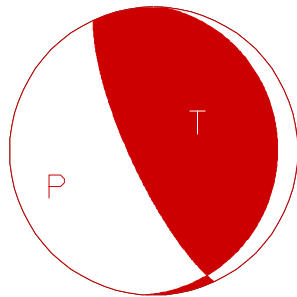
$$\begin{cases} I_1 = \frac{\mu}{\lambda + \mu} \left[\frac{-1}{\cos \delta} \frac{\xi}{R + \hat{d}} \right] - \frac{\sin \delta}{\cos \delta} I_5 \\ I_2 = \frac{\mu}{\lambda + \mu} [-\ln(R + \eta)] - I_3 \\ I_3 = \frac{\mu}{\lambda + \mu} \left[\frac{1}{\cos \delta} \frac{\hat{y}}{R + \hat{d}} - \ln(R + \eta) \right] + \frac{\sin \delta}{\cos \delta} I_4 \\ I_4 = \frac{\mu}{\lambda + \mu} \frac{1}{\cos \delta} [\ln(R + \hat{d}) - \sin \delta \ln(R + \eta)] \\ I_5 = \frac{\mu}{\lambda + \mu} \frac{2}{\cos \delta} \tan^{-1} \frac{\eta(X + q \cos \delta) + X(R + X) \sin \delta}{\xi(R + X) \cos \delta} \end{cases}$$

STATIC DEFORMATION OF OCEAN BOTTOM

EXAMPLE: VALPARAISO, CHILE

17 AUGUST 1906

$$M_0 = 2.8 \times 10^{28} \text{ dyn-cm}$$

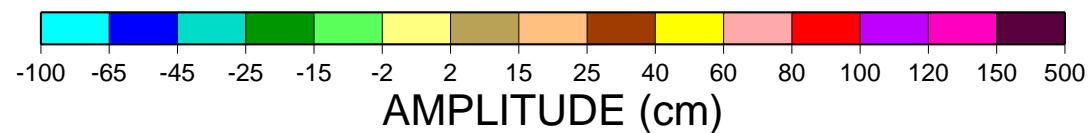
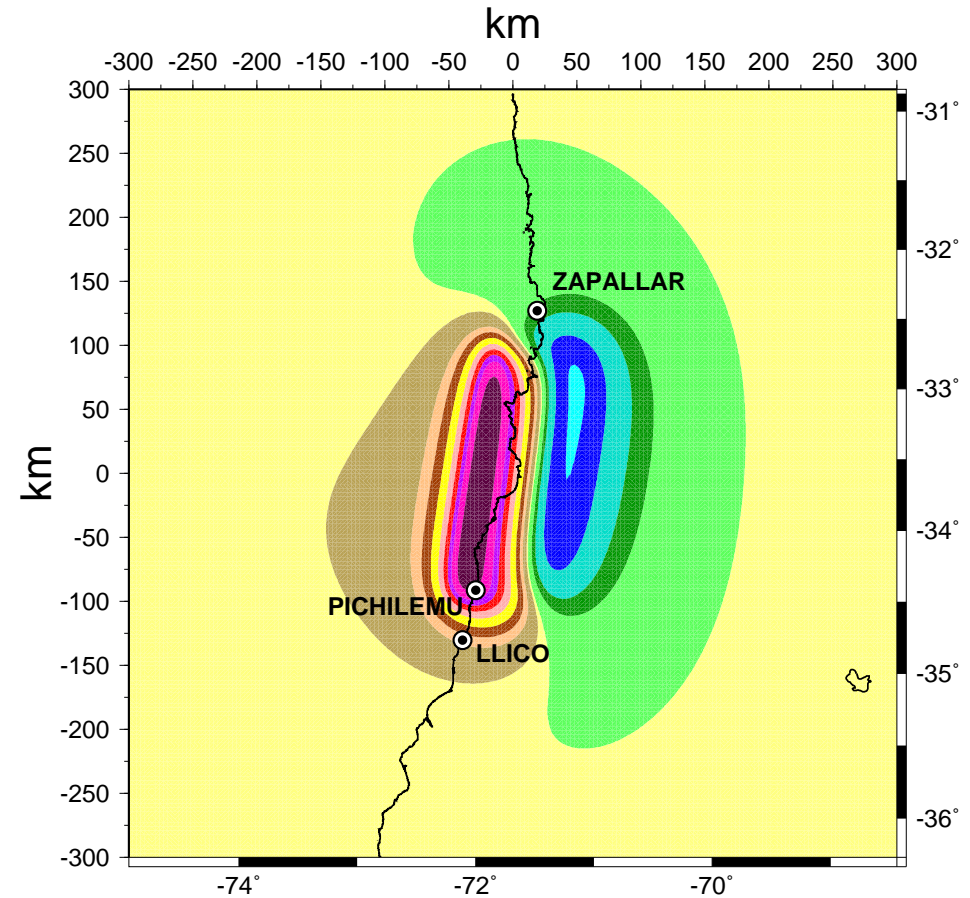


$$\phi_f = 3^\circ; \delta = 15^\circ; \lambda = 117^\circ$$

$$L_F = 200 \text{ km}; W = 75 \text{ km};$$

$$\Delta u = 5.3 \text{ m}$$

1906 CHILEAN EVENT



[Okal, 2005]

- Use this static deformation field (limited to its oceanic portion) as the initial condition ($t = 0_+$) of the hydrodynamic calculation.

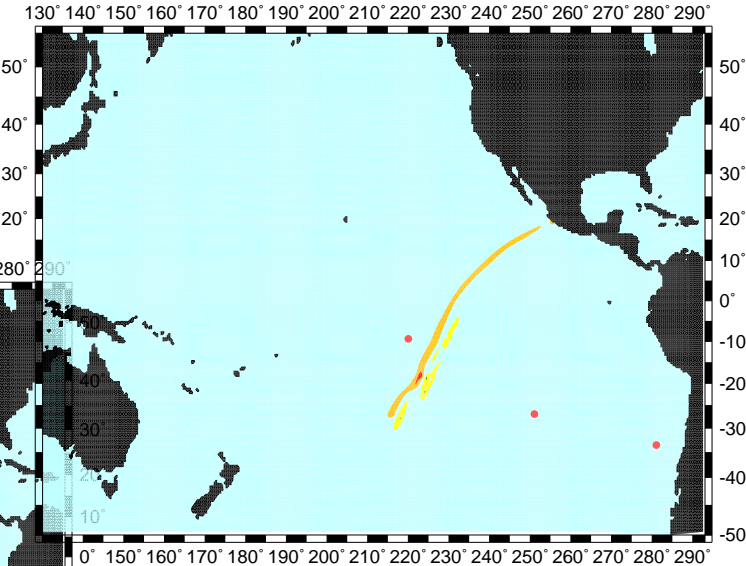
→ *Justification:* The seismic source is generally *MUCH FASTER* than any tsunami process, hence it can be taken as instantaneous.

(even in the case of SLOW, so-called "Tsunami" earthquakes)

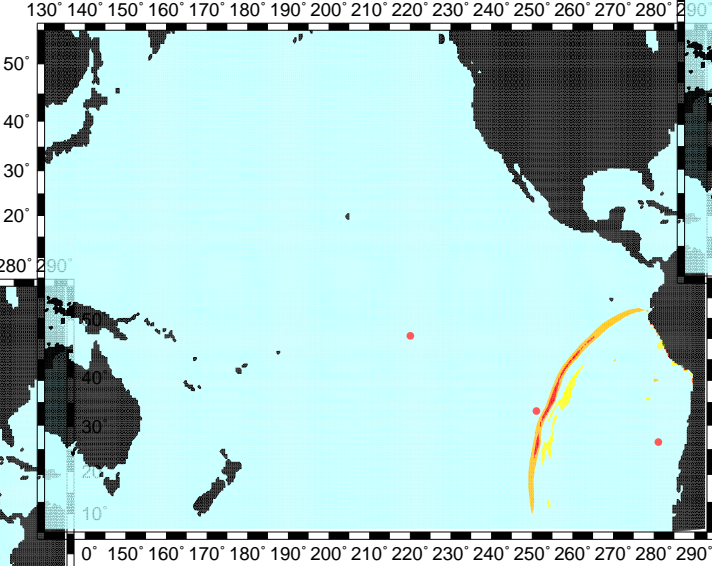
PRODUCTS OF SIMULATION

1. Snapshots of Sea Height at Given Times

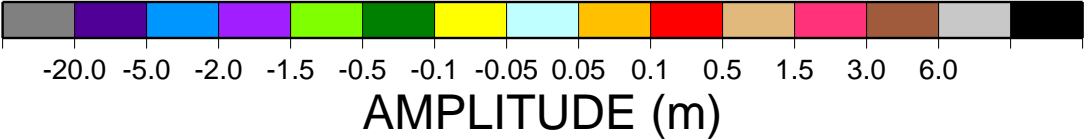
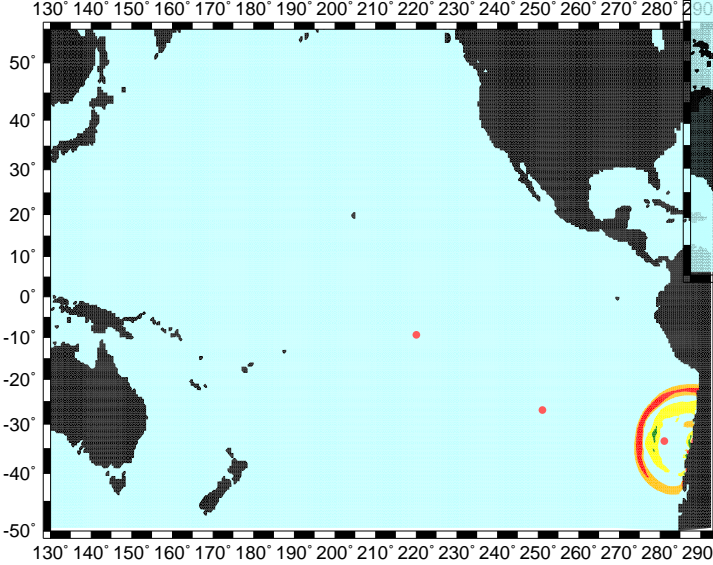
CHILE 1906 +10 hr.



CHILE 1906 + 5 hr.

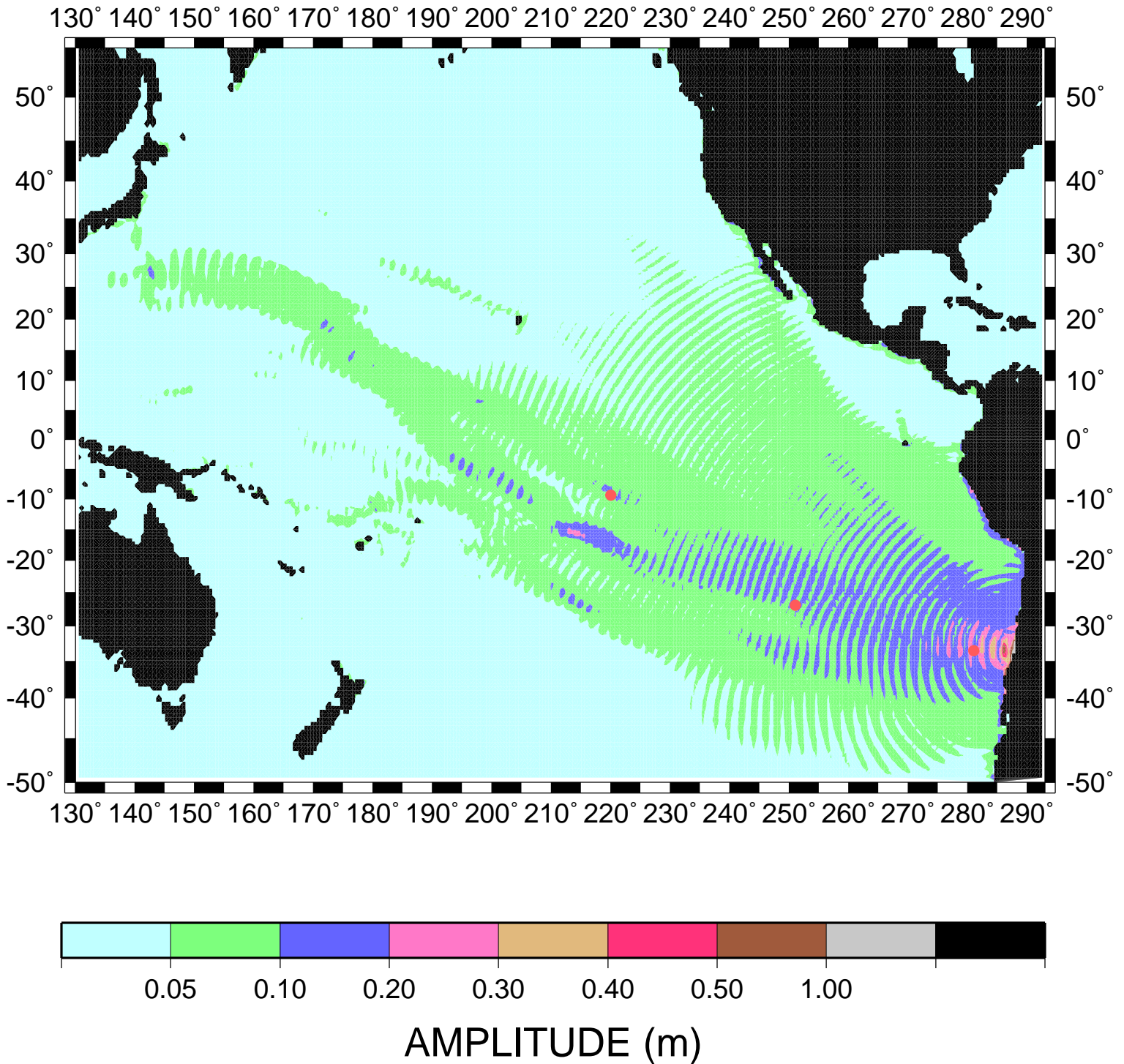


CHILE 1906 + 1 hr. 45 mn



PRODUCTS OF SIMULATION

2. Map of Maximum Amplitude of Tsunami Wave



HOW ROBUST IS THIS PROCEDURE ?

It is worth exploring the robustness of our results in the far field, with respect to detailed parameters of our sources, *a fortiori* unknown in the context of many simulations.

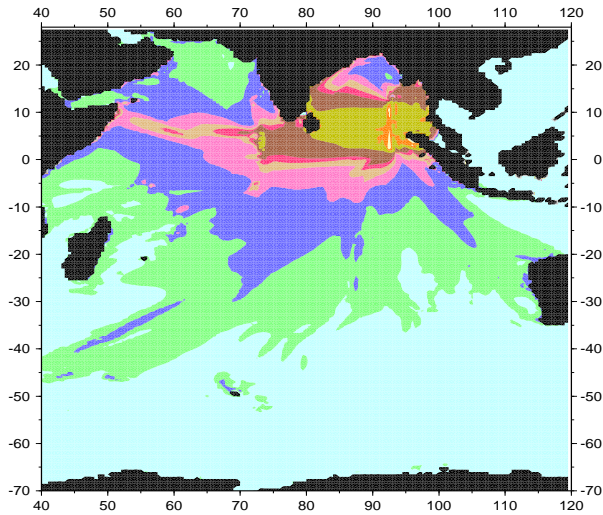
We study simulated amplitudes of the 2004 Sumatra-Andaman tsunami in the far field under fluctuations of source parameters, while keeping the seismic moment of the source constant.

We conclude that our results are indeed robust.

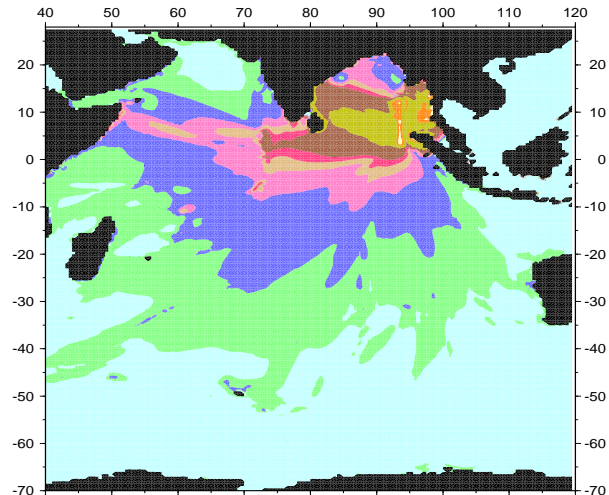
The primary parameters controlling the far field tsunami amplitudes are the size (moment) of the parent earthquake and the depth of the water column in the epicentral area.

*1. MOVE SOURCE
LATERALLY*

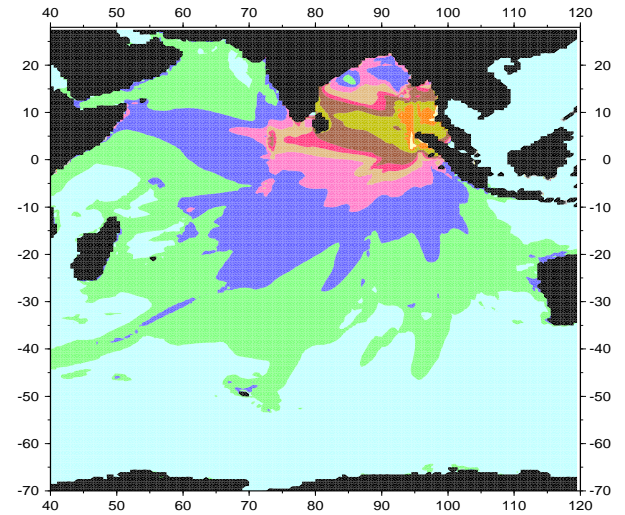
Move 1° West



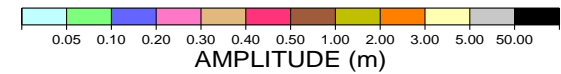
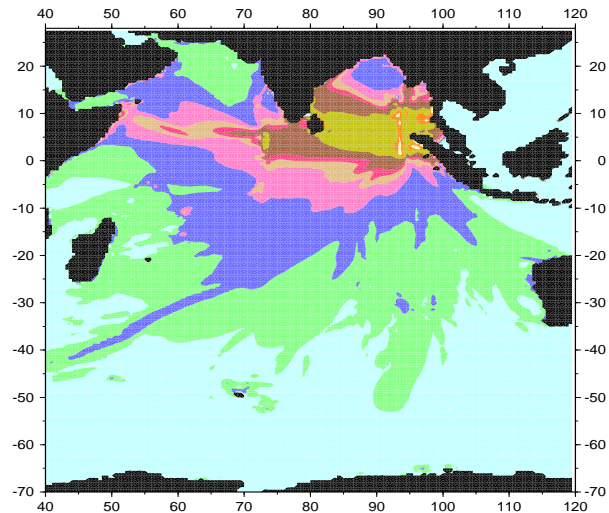
Move 1° North



Move 1° East



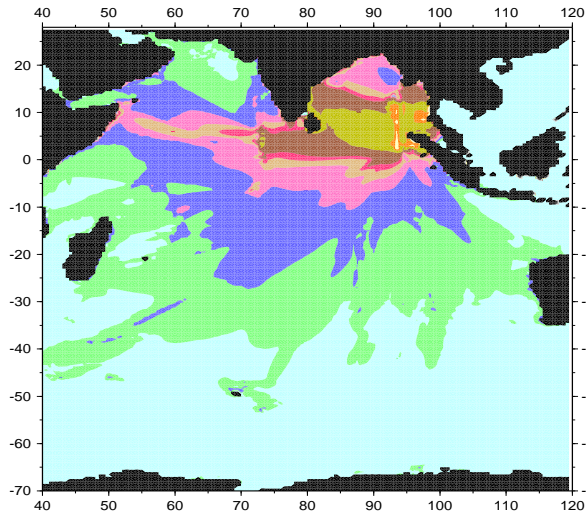
Move 1° South



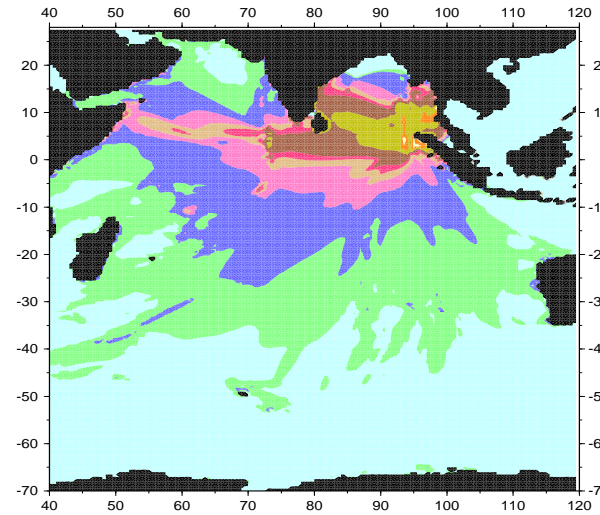
NO MAJOR EFFECT !!

2. CHANGE SOURCE PARAMETERS

SUMATRA 2004 Original

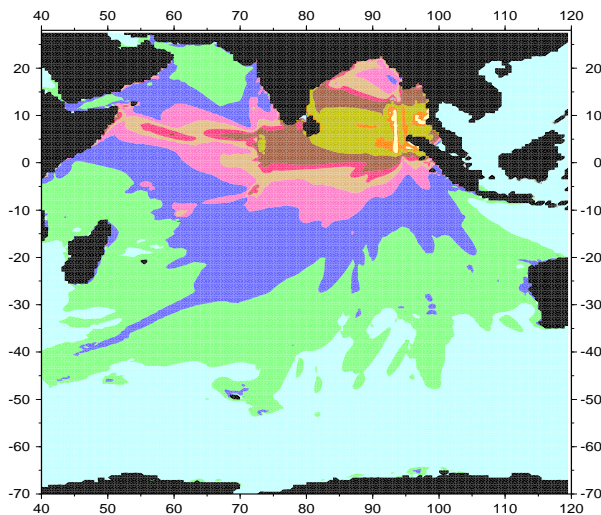


Heterogeneous Slip



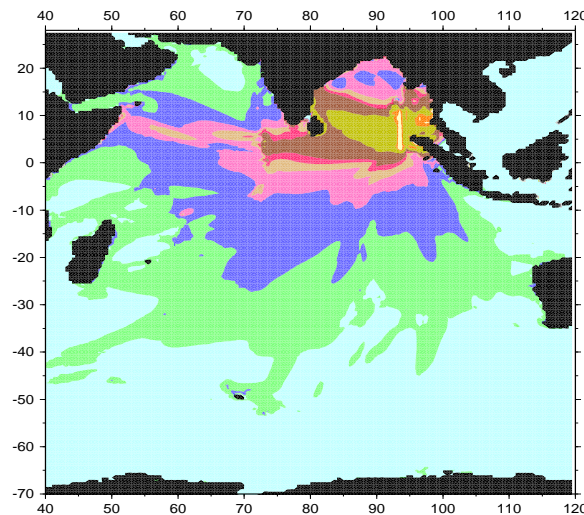
Depth

SUMATRA 2004; D = 20 km



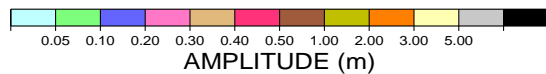
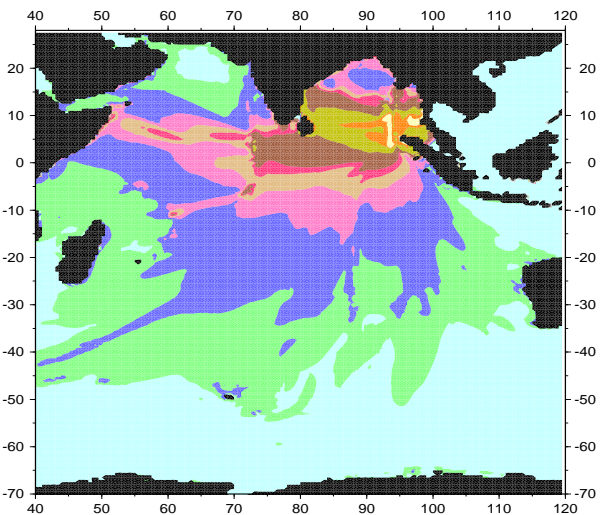
Fault Dip

SUMATRA 2004 Dip = 12 deg.



Strain Released

SUMATRA 2004 Large Strain



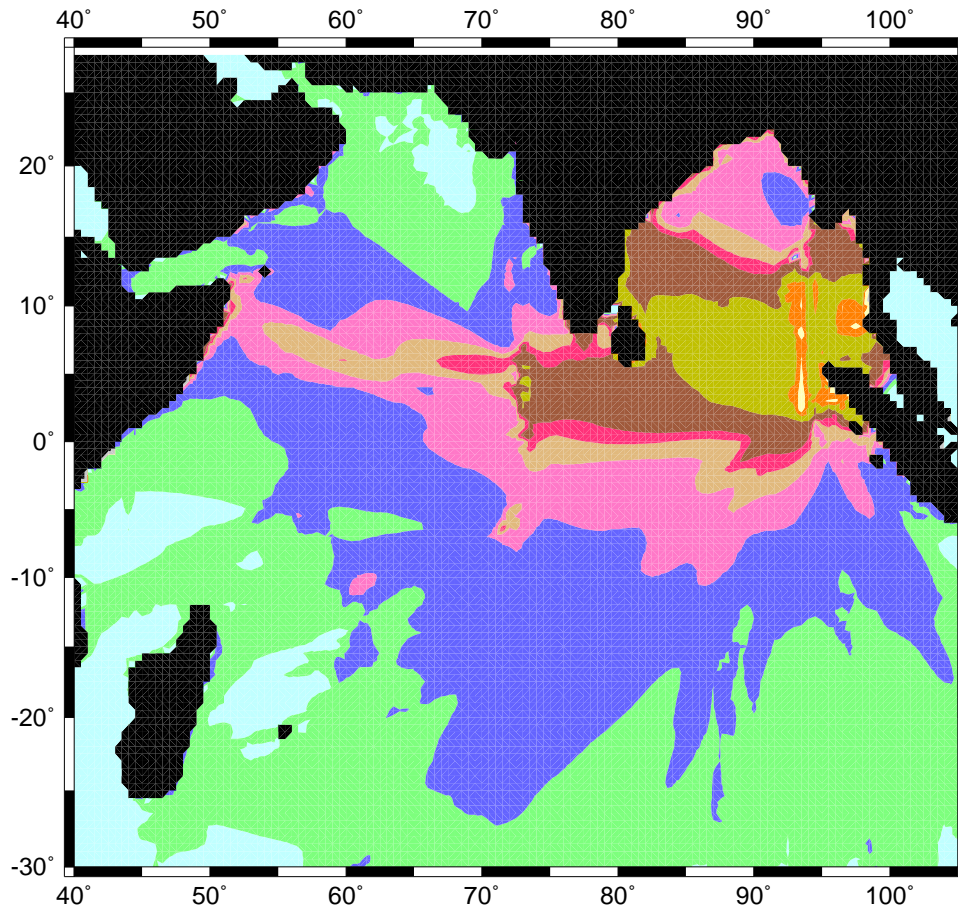
NOTE: $M_0 \cdot \sin \delta$
kept constant

NO MAJOR EFFECT !!

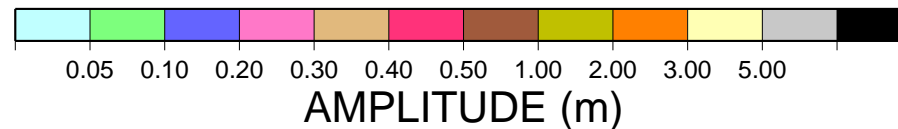
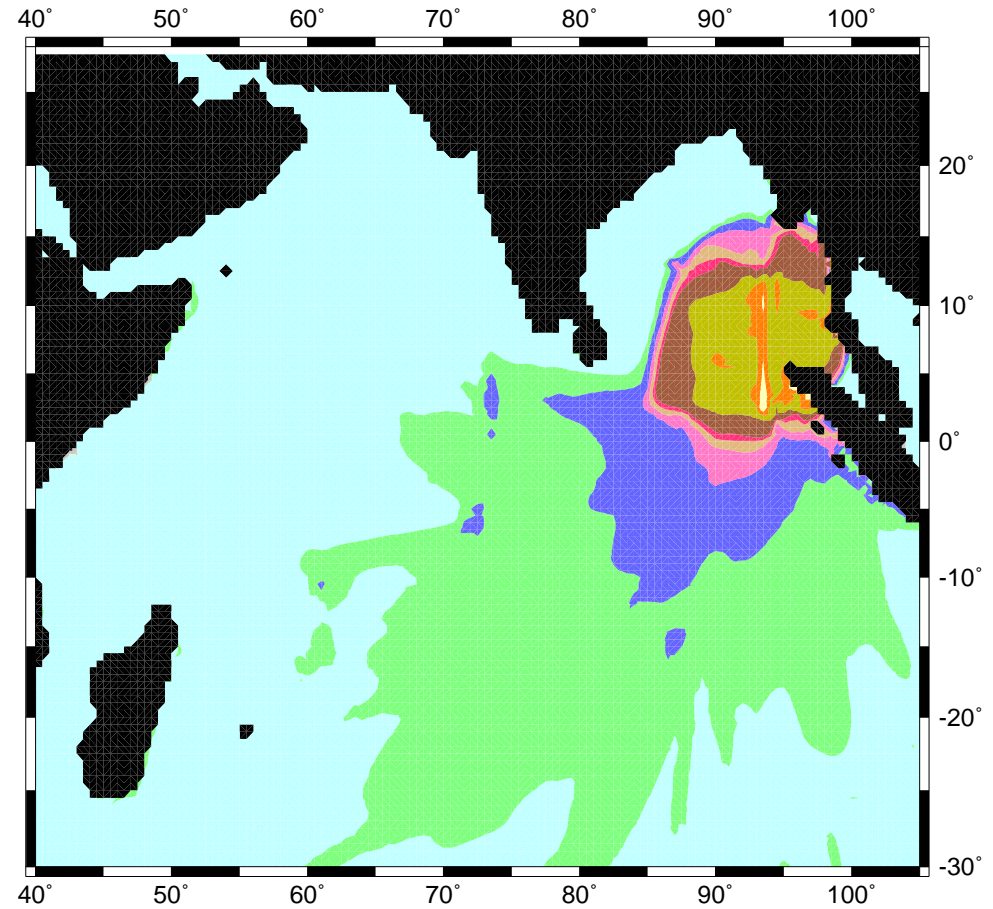
By CONTRAST, WATER DEPTH at the SOURCE PLAYS a CRUCIAL ROLE

NOTE: This explains the much smaller tsunami during the 2005 Nias earthquake.

***UNPERTURBED
EPICENTRAL BATHYMETRY***



***EPICENTRAL BATHYMETRY
DIVIDED BY 4.0***

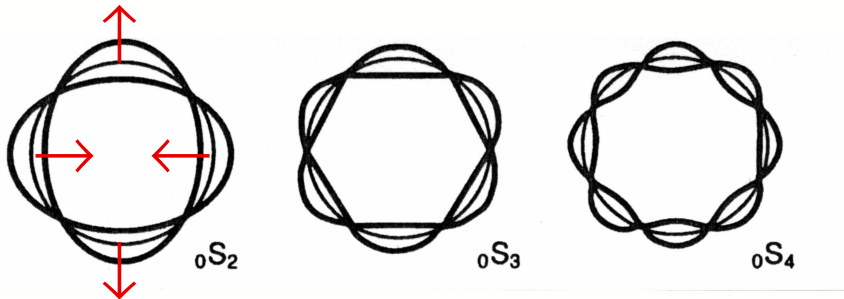


NORMAL MODE FORMALISM: A different approach

[Ward, 1980]

- At very long periods (typically 15 to 54 minutes), the Earth, because of its finite size, can ring like a bell.
- Such *FREE OSCILLATIONS* are equivalent to the superposition of two progressive waves travelling in opposite directions along the surface of the Earth.

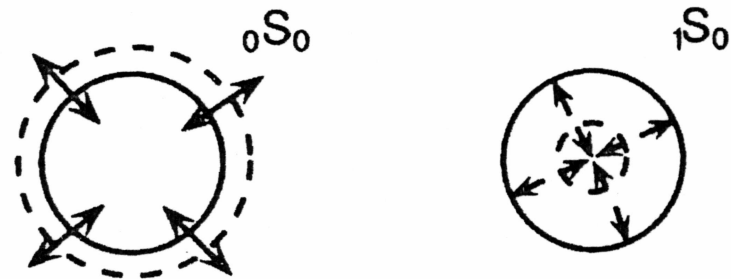
T = 54 minutes



**"FOOTBALL
Mode"**

[After *Lay and
Wallace, 1995*]

T = 21.5 minutes



**"BREATHING
Mode"**

Ward [1980] has shown that **Tsunamis come naturally as a special branch of the normal modes of the Earth**, provided it is bounded by an ocean, and gravity is included in the formulation of its vibrations.

In the normal mode formalism, the solution of the vertical displacement (both in the water and solid Earth) is sought as

$$u_z(\mathbf{x}; t) = u_z(r, \theta, \phi; t) = y_1(r) \cdot Y_l^m(\theta, \phi) \exp(i \omega t) = y_1(r) \cdot P_l^m(\theta, \phi) \cdot e^{i m \phi} \cdot \exp(i \omega t)$$

where Y_l^m is a *spherical harmonic* of order l and degree m ; P_l^m is the Legendre polynomial of order l and degree m ; and $\{r, \theta, \phi\}$ is a system of spherical polar coordinates.

This allows for the *separation* of the variables $\{r, \theta, \phi\}$.

The problem is complemented by similar expressions for the overpressure $p = -y_2$ in the tsunami wave, the horizontal displacement $u_x = l \cdot y_3$, and the change in the gravity potential y_5 .

Under the linear approximation, the equations of hydrodynamics transform into a system of linear differential equations of the first order.

For any given l , *i.e.*, wavenumber $k = (l + 1/2)$ (a radius of the Earth), the system has non trivial solutions for only one value of ω . **The relationship between l and ω is the *Dispersion Relation of the Tsunami*.**

SPHEROIDAL MODE HAS 6-COMPONENT EIGENFUNCTION SATISFYING:

$$\begin{array}{c}
 \frac{dy_1}{dr} \\
 \frac{dy_2}{dr} \\
 \frac{dy_3}{dr} \\
 \frac{dy_4}{dr} \\
 \frac{dy_5}{dr} \\
 \frac{dy_6}{dr}
 \end{array}
 =
 \begin{array}{ccccccc}
 \frac{-2\lambda}{(\lambda+2\mu)r} & \frac{1}{(\lambda+2\mu)} & \frac{L^2 \lambda}{(\lambda+2\mu)r} & 0 & 0 & 0 & \\
 -\omega^2 \rho + \frac{4\mu(3\lambda+2\mu)}{(\lambda+2\mu)r^2} - \frac{4\rho g}{r} & \frac{-4\mu}{(\lambda+2\mu)r} & L^2 \left[\frac{\rho g}{r} - \frac{2\mu(3\lambda+2\mu)}{(\lambda+2\mu)r^2} \right] & \frac{L^2}{r} & 0 & -\rho & \\
 \frac{-1}{r} & 0 & \frac{1}{r} & \frac{1}{\mu} & 0 & 0 & \\
 \frac{\rho g}{r} - \frac{2\mu(3\lambda+2\mu)}{(\lambda+2\mu)r^2} & \frac{-\lambda}{(\lambda+2\mu)r} & -\omega^2 \rho + \frac{4\mu L^2 (\lambda+\mu)}{(\lambda+2\mu)r^2} - \frac{2\mu}{r^2} & \frac{-3}{r} & \frac{-\rho}{r} & 0 & \\
 4\pi G \rho & 0 & 0 & 0 & 0 & 1 & \\
 0 & 0 & \frac{-4\pi L^2 G \rho}{r} & 0 & \frac{L^2}{r^2} & \frac{-2}{r} &
 \end{array}
 \cdot
 \begin{array}{c}
 y_1 \\
 y_2 \\
 y_3 \\
 y_4 \\
 y_5 \\
 y_6
 \end{array}$$

y_1 : Vertical displacement

y_4 : Tangential stress

y_3 : Horizontal displacement

y_5 : Gravity potential

y_2 : Normal stress

y_6 : Auxiliary gravity

EASILY SOLVED WITH APPROPRIATE BOUNDARY CONDITIONS

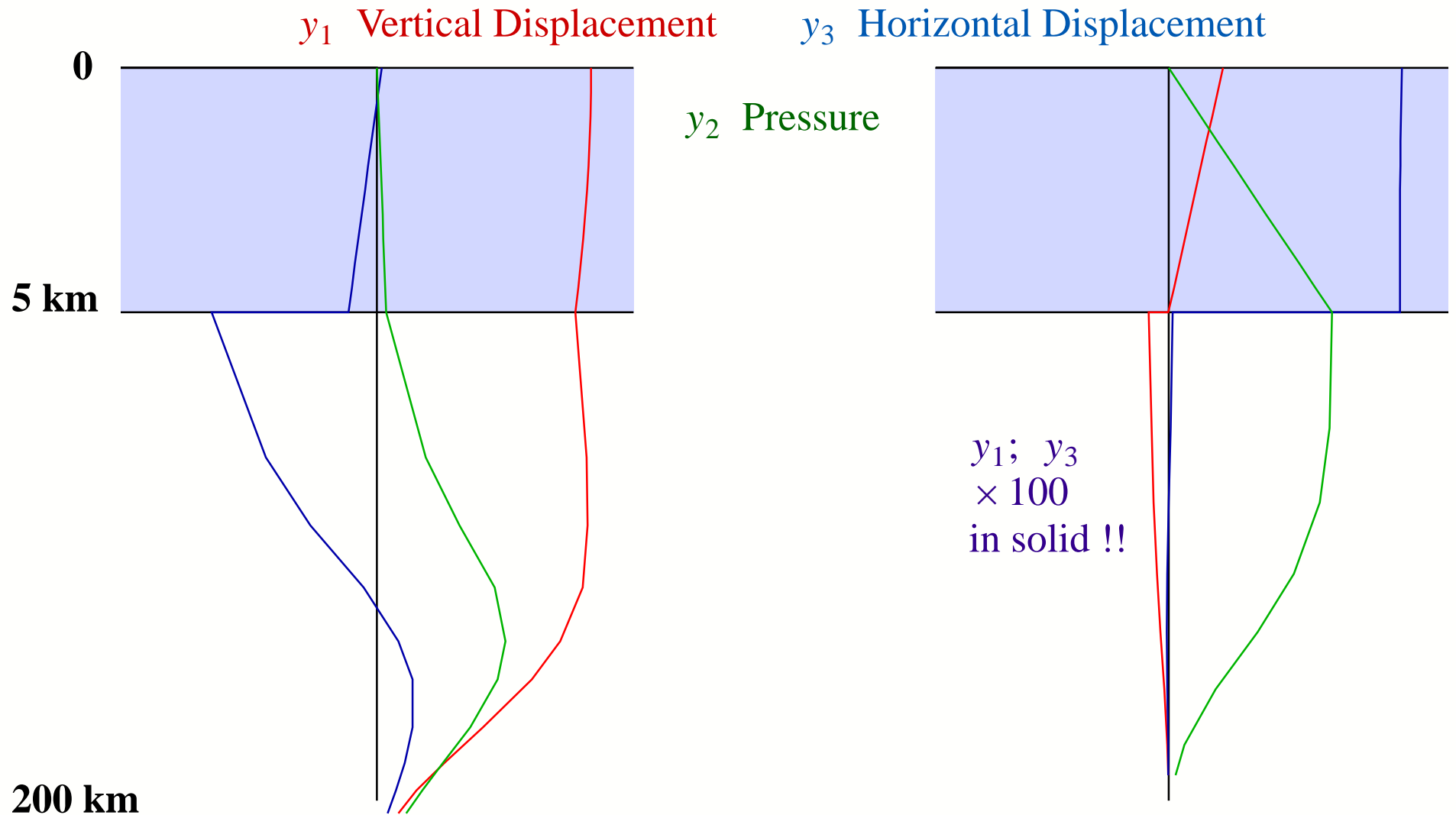
EIGENFUNCTIONS of SPHEROIDAL MODES

Rayleigh Mode

$l = 200; T = 52 s$

Tsunami Mode

$l = 200; T = 908 s$



TSUNAMI EIGENFUNCTION is CONTINUED (SMALL) into SOLID EARTH

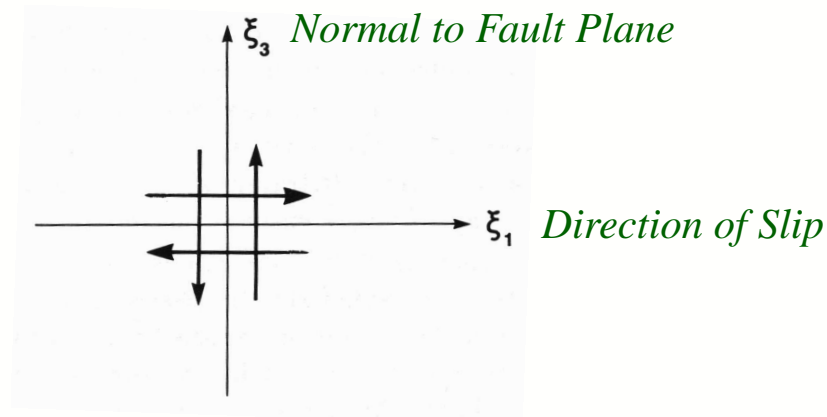
EXCITATION OF TSUNAMI in NORMAL MODE FORMALISM

- *Gilbert* [1970] has shown that the response of the Earth to a point source consisting of a single force \mathbf{f} can be expressed as a summation over all of its normal modes

$$\mathbf{u}(r, t) = \sum_N \mathbf{s}_n(\mathbf{r}) \left(\mathbf{s}_n^*(\mathbf{r}_s) \cdot \mathbf{f}(\mathbf{r}_s) \right) \cdot \frac{1 - \cos \omega_n t \exp(-\omega_n t/2Q_n)}{\omega_n^2},$$

the *EXCITATION* of each mode being proportional to the *scalar product of the force \mathbf{f} by the eigen-displacement \mathbf{s} at location \mathbf{r}_s* .

- Now, an *EARTHQUAKE* is represented by a system of forces called a *double – couple*:



The response of the Earth to an earthquake is thus

$$\mathbf{u}(r, t) = \sum_N \mathbf{s}_n(\mathbf{r}) \left(\boldsymbol{\varepsilon}_n^*(\mathbf{r}_s) : \mathbf{M}(\mathbf{r}_s) \right) \cdot \frac{1 - \cos \omega_n t \exp(-\omega_n t/2Q_n)}{\omega_n^2}$$

where the *EXCITATION* is the *scalar product* of the earthquake's **MOMENT \mathbf{M}** with the local *eigenstrain $\boldsymbol{\varepsilon}$* at the source \mathbf{r}_s .

This formula is directly applicable to the case of a tsunami represented by normal modes of the Earth.

ADVANTAGES of NORMAL MODE FORMALISM

- **Handles any Ocean-Solid Earth Coupling
Including Sedimentary Layers**
- **Works well at Higher Frequencies
No need to assume Shallow-Water Approximation**

DRAWBACKS of NORMAL MODE FORMALISM

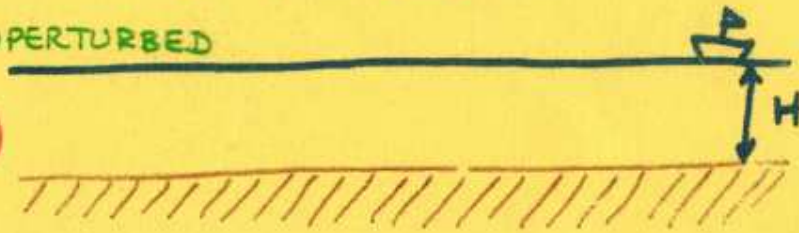
- **Must assume Laterally Homogeneous Structure**
- **Linear Theory -- Does not allow for Large Amplitudes**

ORIGIN of TSUNAMI ENERGY

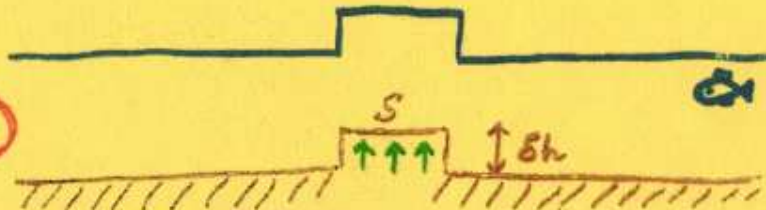
The Dislocation

UNPERTURBED

①



②

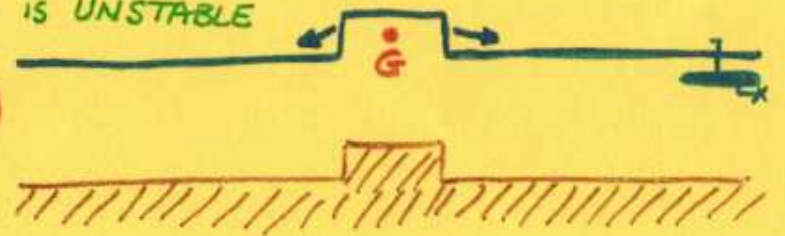


work of pressure forces upon deformation: $W = \rho_w S g H \delta h$

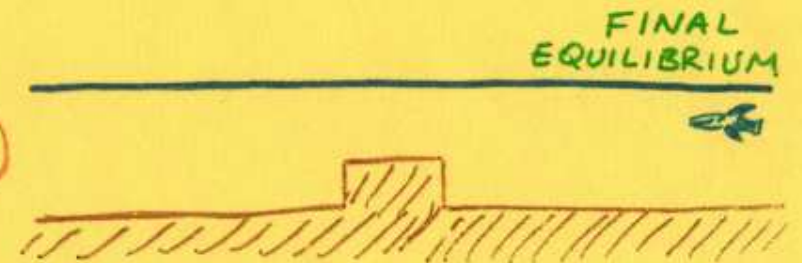
(Also, move water block a height H)

HUMP on SURFACE IS UNSTABLE

③



④



FINAL EQUILIBRIUM

Gravitational energy of hump decreases between ③ and ④

by amount:

$$E_T = \frac{\delta h}{2} \cdot \rho_w \cdot g \cdot S \delta h$$

This is the energy of the tsunami

$$E_T = \frac{1}{2} \rho_w g S (\delta h)^2$$

note:
scales as L^4

NOTE: Energy scales as L^4 , i.e., as $M_0^{4/3}$.

ENERGY of a TSUNAMI -- STATIC THEORY [*Kajiura, 1981*]

$$E = \frac{1}{2} \frac{\rho_w g}{\mu^2} \alpha^{2/3} \cdot F(\delta, \lambda, h, R) \cdot M_0^{4/3} = \frac{1}{2^{4/3}} \frac{\rho_w g}{\mu^{4/3}} \epsilon_{\max}^{2/3} \cdot F \cdot M_0^{4/3}$$

- * α = invariant ratio of M_0 to $S^{3/2}$
- * F : dimensionless factor expressing geometry of faulting, and aspect ratio R of fault rupture area.

NOTE: Energy of Tsunami grows faster than Seismic Moment

Energy released by rupture, proportional to M_0 : ϵ grows like moment.

Hence, Fraction of Earthquake Energy transferred to Tsunami Grows with Earthquake Size

Fortunately, it remains *VERY SMALL*

(max. 1.3% for Chile, 1960)

TSUNAMI ENERGY COMPUTED from NORMAL MODE THEORY

[Okal, 2003]

- Compute Kinetic Energy of water in Normal Mode Formalism

Note that most energy is carried by HORIZONTAL FLOW

Weigh by excitation function for each mode for given seismic moment M_0 .
(averaged over focal geometry)

- Sum over individual modes (equivalent to integrating over frequency)

Account for source spectrum (according to seismic scaling laws)

Account for Finite extent of source depth.

$$E = 0.219 \frac{\rho_w g}{\mu^{4/3}} \cdot \epsilon_{\max}^{2/3} \cdot M_0^{4/3}$$

Essentially Equivalent to Kajiura's.

E grows as $M_0^{4/3}$

Sumatra 2004: $E \approx 7.5 \times 10^{23}$ erg
(100 times Hiroshima)

WHAT ABOUT THE ATMOSPHERE ?

If the tsunami eigenfunction is prolonged into the Solid Earth which is not totally rigid,

- **It should be possible to prolong it into the atmosphere, which is not a perfect vacuum.**

(The sea surface is not a totally "free" boundary)

- **This idea, hinted at by *Yuen et al.* [1970], was proposed by *Peltier* [1976].**

<<<<<< **STAY TUNED** >>>>>>

M_{TSU}

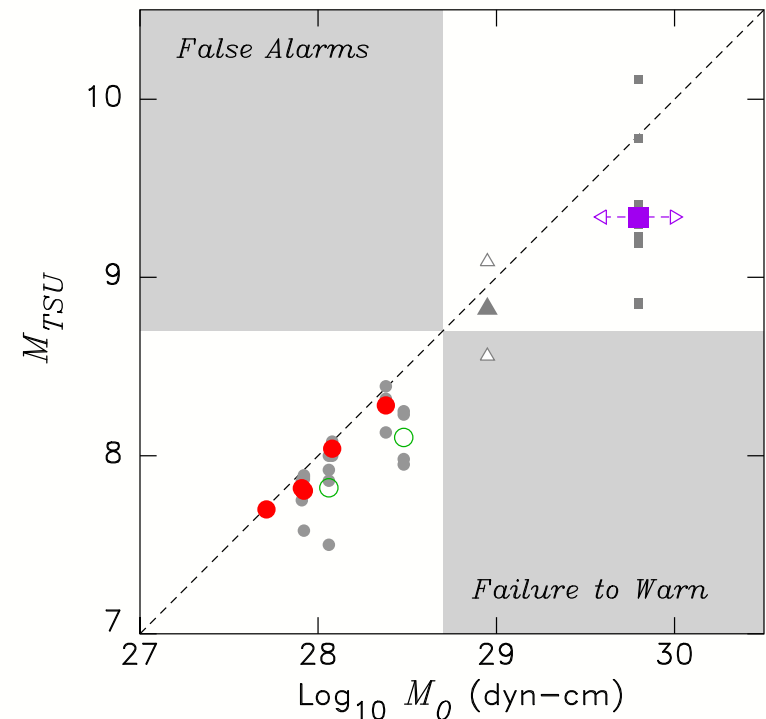
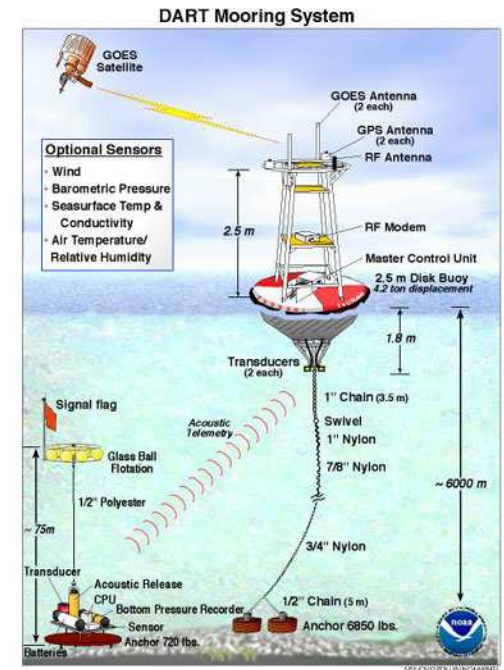
- Use high seas tsunami waveforms recorded by DART system
- Consider tsunami as free oscillation branch of Earth's normal modes [Ward, 1980]
- Recall Magnitude M_m for seismic mantle waves;
Define

$$M_{TSU} = \log_{10} X(\omega) + C_D + C_S + C_0$$

$$\text{Then, } \log_{10} M_0 = M_{TSU} + 20$$

- *IT WORKS !!*

[Okal and Titov, 2006]



RECALL MANTLE MAGNITUDE

[Okal and Talandier, 1989]

$$M_m = X(\omega) + C_D + C_S + C_0$$

- Applied to mantle Rayleigh waves; typically, $T = 50$ to 300 seconds.
- $X(\omega)$ is spectral amplitude in $\mu\text{m}\cdot\text{s}$
- C_D is distance correction
- C_S is source (frequency) correction
- $C_0 = -0.90$ is locking constant (predicted theoretically)

THEN, M_m is directly related to seismic moment M_0 :

$$M_m = \log_{10} M_0 - 20$$

M_m combines simple "**quick-and-dirty**" concept of one-station *magnitude* with modern analytical approach (measuring a *bona fide* physical quantity, the seismic moment, using physical units). **It does not saturate.**

Valid even for 1960 Chilean earthquake.

A tsunami wave on the high seas is a branch of normal modes of the Earth [Ward, 1980].

→ QUESTION: Can we extend the concept of M_m to a tsunami wave measured on the high seas -- and call it M_{TSU} ?

DEVELOPING A FORMULA FOR M_{TSU}

The basic formula for the spectral amplitude of a spheroidal wave by a dislocation remains applicable:

$$X(\omega) = M_0 \cdot a \sqrt{\frac{\pi}{2}} \cdot \frac{1}{\sqrt{\sin \Delta}} e^{-\frac{\omega a \Delta}{2UQ}} \cdot \left[\frac{1}{U} \left| s_R l^{-1/2} K_0 - p_R l^{3/2} K_2 - i q_R l^{1/2} K_1 \right| \right]$$

$$M_m = \log_{10} M_0 - 20 = \log_{10} X(\omega) + C_D + C_S + C_0$$

Need only adjust the corrections C_D and C_S and the constant C_0 .

THE DISTANCE CORRECTION C_D

$$C_D = \frac{1}{2} \log_{10} \sin \Delta$$

THE SOURCE (FREQUENCY) CORRECTION C_S

$$C_S = -\log_{10} \left[\frac{\langle |s_R - p_R| \rangle \omega^{1/2} g^{-3/4}}{8\pi \mu a^{3/2}} \cdot H^{-3/4} \right]$$

$$C_S = 0.087 \theta^3 - 0.069 \theta^2 + 0.508 \theta + 2.299$$

$$(\theta = \log_{10} T - 3.122).$$

(The latter formula uses *Okal's* [2003] asymptotic expressions of the tsunami eigenfunction to compute the various excitation coefficients for a shallow source in the limit $\omega \rightarrow 0$).

DEVELOPING A FORMULA FOR M_{TSU}

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$$M_m = \log_{10} M_0 - 20 = \log_{10} X(\omega) + C_D + C_S + C_0$$

Need only adjust the corrections C_D and C_S and the constant C_0 .

THE LOCKING CONSTANT C_0

- If $X(\omega)$ is the spectrum of the wave height at the surface in **cm*s**, then

$$C_0 = 3.10$$

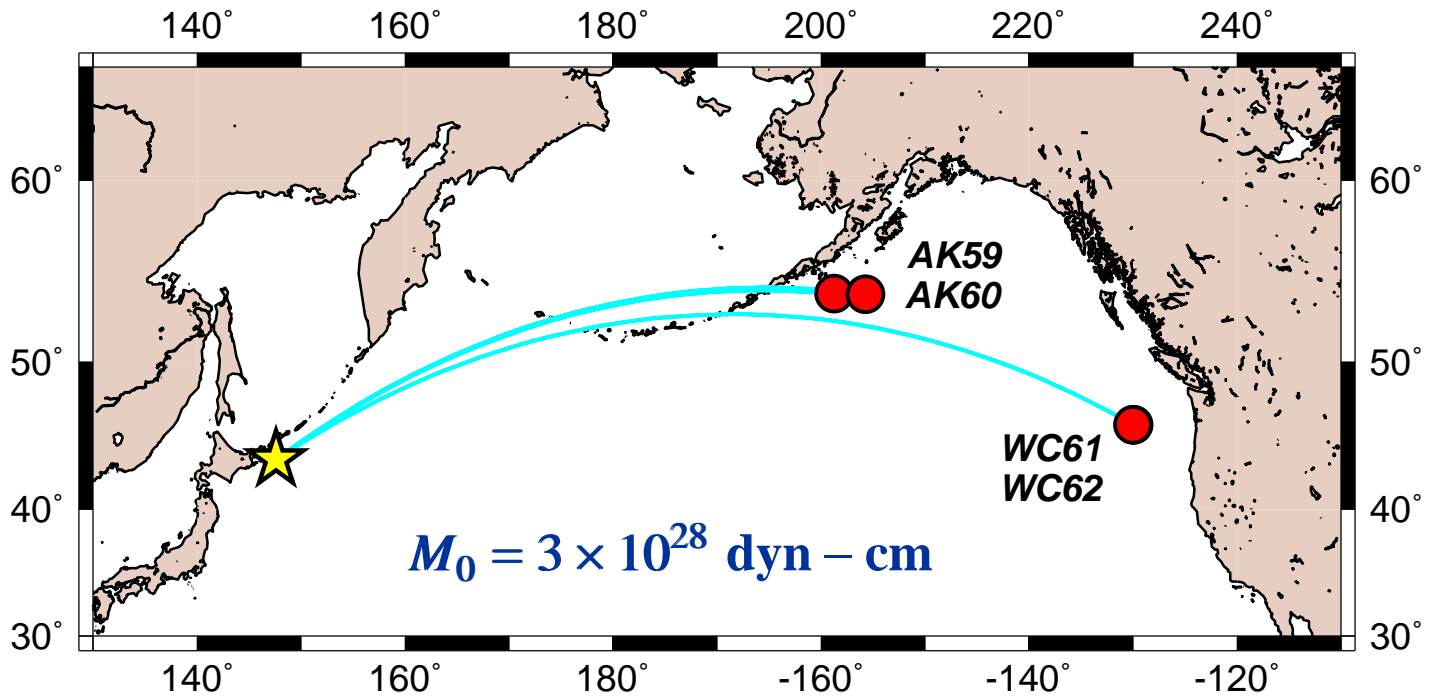
- If one uses the bottom pressure $p(t)$ recorded in **dyn/cm²** on the ocean bottom, then use $P(\omega)$ rather than $X(\omega)$; [$P(\omega) = \rho_w g X(\omega)$], and

$$C_0 = 0.11$$

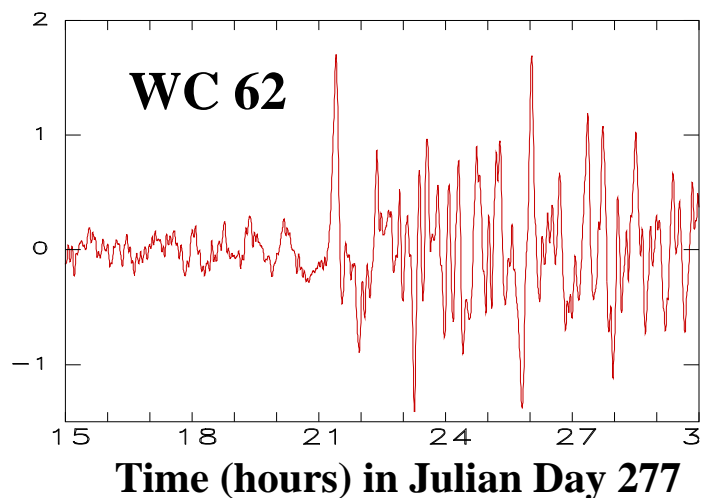
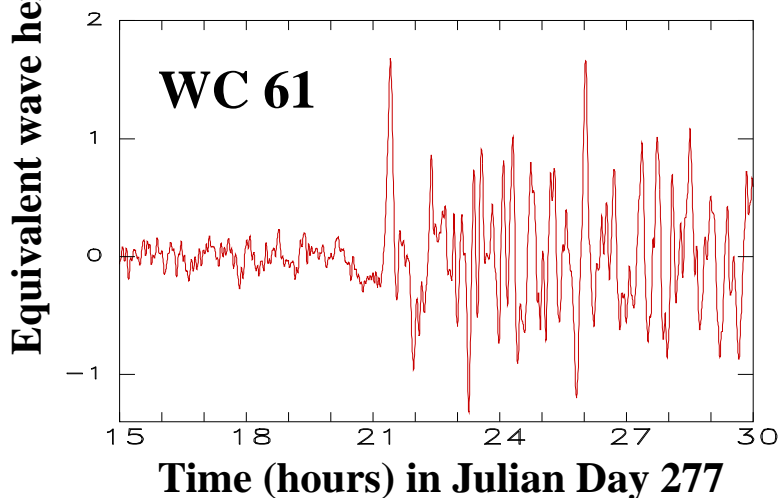
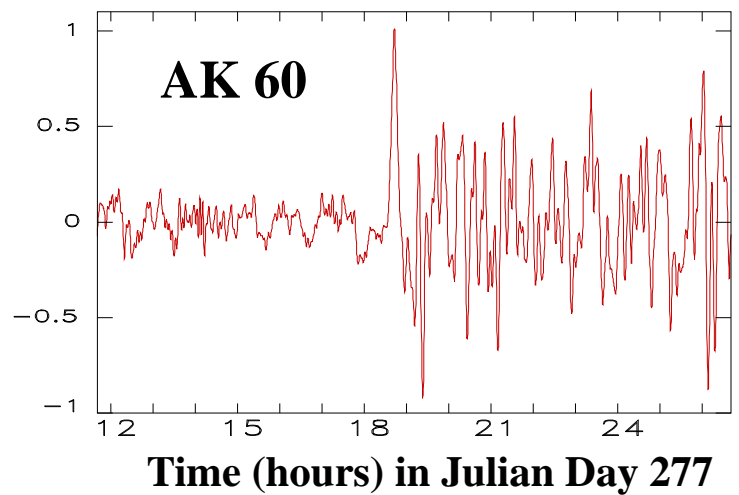
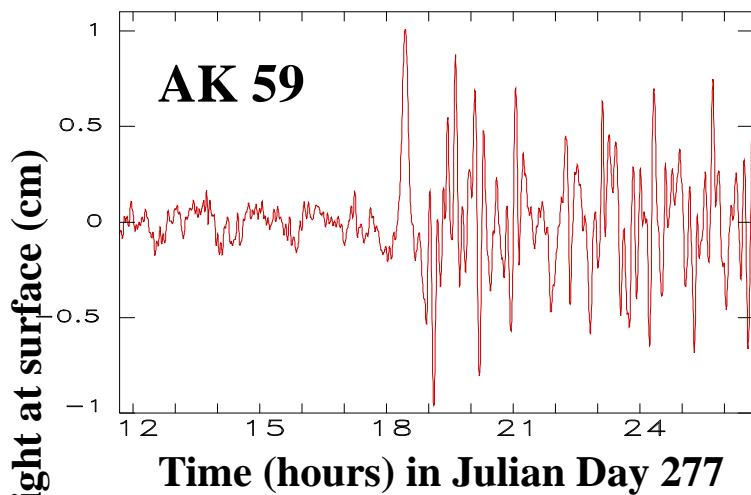
- If $p(t)$ is recorded in **pounds[-force] per square inch**, then

$$C_0 = 4.95$$

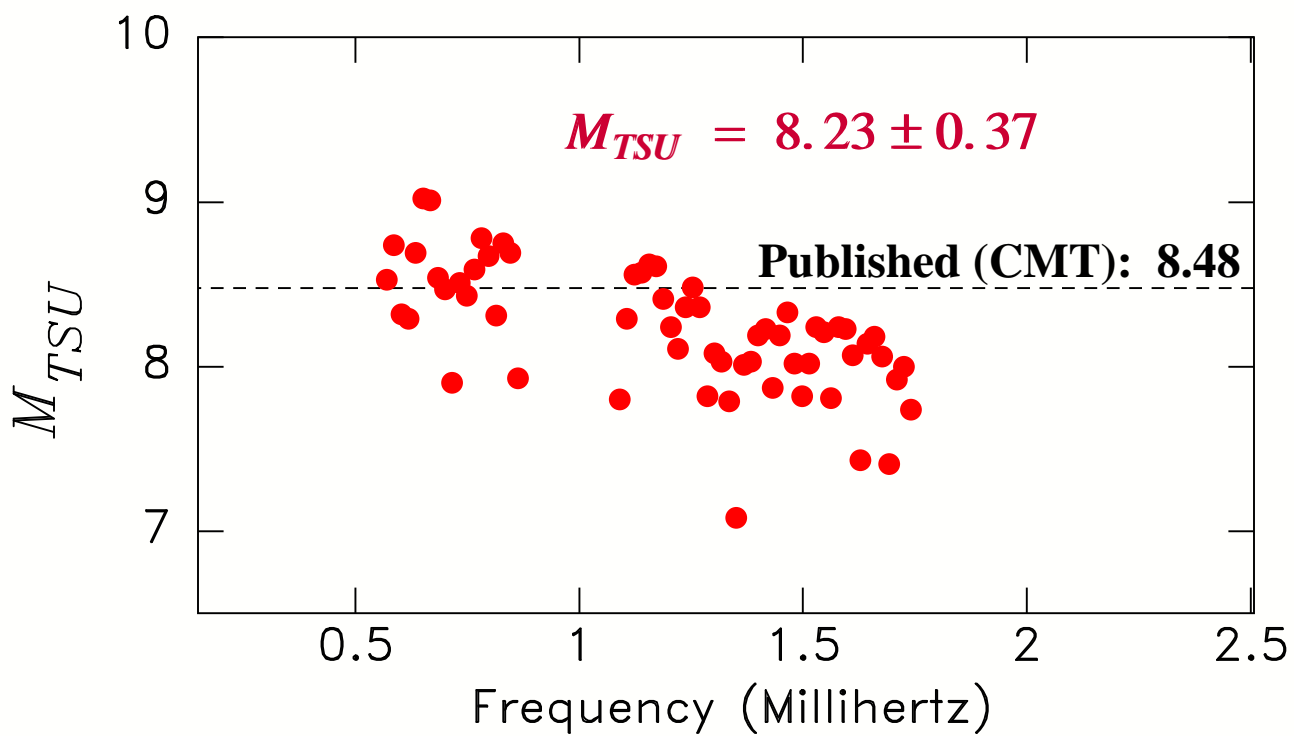
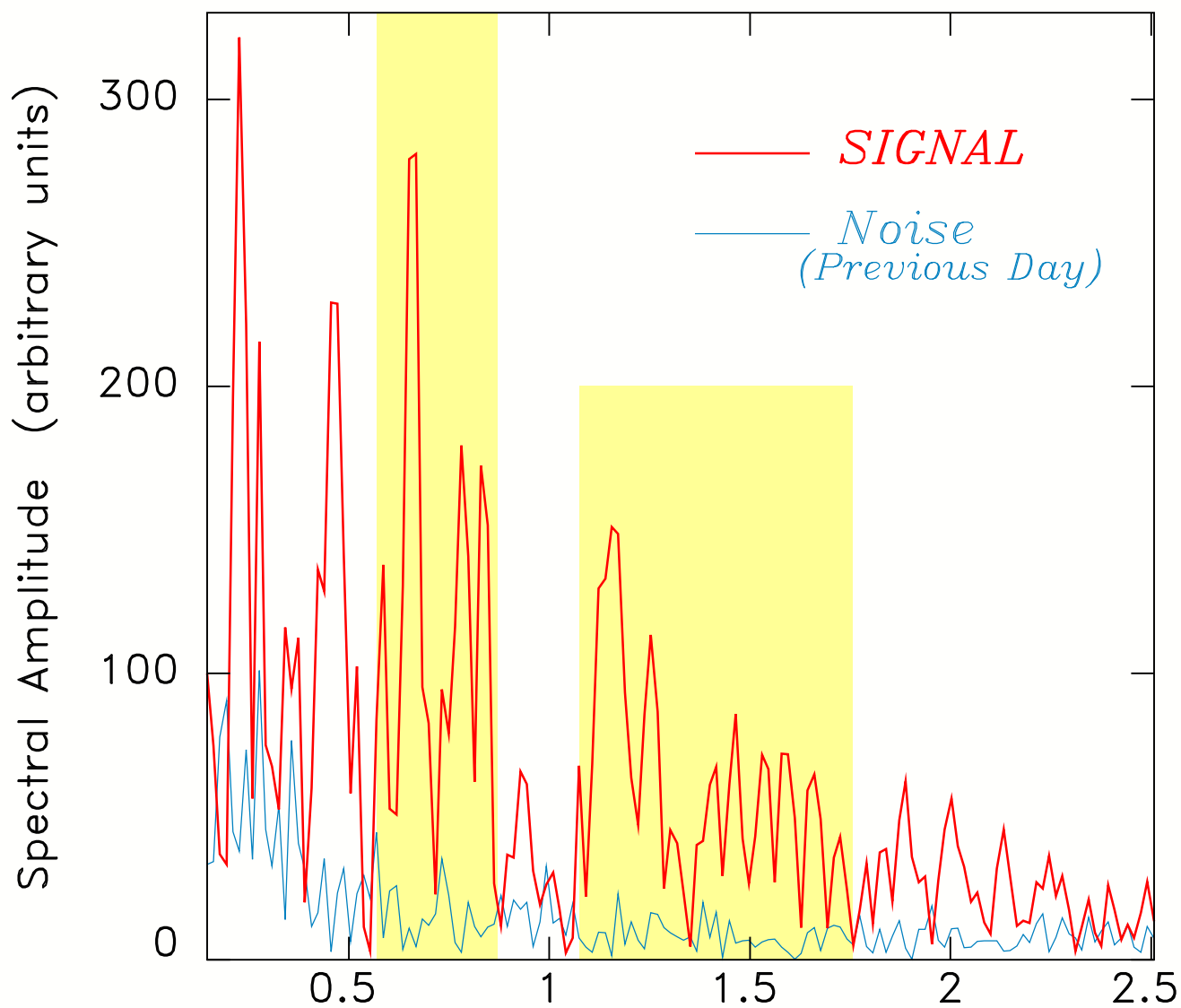
Case Study: KURIL ISLANDS, 04-OCT-1994



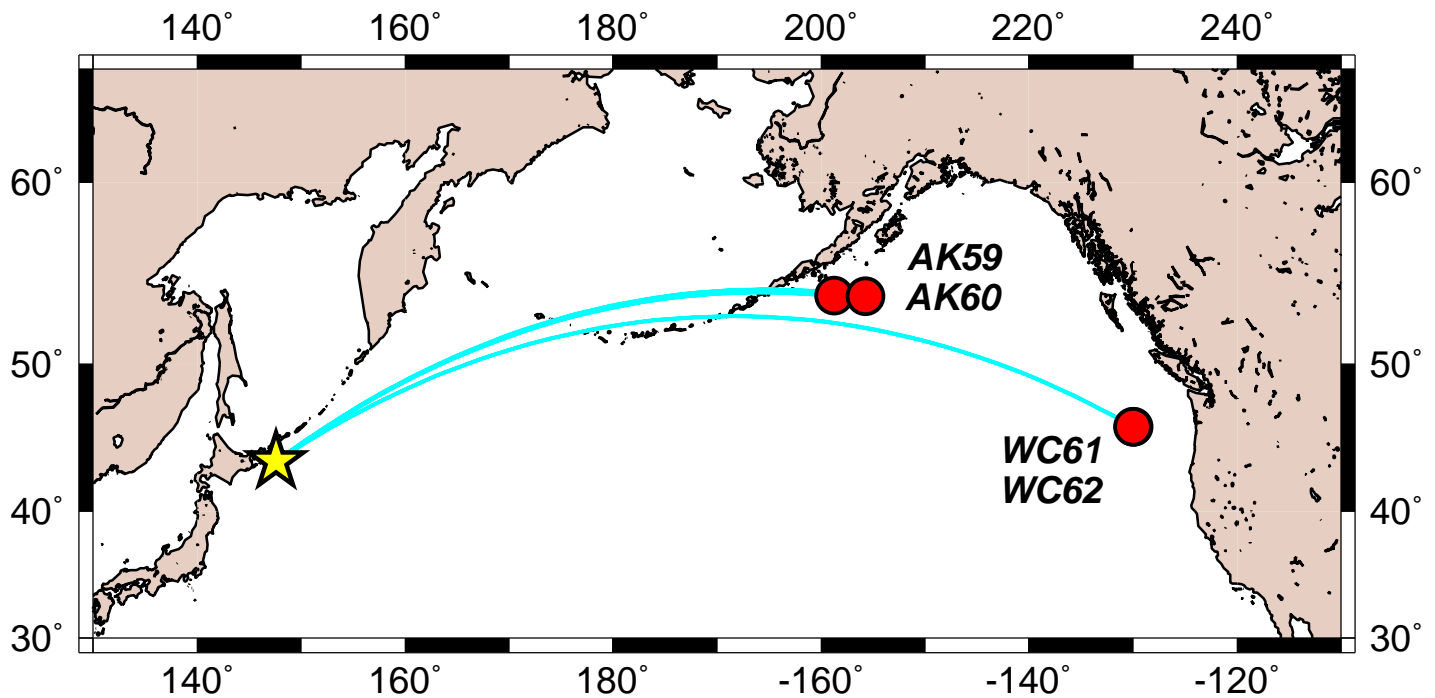
To date, Largest Event Recorded by DART



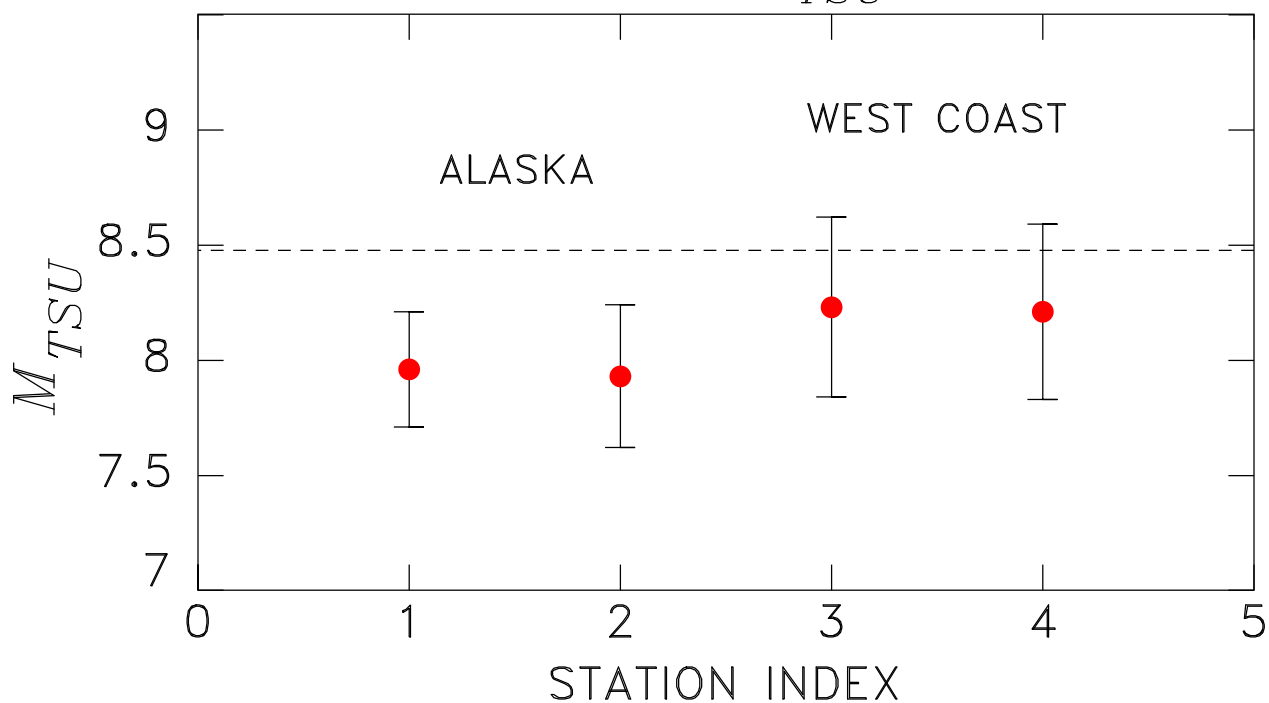
WC62 KURILES 1994



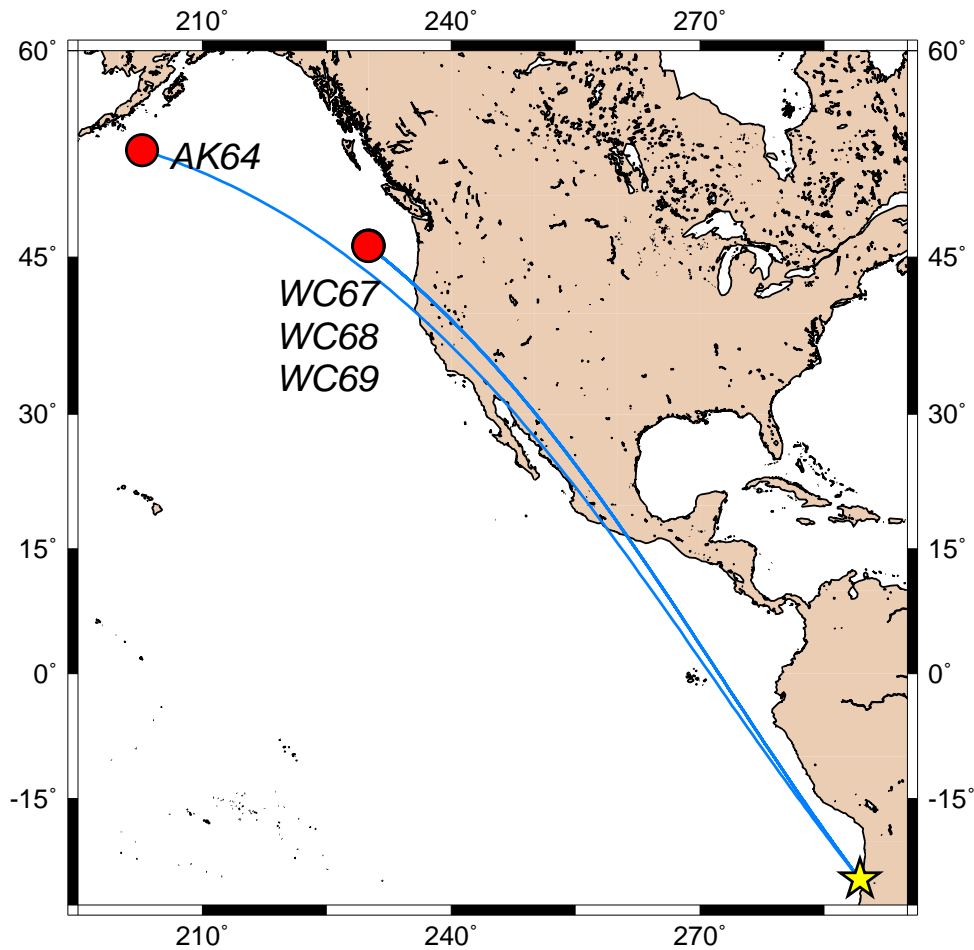
Case Study: KURIL ISLANDS, 04-OCT-1994



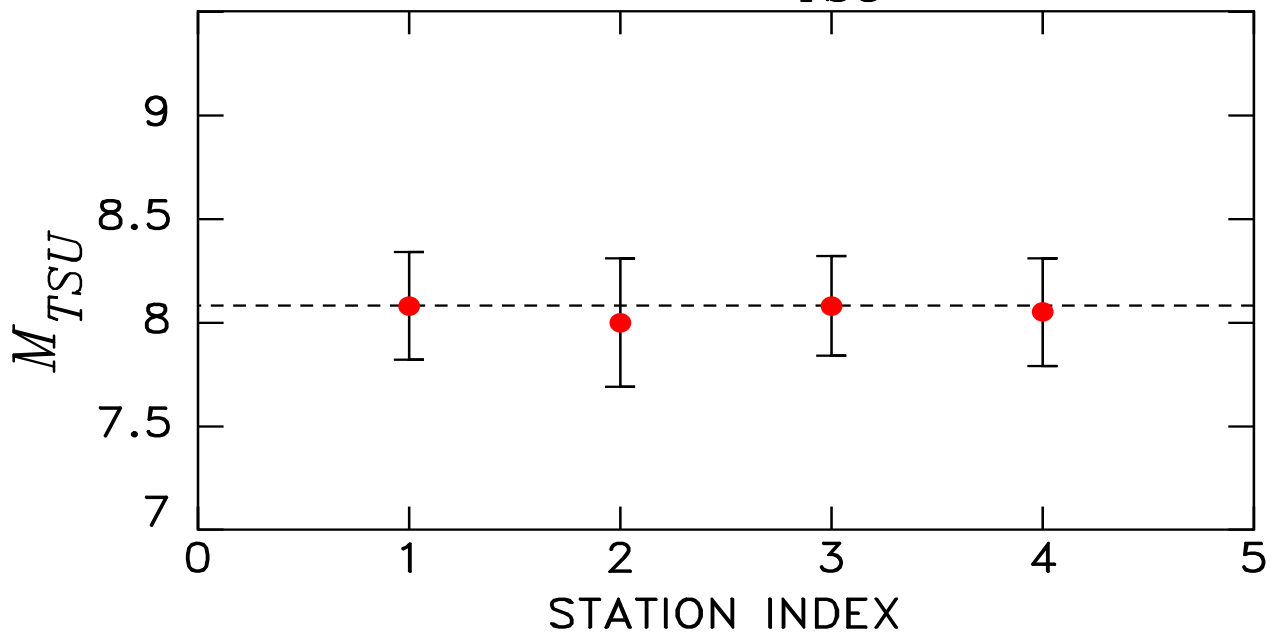
Published: 8.48; Mean $M_{TSU} = 8.08 \pm 0.14$



CHILE -- 30 JUL 1995



Published: **8.08**; Mean $M_{TSU} = 8.05 \pm 0.03$



Works despite *UNFAVORABLE GEOMETRY*
requiring *NON-GEOMETRICAL propagation !!*

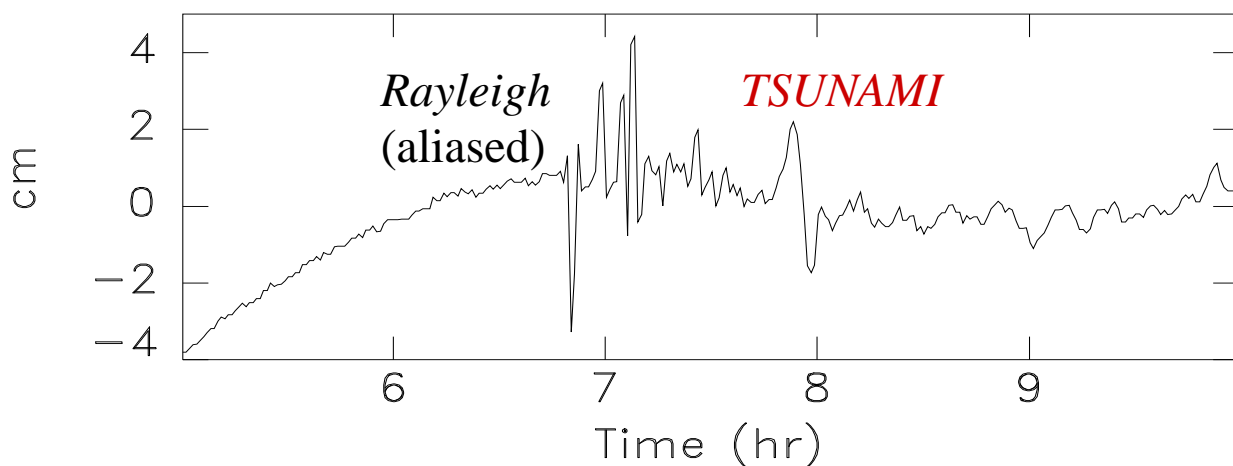
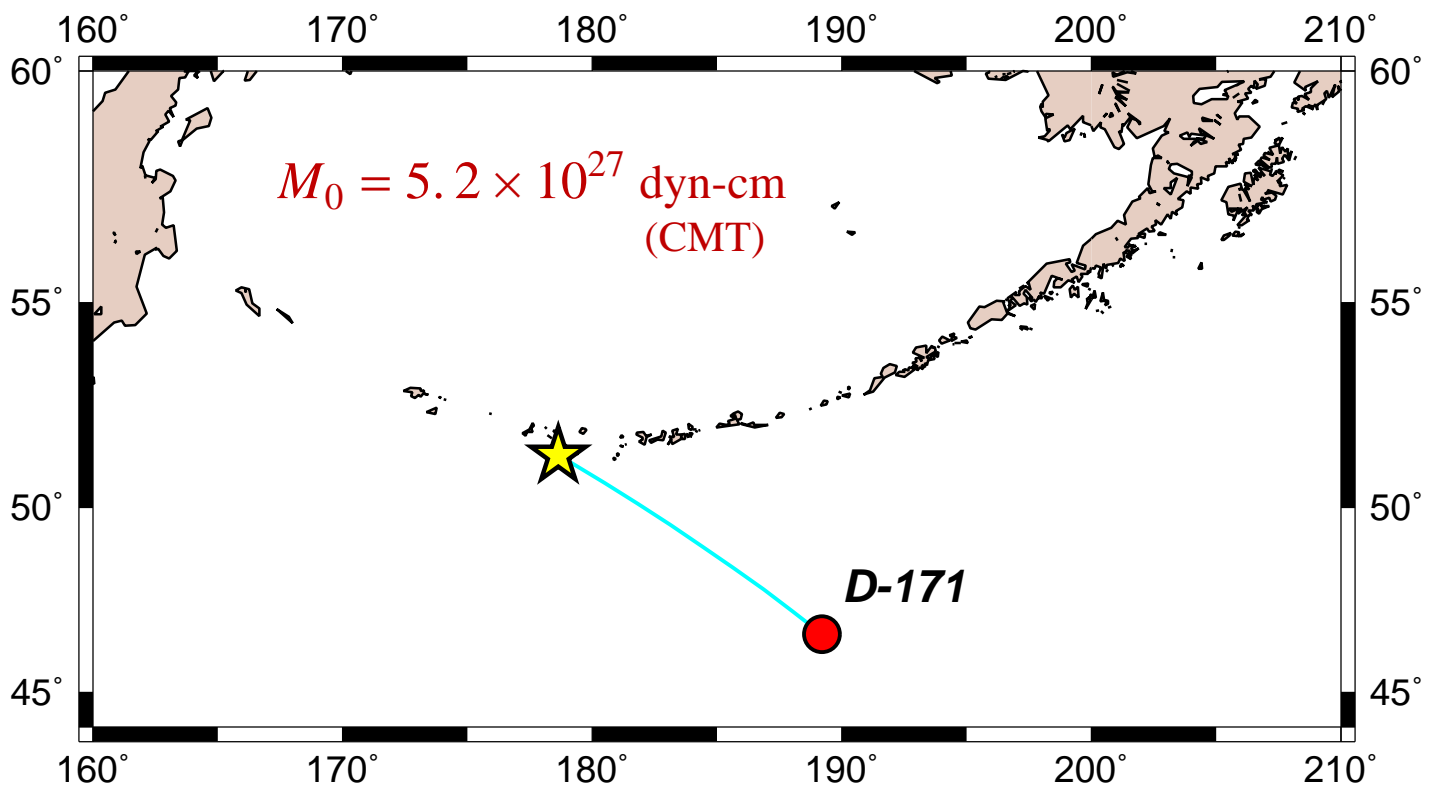
SUCCESSFUL OPERATIONAL USE

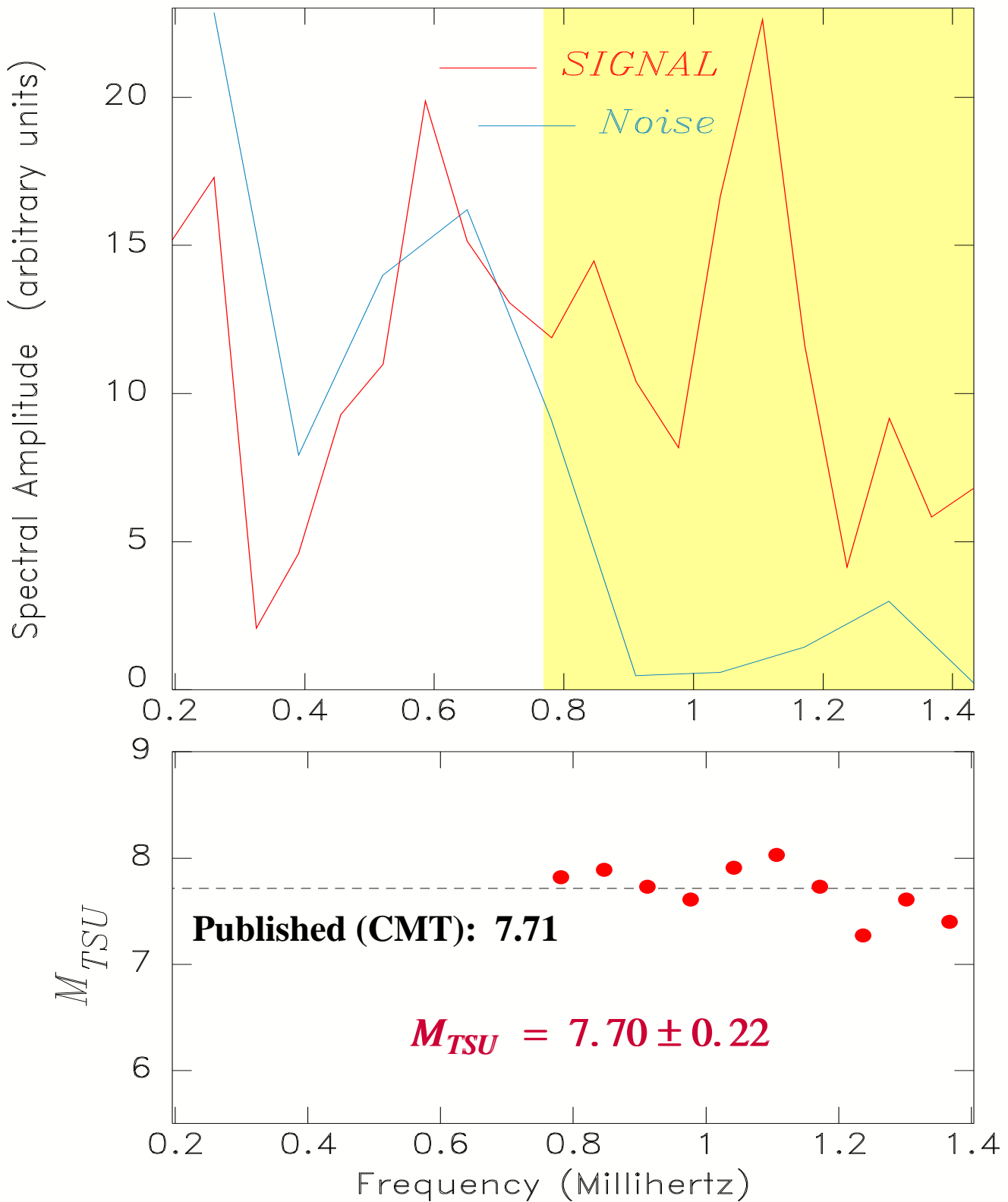
17 NOV 2003

This is a smaller earthquake which was not recorded at the Alaskan and West Coast DART gauges.

However, a new station, D-171, is only 900 km from the epicenter, and clearly recorded the tsunami, although at a very coarse sampling (1 minute).

Despite this limitation, the event can be successfully processed.



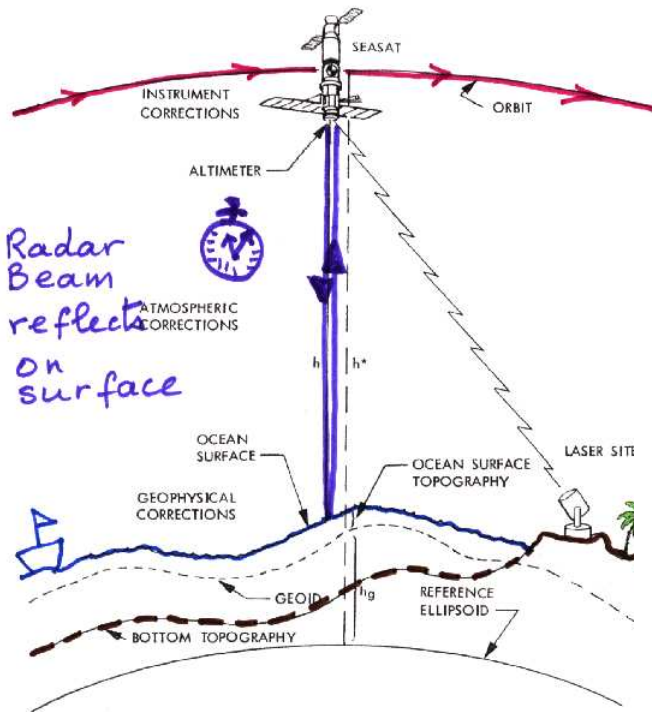


→ This estimate was used in real-time to call off an alert for Hawaii.

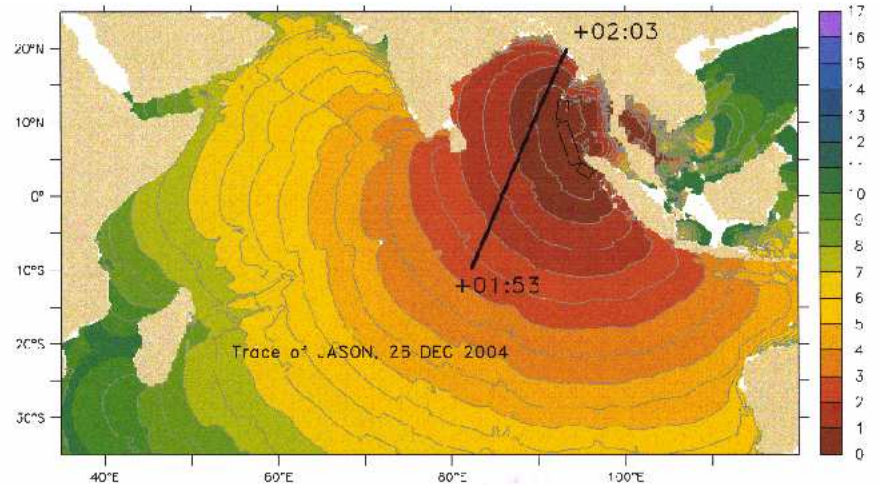
APPLICATION of M_{TSU} to JASON SATELLITE TRACE

DETECTION by SATELLITE ALTIMETRY gives first definitive measurement of **MAJOR tsunami on HIGH SEAS**

(previous detection by *Okal et al.* [1999] during 1992 Nicaragua tsunami -- 8 cm -- at the limit of noise).

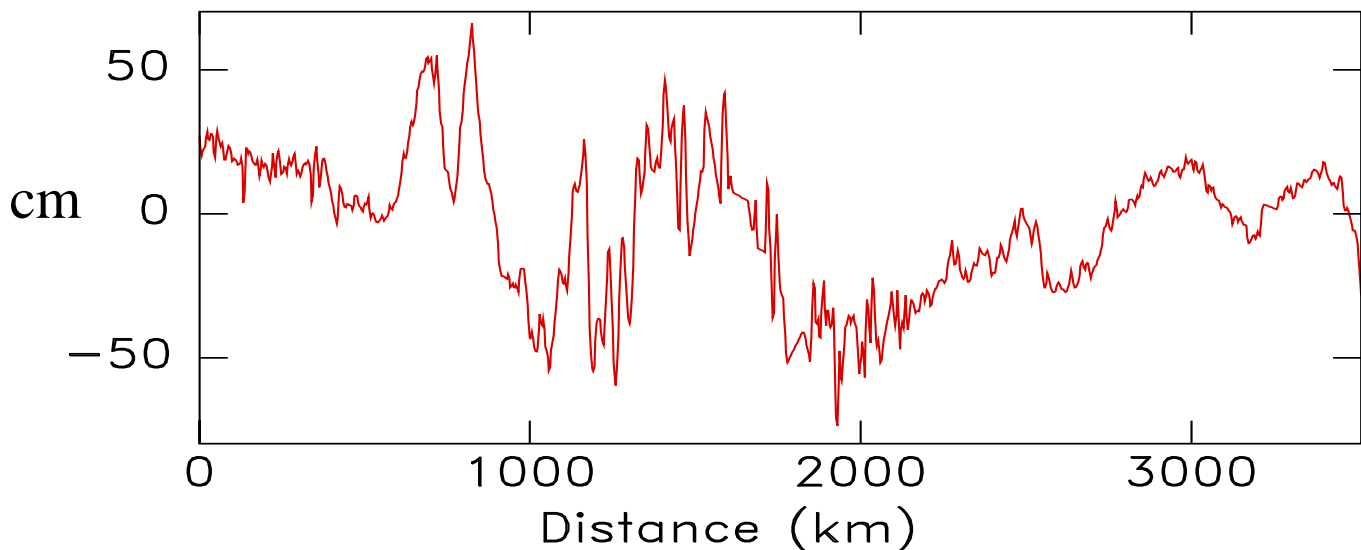


TRACE of ALTIMETRY SATELLITE OVER INDIAN OCEAN

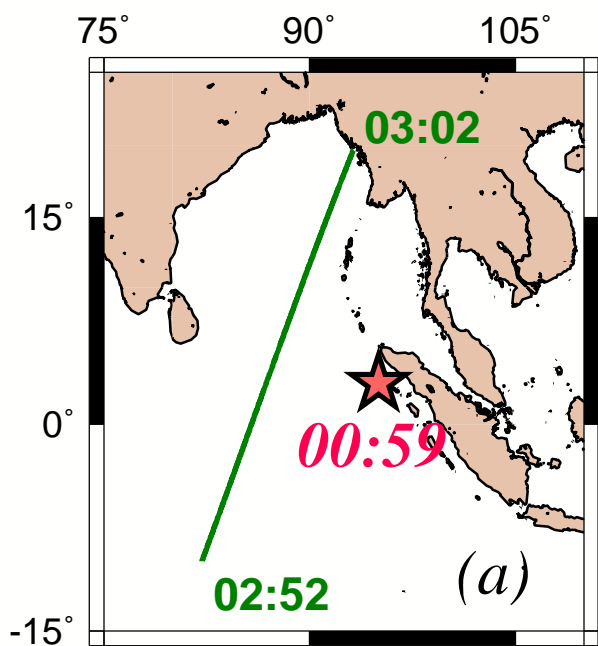


Satellite at the right place at the right time!

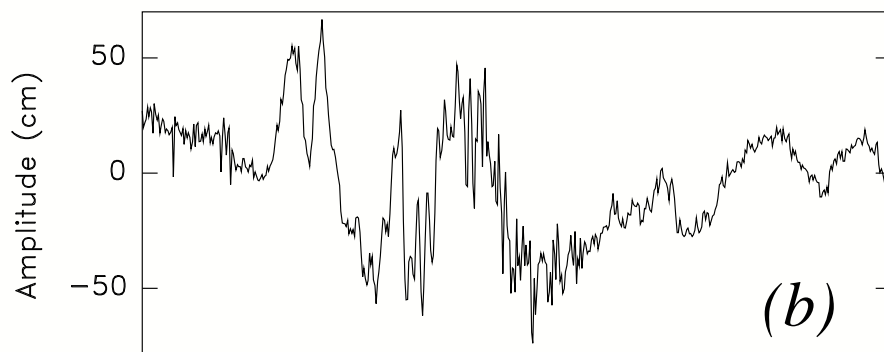
measures 70 cm across Bay of Bengal



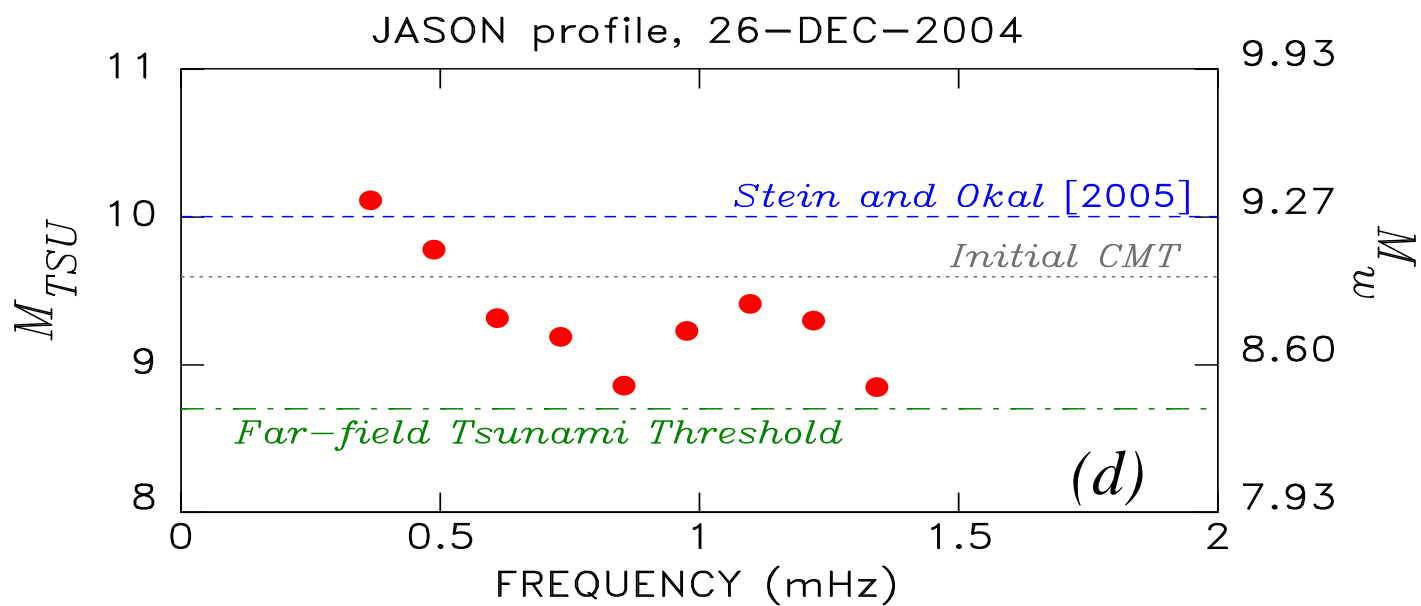
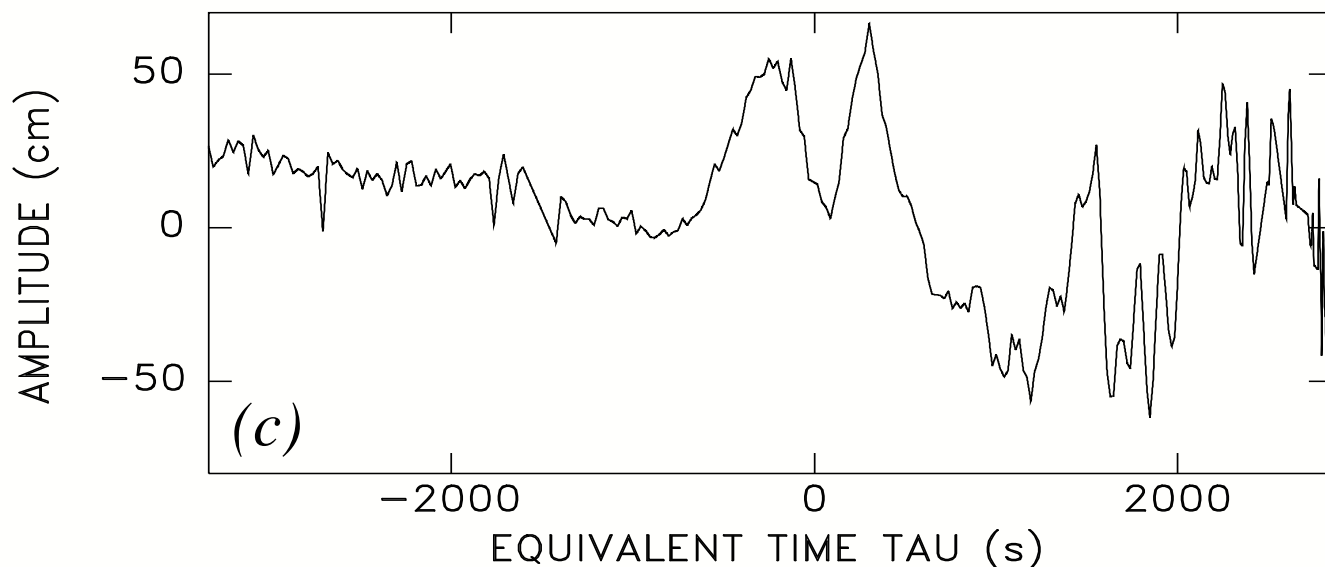
- *QUESTION*: Can we quantify the JASON trace, *i.e.*, recover from it the source of the tsunami ?
- *PROBLEM* : JASON is neither a time series nor a space series.
- *SOLUTION* : Rebuild an approximate times series from the JASON trace, then process through M_{TSU} .



Original Jason Trace



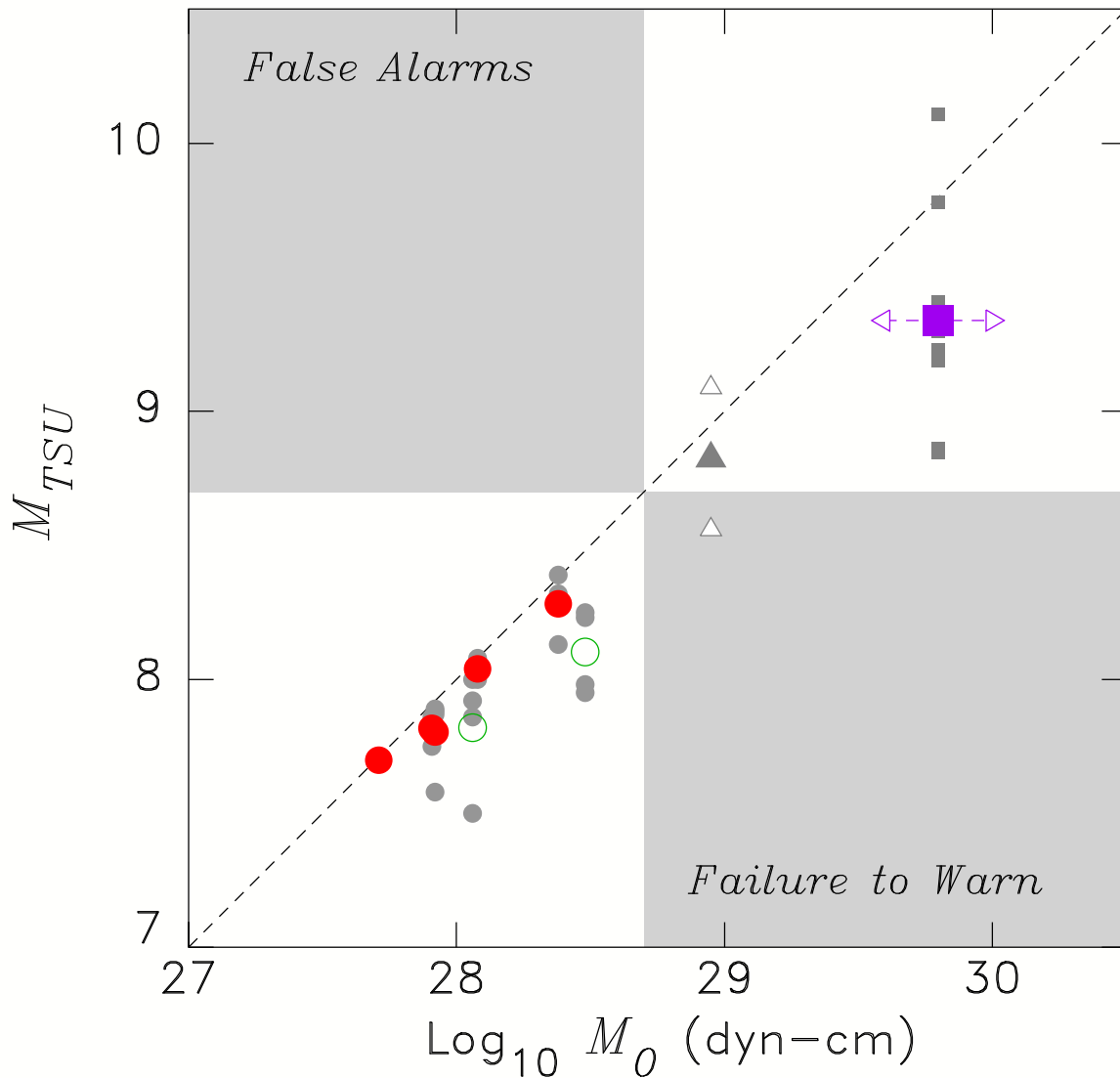
Equivalent Time Series



CONCLUSION: IT WORKS !!

M_{TSU} : CONCLUSION

- The algorithm successfully retrieves the seismic moment of the parent earthquake.



- The examples tested suggest that the precision is sufficient to avoid false alarms and failures to warn.