



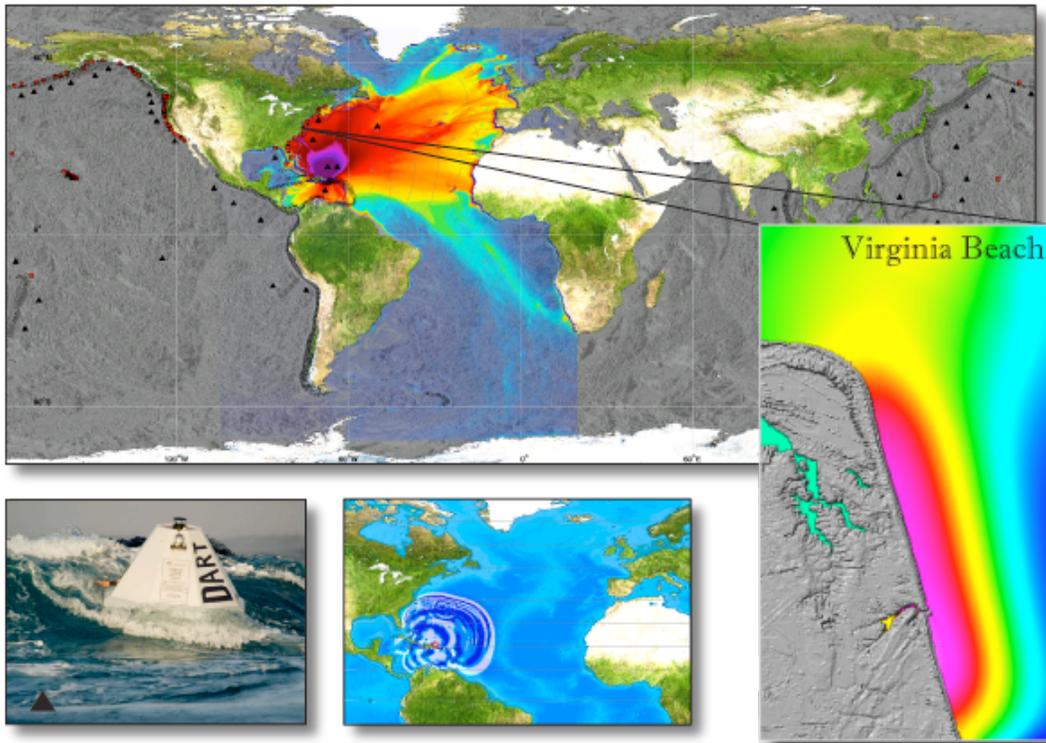
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# *PMEL Tsunami Forecast Series: Vol. 68*

## A Tsunami Forecast Model for Virginia Beach, Virginia

(Draft)

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## Contents

Abstract.....	3
1 Introduction.....	4
2 Forecast Method.....	5
2.1 Construction of a Propagation Scenario Based on Deep-Ocean Tsunameter Measurements and Pre-Computed Tsunami Source Functions .....	5
2.2 Coastal Predictions by Using High-Resolution Forecast Models in Real-Time. 7	
3 Model Development.....	8
3.1 Forecast area .....	8
3.2 Bathymetry and Topography .....	9
3.3 Model Setup.....	10
4 Results and Discussion .....	11
4.1 Sensitivity of modeled amplitude to friction coefficients.....	11
4.2 Model verification and stability testing .....	12
5 Summary and Conclusions .....	13
Acknowledgements.....	14
References.....	15
Tables.....	19
Appendix A.....	22
A1. Reference model *.in file for Virginia Beach, Virginia—updated for 2013 .....	22
A2. Forecast model *.in file for Virginia Beach, Virginia—updated for 2013 .....	24
Figures.....	25
Appendix B Propagation Database: Atlantic Ocean Unit Sources .....	63
Appendix C SIFT Testing Report.....	74

**List of Tables**

<b>Table 1</b> Tsunami source functions in the Pacific, Atlantic and Indian Oceans.....	19
<b>Table 2</b> MOST setups for the Virginia Beach reference and forecast models. ....	20
<b>Table 3</b> Sources of the 9 simulated magnitude-9.3 tsunamis and the maximum computed wave crests at the Virginia Beach warning point.....	21

1 **PMEL Tsunami Forecast Series: Vol. 68**  
2 **A Tsunami Forecast Model for Virginia Beach, Virginia**

3  
4 Liujuan Tang and Christopher Moore

5 **Abstract**

6 This report documents the development and testing of a tsunami forecast model for  
7 Virginia Beach, Virginia as part of NOAA's operational tsunami forecast system. Based  
8 on the Method of Splitting Tsunamis (MOST) model, the forecast model performs  
9 calculations on bathymetry grids with a horizontal resolution of 2 arc-seconds. At this  
10 resolution it is capable of simulating four hours of tsunami wave dynamics in under ten  
11 minutes of computational time. A reference inundation model of higher resolution (1/3  
12 arc-seconds) was also developed in parallel, to provide a reference for the forecast model.  
13 Both models were tested with nine simulated magnitude-9.3 tsunamis from different  
14 source regions and one micro tsunami. Good agreement was observed between the  
15 model computations, and the numerical consistency between the model results for the  
16 maximum amplitudes and currents indicate reliability, robustness, and stability of the  
17 forecast model.

18  
19 The study shows that mega tsunamis from subduction zone earthquakes near the  
20 Puerto Rico Trench can cause severe inundation at Virginia Beach. The results also  
21 highlight that large waves can arrive 12-30 hours after the first wave arrival for far-field,  
22 small to medium sized tsunamis (maximum wave amplitudes near or smaller than 1  
23 meter). This typical long arrival time requires longer warning duration for such events.  
24 Wavelet analyses show broad and relatively long resonant periods from 0.5 hours to  
25 several hours, also suggesting the necessity for long warning durations.

26  
27 The simulated magnitude-9.3 tsunamis show an impressive local variability of  
28 tsunami amplitudes at Virginia Beach, and indicate the complexity of forecasting tsunami  
29 amplitudes at a coastal location. It is essential to use high-resolution models to provide  
30 the accuracy useful for coastal tsunami forecasts and practical guidance.

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36

37 **1 Introduction**

38 The National Oceanic and Atmospheric Administration (NOAA) Center for Tsunami  
39 Research, located at NOAA's Pacific Marine Environmental Laboratory (PMEL), has  
40 developed a tsunami forecasting system for operational use by NOAA's two Tsunami  
41 Warning Centers located in Hawaii and Alaska (Titov *et al.*, 2005; Titov, 2009). The  
42 forecast system combines real-time deep-ocean tsunami measurements from tsunameters  
43 (González *et al.*, 2005; Meinig *et al.*, 2005, Bernard *et al.*, 2006, Bernard and Titov, 2007)  
44 and the Method of Splitting Tsunami (MOST) model, a suite of finite difference  
45 numerical codes based on the nonlinear shallow water wave equations (Titov and  
46 Synolakis, 1998; Titov and González, 1997; Synolakis *et al.*, 2008; Titov *et al.*, 2011) to  
47 produce real-time forecasts of tsunami arrival time, heights, periods and inundation. To  
48 achieve accurate and detailed forecasts of tsunami impact for specific sites, high-  
49 resolution tsunami forecast models are under development for United States coastal  
50 communities at risk (Tang *et al.*, 2008a; 2009; 2010; Arcas and Uslu, 2010; Righi and  
51 Arcas, 2010; Uslu *et al.* 2010; Wei and Arcas, 2010). The resolution of these models has  
52 to be high enough to resolve the dynamics of a tsunami inside a particular harbor,  
53 including influences of major harbor structures such as breakwaters and seawalls. These  
54 models have been integrated as crucial components into the tsunami forecast system.

55

56 As of March 2013 the forecast system real-time measurements come from a network  
57 of 58 tsunameter stations deployed at optimal locations in the Pacific, Atlantic, Indian  
58 Oceans, Caribbean Sea, the Gulf of Mexico and South China Sea (Spillane *et al.*, 2008).  
59 While the buoy array is owned and maintained by nine different nations (U.S.A.,  
60 Australia, Chile, China, Japan, India, Indonesia, Thailand and Russian), the data from the  
61 entire array are made publically available in real-time via the Global  
62 Telecommunications System (GTS). The data from the tsunameters is used to provide  
63 guidance by comparing them to pre-computed open ocean model results. These pre-  
64 computed propagation models currently cover all three ocean basins (Pacific, Atlantic,  
65 and Indian), and are comprised of 1,725 different tsunami scenarios with initial  
66 deformations covering the major tsunamigenic subduction zones throughout the world  
67 (Figure 1 and Table 1). High-resolution forecast inundation models are now set up for 75  
68 U.S. coastal communities (e.g. Fig. 1). The fully implemented system will use real-time  
69 data from the tsunameter network to provide high-resolution tsunami forecasts for at least  
70 75 communities in the U.S. by 2013, with additional models envisioned later for smaller  
71 communities. Since its first testing in the 17 November 2003 Rat Island tsunami, the  
72 forecast system has produced experimental real-time forecasts for more than 20 tsunamis  
73 in the Pacific and Indian oceans (Titov *et al.*, 2005; Wei *et al.*, 2008; Titov, 2009; Titov  
74 and Tang, 2011; Tang *et al.*, 2012; [http://nctr.pmel.noaa.gov/database\\_devel.html](http://nctr.pmel.noaa.gov/database_devel.html)). The  
75 forecast method has also been tested with data from nine additional events that produced  
76 deep-ocean tsunameter data including several near-field tsunamis  
77 ([http://nctr.pmel.noaa.gov/database\\_devel.html](http://nctr.pmel.noaa.gov/database_devel.html); Titov *et al.*, 2005; Tang *et al.*, 2008b;  
78 Wei *et al.*, 2012).

79

80 This report describes the development and testing of the Virginia Beach forecast  
81 model. The objective in developing this model is to provide NOAA's Tsunami Warning  
82 Centers the ability to assess danger posed to Virginia Beach following tsunami generation  
83 in the Atlantic Ocean Basin with a goal to provide accurate and timely forecasts to enable  
84 the community to respond appropriately. Dr. Aurelio Mercado developed the first version  
85 of a Virginia Beach forecast model in 2007. It was updated in 2008 and had been  
86 working in the tsunami forecast system. As new bathymetric/topographic and tsunami  
87 data came in and the model development technique progressed further, the model had  
88 been updated and re-tested in March 2013. A secondary objective of the report is to  
89 explore the potential tsunami impact from earthquakes at major subduction zones in the  
90 Atlantic Ocean to the city by using the developed forecast model. Wavelet analysis was  
91 applied to investigate the local responses to tsunami waves.

92

93 The report is organized as follows. Section 2 briefly introduces NOAA's tsunami  
94 forecast method. Section 3 describes the model development. Section 4 presents the  
95 results and discussion, which includes model sensitivity study to friction coefficient,  
96 model verification, and testing for simulated tsunamis. A summary and conclusion are  
97 provided in section 5.

98

## 99 **2 Forecast Method**

100 NOAA's real-time tsunami forecasting scheme is a process that comprises two steps:  
101 (1) construction of a propagation scenario via inversion of deep ocean tsunameter  
102 measurements with pre-computed tsunami source functions; and (2) coastal predictions  
103 by running high-resolution forecast models in real time (Titov *et al.* 1999; 2005; Titov  
104 2009; Tang *et al.*, 2009, Tang *et al.*, 2012). The tsunameter-constrained tsunami source,  
105 the corresponding offshore scenario from the tsunami source function database, and high-  
106 resolution forecast models cover the entire evolution of earthquake-generated tsunamis,  
107 generation, propagation and coastal inundation, providing a complete tsunami forecast  
108 capability.

109

### 110 **2.1 Construction of a Propagation Scenario Based on Deep-Ocean Tsunameter** 111 **Measurements and Pre-Computed Tsunami Source Functions**

112 Several real-time data sources, including seismic data, coastal tide gage and deep-  
113 ocean data have been used for tsunami warning and forecasting (Satake *et al.*, 2008;  
114 Whitmore, 2003; Titov, 2009). NOAA's strategy for the real-time forecasting is to use  
115 deep-ocean measurements at tsunameter stations, also known as DART™ (Deep-ocean  
116 Assessment and Reporting of Tsunami) buoys, as the primary data source due to several  
117 key features: (1) tsunameters provide a direct measure of tsunami waves, unlike seismic  
118 data, which are an indirect measure of tsunamis, (2) deep ocean tsunami measurements  
119 are in general the earliest tsunami information available, since tsunamis propagate much

120 faster in deep ocean than in shallow coastal area where coastal tide gages are located, (3)  
121 compared to coastal tide gages, tsunameter data with a high signal to noise ratio can be  
122 obtained without interference from harbor and local shelf effects, and (4) wave dynamics  
123 of tsunami propagation in deep water is assumed to be linear (Kânoğlu and Synolakis,  
124 2006; Liu, 2009). This linear process allows application of efficient inversion schemes.

125 Time series of tsunami observations in deep water (depths  $\ll$  wave length) can be  
126 decomposed into a linear combination of a set of tsunami source functions in the time  
127 domain by a linear Least Squares method (Percival *et al.*, 2011). The coefficients  
128 obtained through this inversion process are called *tsunami source coefficients*. During  
129 real-time tsunami forecasting, seismic waves propagate much faster than tsunami waves  
130 so the initial seismic magnitude can be estimated before the tsunameter data are available.  
131 Since time is of the essence, this initial tsunami forecast is based on the seismic  
132 magnitude only. An updated forecast will be made via the inversion method when  
133 tsunameter is available.

134  
135 Titov *et al.* (1999; 2001) conducted sensitivity studies on far-field deep-water  
136 tsunamis with different parameters of an elastic deformation model described in  
137 Gusiakov (1978) and Okada (1985). The results showed source magnitude and location  
138 essentially define far-field tsunami signals for a wide range of subduction zone  
139 earthquakes. Other parameters have a secondary influence and can be pre-defined during  
140 the forecast. Based on these results, tsunami source function databases for the Pacific,  
141 Atlantic, and Indian Oceans have been built using these pre-defined source parameters:  
142 length = 100 km, width = 50 km, slip = 1 m, rake = 90 or -90 and rigidity =  $4.5 \times 10^{10}$   
143  $\text{N/m}^2$ . The other parameters (strike, dip, and depth) are location-specific and are chosen  
144 with knowledge of the subduction zone where they are located. Details of the propagation  
145 database are described in Gica *et al.* (2008). Each tsunami source function models a  
146 tsunami generated by a typical magnitude-7.5 earthquake with predefined source  
147 parameters mentioned above. Figure 1 shows the locations of tsunami source functions.  
148 Figure 2 shows the maximum amplitudes at Virginia Beach offshore from the tsunami  
149 source functions in Atlantic Ocean.

150  
151 The tsunami source functions in the database are computed with a time step of 10  
152 seconds and a spatial resolution of 4-arc-minute (approximately 7.4 km along the north-  
153 south direction). The output (offshore wave height and depth-average velocities of the  
154 entire domain) are then compressed and saved every 1 minute in time and 16-arc-minute  
155 in space (Tolkova, 2007). As inundation is calculated by the high resolution forecast  
156 models, the propagation scenarios do not include inundation, and a reflection boundary  
157 condition is enforced at 20 m water depth (Gica *et al.*, 2008), and friction is assumed to  
158 be negligible.

159  
160 When tsunami waves propagate into shallow water, the steady-state assumption  
161 requires no net energy losses or gains. The decrease in transport speed must be  
162 compensated by an increase in energy density in order to maintain a constant energy flux.  
163 The low spatial resolution and simplified boundary conditions of the propagation model  
164 result in inaccuracies in near-shore dynamics. As a consequence, the numerical  
165 dissipation (due to the low spatial resolution) will cause energy decay in the propagation

166 modeling (Tang *et al.*, 2012). Based on the consideration of energy conservation, we  
167 have developed high-resolution, site-specific inundation forecast models built on the  
168 MOST model to more accurately simulate the near shore wave dynamics.

169

170 That percentage of energy released from an earthquake that is transferred into the  
171 water column during tsunami generation is difficult to accurately model using seismic  
172 methods. However, the goal of tsunameter inversion is not to quantify the energy at the  
173 initial stage of tsunami generation. Instead, we try to quantify the amount of wave energy  
174 that propagates outside the source area in the form of surface long gravity waves, which  
175 can be well measured by the tsunameter stations. Since it is this propagating energy that  
176 results in the impacts at the coast, we estimate the tsunami source (the propagation  
177 scenario) by directly measuring the deep ocean tsunami data. Regardless of the details of  
178 earthquake processes for tsunami generation at the initial stage, the inversion can ensure  
179 the propagation scenario gives the best approximation to the tsunami measurements, and  
180 therefore, the best estimation of the total energy transferred to the tsunami waves. The  
181 database can provide offshore forecasts of tsunami amplitudes and all other wave  
182 parameters immediately once the inversion is complete. The tsunami source, constrained  
183 by real-time tsunami measurements, provides an accurate offshore tsunami scenario  
184 without additional time-consuming deep-water model runs.

185

## 186 **2.2 Coastal Predictions by Using High-Resolution Forecast Models in Real-Time.**

187 High-resolution forecast models are designed for the final stage of the evolution of  
188 tsunami waves: coastal runup and inundation. Once the tsunameter-constrained tsunami  
189 source is obtained (as a linear combination of tsunami source functions), the pre-  
190 computed time series of offshore wave height and depth-averaged velocity from the  
191 model propagation scenario are applied as the dynamic boundary conditions for the  
192 forecast models. This saves the simulation time of basin-wide tsunami propagation.  
193 Tsunami inundation and nearshore currents are highly nonlinear processes, therefore a  
194 linear combination would not provide an accurate solution. A high-resolution model is  
195 also required to resolve shorter tsunami wavelengths nearshore with accurate  
196 bathymetric/topographic data. The forecast models are constructed with the Method of  
197 Splitting Tsunami (MOST) model, a finite difference tsunami inundation model based on  
198 the nonlinear shallow-water wave equations (Titov and Synolakis, 1998; Titov and  
199 González, 1997; Synolakis *et al.*, 2008; Titov *et al.*, 2011). Each forecast model contains  
200 three telescoping computational grids with increasing resolution, covering regional,  
201 intermediate and near shore areas. Run-up and inundation are computed at the coastline.  
202 The highest resolution grid includes the population center and coastal water level stations  
203 for forecast verification. The grids are derived from the best available  
204 bathymetric/topographic data at the time of development, and will be updated as new  
205 survey data become available.

206

207 The forecast models are optimized for speed and accuracy. By reducing the  
208 computational areas and grid resolutions, each model is optimized to provide 4-hour  
209 event forecasting results in a maximum of 10 minutes of computational time using

210 a single processor, while still providing enough accuracy for forecasting. To ensure  
211 forecast accuracy at every step of the process, the model output is validated with  
212 historical tsunami records when available and compared to numerical results from the  
213 original full-resolution, and full-extent “reference” inundation model. In order to provide  
214 warning guidance over a long duration during a tsunami event, each forecast model has  
215 been developed to provide simulation output for up to 24 hours (or 30 hours for the  
216 Atlantic sites) from the time of tsunami generation.  
217

## 218 **3 Model Development**

### 219 **3.1 Forecast area**

220 Virginia Beach is a coastal city in the mid-Atlantic region in the southeastern corner  
221 of Virginia, within the geologic region called the Atlantic Coastal Plain (Tayler *et al.*,  
222 2007). The city is bordered by the Atlantic Ocean to the east and the Chesapeake Bay to  
223 the north (Fig. 4). The Atlantic Coastal Plain features a thick basement layer of igneous  
224 and metamorphic rock overlain with a thick wedge of sediment that increases in thickness  
225 and dips towards the eastern shoreline (Tayler *et al.*, 2007). This sedimentary wedge  
226 consists primarily of eroded clays, sands, and gravel from the Appalachian mountains,  
227 covered with a thin layer of marine sands deposited in a series of sea level changes.  
228 Chesapeake Bay also contains an impact crater estimated to be 35 million years old,  
229 stretching 90 km in diameter (USGS Fact Sheet 049-98). As the plains were uplifted,  
230 numerous peninsulas were incised by stream cutting, with the larger rivers forming tidal  
231 rivers.

232 Virginia Beach's enormous popularity is derived from 28 miles of beach front which,  
233 according to the Guinness Book of Records, is the largest pleasure beach in the world.  
234 The present-day beach extent is shown in Figure 5. Since the late 1920s, the city has  
235 experienced tremendous growth both as a resort and as a center of industry for the East  
236 Coast. Virginia Beach is the largest city in Virginia. Figure 6 shows the population  
237 density for the city, with many high-density tracts right along the coveted beach front  
238 area.

239 The nearest Nation Ocean Service tide gage is the Chesapeake Bay Bridge Tunnel  
240 station (e.g. Allen *et al.*, 2008), which is about 18 km northwest of the warning point for  
241 Virginia Beach. According to the station, the mean range of tide is 0.777m. The mean high  
242 water is used as the reference level for the forecast model to provide a worst case for  
243 inundation forecast.

244 Although no tsunami run-up data were found for Virginia Beach from NGDC's  
245 database, due to its low lying coastal area, high coastal population density and the  
246 potential tsunami hazard from Caribbean Sea subduction zone earthquakes, Virginia  
247 Beach is in need of a forecast model to aid site-specific evacuation decisions.

248

248

249 **3.2 Bathymetry and Topography**

250 In January of 2007, NOAA's National Geophysical Data Center (NGDC)  
251 developed a 1/3" digital elevation model (DEM) covering the Virginia Beach, Virginia  
252 region (Taylor et al., 2007). At the latitude of Virginia Beach, Virginia (36°51' N, 76°00'  
253 W) 1/3 arc-second of latitude is equivalent to 10.27 meters; 1/3 "of longitude is  
254 equivalent to 8.26 meters. The details of this "base" DEM development can be found in  
255 Taylor *et al.* (2007), and an overview is provided here:

256

257 The DEM was generated from diverse digital datasets in the region (sources  
258 shown in Fig. 7) and were designed to represent modern morphology. The digital data  
259 were obtained from several U.S. federal, state and local agencies:

260

261 (1) Bathymetry data include

262

- 263 • NOAA's National Ocean Service (NOS) hydrographic survey data
- 264 • Recent NOS shallow-water multibeam survey data
- 265 • USACE surveys of dredged shipping channels and the Intracoastal  
266 Waterway
- 267 • NGDC-digitized Atlantic Intracoastal Waterway
- 268 • ENC-extracted sounding data

269

270 (2) Topography dataset include:

271

- 272 • City of Virginia Beach 2004 LiDAR data with ~2m spacing
- 273 • USGS 1999 NED 1/3 to 1 arc-second data.

274

275 All dataset were shifted to the World Geodetic System 1984 (WGS84) horizontal  
276 datum and transferred to the MHW vertical datum.

277

278 A grid generation algorithm was used to generate 36 arc-second and 60 arc-  
279 second grids for the high-resolution reference model, covering the East coast of Virginia.  
280 The data consisted largely of the above-referenced 1/3 arc-second Virginia Beach DEM,  
281 but outside it's extent, data were also used from the following sources:

282

- 283 • Virginia Beach VA 1/3"
- 284 • Morehead City, NC 1/3 "
- 285 • Ocean City, MD 1/3 "
- 286 • Cape Hatteras 1/3 "
- 287 • Savannah GA 1/3 "
- 288 • Atlantic City NJ 1/3 "
- 289 • Nantucket MA 1/3 "
- 290 • Montauk NY 1/3 "

- 291 • Daytona Beach FL 1/3 "
- 292 • Myrtle Beach SC 1/3 "
- 293 • East Coast 9 "
- 294 • Atlantic Test 1 ' (ETOPO1 from NGDC)

295

296 The bathymetry and topography at Virginia Beach used in the development of this  
297 forecast model was based on the 1/3" DEM provided by the National Geophysical Data  
298 Center. The author considers it to be a good representation of the local  
299 topography/bathymetry. As new digital elevation models become available, the forecast  
300 model will be updated and report updates will be posted at:

301

302 [http://nctr.pmel.noaa.gov/forecast\\_reports/](http://nctr.pmel.noaa.gov/forecast_reports/)

303

### 304 3.3 Model Setup

305 By sub-sampling the DEMs described in section 3.2, two sets of computational  
306 grids were derived for Virginia Beach, a reference inundation model and the optimized  
307 forecast model.

308

309 The reference grids consist of four levels of telescoping grids with increasing  
310 resolution (Fig. 8). The A-grid covers the coast of Virginia in 36 arc-second. The B-grid  
311 covers Virginia Beach City, Chesapeake Bay and Pamlico Sound in 12 arc-second  
312 resolution, and run-up and inundation simulations are computed at the coastline in C grid  
313 with full 1/3 arc-second resolution.

314

315 To improve the computational speed for operational use, the forecast model needs  
316 to reduce the number of grid nodes, while still accurately capturing model dynamics. The  
317 Virginia Beach forecast model has three levels of telescoping grids (Fig. 9). Due to the  
318 shallow, wide continental shelf offshore, a 60 arc-second resolution was necessary for  
319 the forecast A-grid, to propagate the wave from the propagation database (16 arc-second)  
320 to the forecast site. An 18 arc-second resolution was used for the forecast B-grid, and  
321 run-up and inundation simulations are computed at the coastline in C-grid at 2 arc-second  
322 resolution. Figure 8c shows the Virginia Beach warning point at 284.0286°E , 6.8530°N  
323 in 6.0 m of water depth.

324

325 Grid details at each level and input parameters are summarized in Table 3. As will  
326 be discussed in Section 4.1, a small friction coefficient is chosen due to the shallow  
327 continental shelf of U.S. East Coast. Reflection boundary conditions imposed at different  
328 water depth of 0.5-10m were tested. We have noticed that even with 0.5 m, waves could  
329 not propagate into some shallow areas in A- and B- grids. Due to the small friction  
330 coefficient, a slightly deep offshore water depth of 5 m is chosen here to make the models  
331 stable for all tested scenarios. Therefore, reflection boundary conditions were imposed at  
332 5 meter water depth for the A- and B- grids

333

334 All model runs were tested on a DELL PowerEdge R510 computer equipped with  
335 two Xeon E5670 processors at 2.93 Ghz, each with 12 MBytes of cache and 32GB  
336 memory. The processors are hex core and support hyperthreading, resulting in the  
337 computer performing as a 24 processor machine. Additionally, the testing computer  
338 supports 10 Gigabit Ethernet for fast network connections. This computer configuration  
339 is similar or the same as the configurations of the computers installed at the Tsunami  
340 Warning Centers so the compute times should only vary slightly. For a 4-hour event  
341 simulation, it takes eight processors 2 hours for the reference model while it takes only  
342 ~8 minutes on a single processor for the forecast model.

343

344

345

## 346 4 Results and Discussion

### 347 4.1 Sensitivity of modeled amplitude to friction coefficients

348

349 Accurate simulation of tsunami induced current, run-up and inundation requires  
350 high-resolution bathymetry and topography data in the run-up area and good tsunami  
351 source and model parameters. Titov *et al.* (2005) have shown that, under these conditions,  
352 the MOST run-up and inundation agree quite well with the stereo aerial photo data and  
353 field survey data on Okushiri Island by the 12 July 1993 Hokkaido-Nansei-Oki Mw 7.8  
354 earthquake. Wei *et al.* (2012) have also shown excellent agreement between the modeled  
355 near-field run-up and inundation and the survey data for the March 11, 2011 Japan  
356 tsunami.

357

358 At present, one major difficulty is the lack of high quality inundation/run-up and  
359 current measurements to verify the accuracy of topography and to calibrate the friction  
360 coefficient. Modeling work in similar near-shore geometry has suggested that lowering  
361 the friction coefficient for areas with beach slope shallower than 1:50 can have a marked  
362 affect on inundation. In this section, we focus on the sensitivity of modeled amplitude at  
363 Virginia Beach to the friction coefficient.

364

365 Figure 11 shows different Manning roughness coefficients ( $n$ ) can affect the  
366 tsunami amplitude and inundations significantly at Virginia Beach for a Puerto Rico  
367 magnitude-9.3 tsunami. The testes are done using a set of testing grids with resolutions of  
368 120, 18 and 3 arc-second for the A- B and C grids respectively. The Manning roughness  
369 coefficient ( $n$ ) ranges from 0-0.04. The roughness coefficient can affect results not only  
370 within C-grid, but also the amplitudes in the B-grid, and those over the shallow  
371 continental shelf (depth less than 100-200m) in the A-grid.

372

373 The above results indicate friction does influence the results, and it is very  
374 difficult to provide the friction coefficient that is reasonable, since there are actually

375 many factors involved -- not only the roughness itself, but the approximation inherent in  
 376 the shear stress of the flow, turbulent parameterization, and numerical dissipation  
 377 approximation. The Manning formula used in the MOST model is an engineering  
 378 empirical “roughness” estimation only. Using any specific number is not really validated  
 379 in any way for tsunamis and the choice of a specific coefficient for a specific site is fairly  
 380 arbitrary. The goal is to account for friction that we know exists, and to improve the  
 381 stability of the runs for a particular site. The best way to validate the friction is with  
 382 observation data, but such data is rarely available for east coast sites, especially for  
 383 inundation. For our application, we want to be conservative in choosing the coefficient.

384

385 So for Virginia Beach, with beach slopes sometimes approaching 1:75, we use the  
 386 smallest possible friction value that produces consistent stable computations:  $n=0.01$ . It  
 387 should be noted for MOST version 4,  $n$  can be set to different values for different grids.  
 388 For example we can set  $n=0$  for the A- and B-grids, while a relatively larger  $n$  can be  
 389 chosen for C-grid to stabilize the model for large run-up/run-down. Model locations with  
 390 steeper beach profiles and deeper shelf depths may be best run with  $n$  set to the more  
 391 common west-coast value of  $n=0.025-0.03$ .

392

## 393 4.2 Model verification and stability testing

394

395 Figure 2 shows the maximum amplitude offshore at Virginia Beach from the  
 396 propagation database. The Puerto Rico trench can easily be identified as the most  
 397 hazardous tsunami-generating area for Virginia Beach, with large offshore amplitudes  
 398 and fast arrivals. A set of nine simulated magnitude-9.3 tsunamis was selected here for  
 399 further examination (Table 3). Each simulated earthquake involves 20 tsunami source  
 400 functions (10 pairs) and a uniform 25-m coefficient. Both the Virginia Beach reference  
 401 and forecast models were tested with the nine scenarios.

402

403 Figure 12 show the amplitude ( $\eta$ ) time series at the Virginia Beach warning point for  
 404 the simulated magnitude-9.3 tsunamis. Table 3 summarize the  $\eta_{\max}$  and uncertainty due  
 405 to different model setup. The uncertainty are computed as:

406

$$407 \text{ uncertainty} = \frac{|\eta_{\max 2} - \eta_{\max 1}|}{\eta_{\max 1}} \times 100$$

408

409 where  $\eta_{\max 1}$  and  $\eta_{\max 2}$  are the maximum water surface elevation computed by the  
 410 reference and forecast models respectively.

411

412 Based on the nine scenarios, the uncertainty in  $\eta_{\max}$  at the Virginia Beach warning  
 413 point computed by the forecast model is within 22%. The largest error of 1.07 m in  $\eta_{\max}$   
 414 among the tested tsunamis occurs in the 5th, Puerto Rico scenario, where  $\eta_1 = 4.94$  m  
 415 and  $\eta_{\max 2} = 6.01$  m, 22% overestimated (Fig. 12.5). The arrival time of the maximum  
 416 amplitudes can be 10-30 hours after the first wave. The forecast model was tested by

417 running the model up to 30 hours after the earthquake to ensure capturing the maximum  
418 in the run.

419

420 Figure 13 shows the model is also stable for a micro tsunami (about 0.22mm in  
421 amplitude) generated by a magnitude-6.8 earthquake in the distant South Sandwich  
422 Islands subduction zone. Accurate forecasting of small tsunamis gives forecasters the  
423 confidence to issue an all-clear for small events.

424

425 Wavelet analyses were performed for the scenarios to explore peak resonant periods,  
426  $T_p$ , at the Virginia Beach warning point. Figures 14 show the amplitude spectrograms.  
427 The site shows relatively long and broad resonant periods from 0.5 to 4.5 hours (Fig. 15b).

428

429 Figure 16 shows both the reference and forecast models produced similar maximum  
430 water elevation, maximum current and inundation limit in the study area. Large  
431 maximum currents can be seen in both the reference and forecast models for many of the  
432 scenarios, especially over the shallow areas.

433

434 Tsunami waves in the study area vary significantly for the 9 magnitude-9.3 scenarios.  
435 The 5th Puerto Rico scenario produces waves with amplitudes over 6 meters at the  
436 Virginia Beach warning point. The inundation and run-up for these aphysical synthetic  
437 test sources can be significant, but model shows stable characteristics even for these large  
438 amplitude overland flows. The 4th Dominica scenario generated wave amplitudes of over  
439 2 meters at Virginia Beach. These results show the complexity and high nonlinearity of  
440 tsunami waves nearshore, which again demonstrate the value of high-resolution forecast  
441 model for providing accurate site-specific forecast details.

442

443

## 444 **5 Summary and Conclusions**

445 A tsunami forecast model was developed for Virginia Beach, Virginia. The  
446 computational grids for the Virginia Beach forecast model were derived from the best  
447 available bathymetric and topographic data sources. The forecast model is optimally  
448 constructed at 2 arc-second resolution, to enable a 4 hour inundation simulation within ~8  
449 minutes of computational time using a single processor. A reference inundation model of  
450 higher resolution of 1/3 arc-second was also developed in parallel, to provide a modeling  
451 reference for the forecast model. Both models were tested for a set of nine simulated  
452 magnitude-9.3 tsunamis. One point at the Virginia Beach, 284.0286°E , 6.8530°N in 6.0  
453 meters of water depth, was chosen as the warning point for the site.

454

455 The modeled amplitude, inundation and current are sensitive to the friction coefficient.  
456 Due to the lack of data for calibration and to be on the conservative side, we use the  
457 smallest possible friction value,  $n=0.01$ , that produces consistent stable computations for  
458 both models.

459

460 Based on the nine tested scenarios, the uncertainty in  $\eta_{\max}$  due to grid setup at the  
461 Virginia Beach warning point computed by the forecast model is within 22%. The  
462 modeled inundation limits and currents agree reasonably well between the forecast and  
463 reference models. Wavelet analyses show broad and relatively long resonant periods from  
464 0.5 to several hours for the site.

465

466 Mega-tsunamis from the Puerto Rico subduction zone can cause appreciable  
467 inundation at the site. The results also highlight the fact that, due to the broad continental  
468 shelf on the east coast, the maximum wave can arrive 12-30 hours after the first wave,  
469 requiring longer warning duration for such events. The simulated magnitude-9.3 tsunamis  
470 show an impressive local variability of tsunami amplitudes at Virginia Beach, and  
471 indicate the complexity of forecasting tsunami amplitudes at this coastal location. It is  
472 essential to use high-resolution models in order to provide enough accuracy to be useful  
473 for coastal tsunami forecasts and practical guidance.

474

475

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481

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488

488

489 **References**

- 490 Allen, A.L., N.A. Donoho, S.A. Duncan, S.K. Gill, C.R. McGrath, R. S. Meyer, M. R.  
491 Samant (2008), NOAA's National Ocean Service Supports Tsunami Detection and  
492 Warning through Operation of Coastal Tide Stations, In: Solutions to Coastal  
493 Disasters 2008 /Tsunamis/: Proceedings of Sessions of the Conference, April 13-  
494 16, 2008 Turtle Bay, Oahu, Hawaii. American Society of Civil Engineers.
- 495 Arcas, D., and B. Uslu (2010): A Tsunami Forecast Model for Crescent City, California.  
496 NOAA OAR Special Report, PMEL Tsunami Forecast Series: Vol. 2, 112 pp, Gov.  
497 Print. Off., Seattle, Wash.
- 498 Bernard, E.N., H.O. Mofjeld, V.V. Titov, C.E. Synolakis, and F.I. González (2006):  
499 Tsunami: Scientific frontiers, mitigation, forecasting, and policy implications.  
500 Proc. Roy. Soc. Lon. A, 364(1845), doi: 10.1098/rsta.2006.1809, 1989–2007.
- 501 Bernard, E., and V.V. Titov (2007): Improving tsunami forecast skill using deep ocean  
502 observations, Mar. Technol. Soc. J., 40(3), 23–26.
- 503 Gica E., Spillane, M.C., Titov, V.V., Chamberlin, C.D. and Newman, J.C. (2008):  
504 Development of the forecast propagation database for NOAA's Short-Term  
505 Inundation Forecast for Tsunamis (SIFT). NOAA Tech. Memo. OAR PMEL-139,  
506 89pp.
- 507 Gusiakov, V.K. (1978): Static displacement on the surface of an elastic space. Ill-posed  
508 problems of mathematical physics and interpretation of geophysical data,  
509 Novosibirsk, VC SOAN SSSR, 23–51 (in Russian).
- 510 Gonzalez, F.I., E.N. Bernard, C. Meinig, M. Eble, H.O. Mofjeld, and S. Stalin (2005):  
511 The NTHMP tsunameter network. *Nat. Hazards*, 35(1), Special Issue, U.S.  
512 National Tsunami Hazard Mitigation Program, 25-39.
- 513 Liu, P. L.-F. (2009): Tsunami modeling—Propagation, in *The Sea*, vol. 15, edited by E.  
514 Bernard and A. Robinson, chap. 9, pp. 295– 319, Harvard Univ. Press, Cambridge,  
515 Mass.
- 516 Meinig, C., S.E. Stalin, A.I. Nakamura, F. González, and H.G. Milburn (2005):  
517 Technology Developments in Real-Time Tsunami Measuring, Monitoring and  
518 Forecasting. In *Oceans 2005 MTS/IEEE*, 19–23 September 2005, Virginia, D.C.
- 519 National Geophysical Data Center, Global Tsunami Database (2000 BC to present):  
520 [http://www.ngdc.noaa.gov/seg/hazard/tsu\\_db.shtml](http://www.ngdc.noaa.gov/seg/hazard/tsu_db.shtml)

- 521 Okada, Y., 1985, Surface deformation due to shear and tensile faults in a half-space. *Bull.*  
522 *Seismol. Soc. Am.*, 75, 1135-1154.
- 523 Percival, D.B., D.W. Denbo, M.C. Eble, E. Gica, H.O. Mofjeld, M.C. Spillane, L. Tang,  
524 and V.V. Titov (2011): Extraction of tsunami source coefficients via inversion of  
525 DART® buoy data. *Nat. Hazards*, 58(1), doi: 10.1007/s11069-010-9688-1, 567–  
526 590.
- 527 Satake, K., Y. Hasegawa, Y. Nishimae and Y. Igarashi (2008), Recent Tsunamis That  
528 Affected the Japanese Coasts and Evaluation of JMA's Tsunami Warnings.  
529 OS42B-03, AGU Fall Meeting, San Francisco.
- 530 Spillane, M.C., E. Gica, V.V. Titov, and H.O. Mofjeld (2008): Tsunameter network  
531 design for the U.S. DART® arrays in the Pacific and Atlantic Oceans, Tech.  
532 Memo, OAR PMEL-143, 165pp., Gov. Print. Off., Seattle, Wash.
- 533 Synolakis, C.E., E.N. Bernard, V.V. Titov, U. Kânoğlu, and F.I. González (2008):  
534 Validation and verification of tsunami numerical models. *Pure Appl. Geophys.*,  
535 165(11–12), 2197–2228.
- 536 Tang, L., C. Chamberlin, E. Tolkova, M. Spillane, V.V. Titov, E.N. Bernard, and H.O.  
537 Mofjeld (2006): Assessment of potential tsunami impact for Pearl Harbor, Hawaii.  
538 NOAA Tech. Memo. OAR PMEL-131.
- 539 Tang, L., C. Chamberlin and V.V. Titov, (2008a): Developing tsunami forecast  
540 inundation models for Hawaii: procedures and testing, *NOAA Tech. Memo., OAR*  
541 *PMEL -141*, 46 pp.
- 542 Tang, L., V.V. Titov, Y. Wei, H.O. Mofjeld, M. Spillane, D. Arcas, E.N. Bernard, C.  
543 Chamberlin, E. Gica, and J. Newman (2008b): Tsunami forecast analysis for the  
544 May 2006 Tonga tsunami. *J. Geophys. Res.*, 113, C12015, doi:  
545 10.1029/2008JC004922.
- 546 Tang, L., V. V. Titov, and C. D. Chamberlin (2009): Development, Testing, and  
547 Applications of Site-specific Tsunami Inundation Models for Real-time  
548 Forecasting. *J. Geophys. Res.*, 114, C12025, doi:10.1029/2009JC005476..
- 549 Tang, L., V.V. Titov and C.D. Chamberlin (2010): A Tsunami Forecast Model for Hilo,  
550 Hawaii. NOAA OAR Special Report, PMEL Tsunami Forecast Series: Vol. 1, 44  
551 pp.
- 552 Tang, L., V. V. Titov, E. Bernard, Y. Wei, C. Chamberlin, J. C. Newman, H. Mofjeld, D.  
553 Arcas, M. Eble, C. Moore, B. Uslu, C. Pells, M. C. Spillane, L. M. Wright, and E.  
554 Gica (2012): Direct energy estimation of the 2011 Japan tsunami using deep-ocean  
555 pressure measurements. *J. Geophys. Res.*, 117, C08008,  
556 doi:10.1029/2011JC007635.

- 557 Taylor, L.A., B.W. Eakins, K.S. Carignan, R.R. Warnken, T. Sazonova, D.C.  
558 Schoolcraft, and G.F. Sharman (2007): Digital Elevation Model for Virginia Beach,  
559 Virginia: Procedures, Data Sources and Analysis, NOAA, National Geophysical  
560 Data Center, Boulder, Colorado
- 561 Titov, V. V., C. W. Moore, D. J. M. Greenslade, C. Pattiaratchi, R. Badal, C. E.  
562 Synolakis, and U. Kânoğlu (2011): A new tool for inundation modeling:  
563 Community Modeling Interface for Tsunamis (ComMIT). *Pure Appl. Geophys.*,  
564 168, 2121–2131, doi:10.1007/s00024-011-0292-4.
- 565 Titov, V. V., and L. Tang (2011): Estimating tsunami magnitude in real time  
566 using tsunami data, paper presented at XXV IUGG General Assembly,  
567 Melbourne, Victoria, Australia, 28 Jun to 7 Jul.
- 568 Titov, V.V. (2009): Tsunami forecasting. Chapter 12 in *The Sea, Volume 15: Tsunamis*,  
569 Harvard University Press, Cambridge, MA and London, England, 371–400.
- 570 Titov, V.V., F.I. González, E.N. Bernard, M.C. Eble, H.O. Mofjeld, J.C. Newman, and  
571 A.J. Venturato (2005): Real-time tsunami forecasting: Challenges and solutions.  
572 *Natural Hazards*, 35(1), Special Issue, U.S. National Tsunami Hazard Mitigation  
573 Program, 41–58.
- 574 Titov, V. V., Mofjeld, H. O., González, F. I., and Newman, J. C.: 2001, Offshore  
575 forecasting of Virginian tsunamis in Hawaii. In: G. T. Hebenstreit (ed.), *Tsunami  
576 Research at the End of a Critical Decade*. Birmingham, England, Kluwer Acad.  
577 Pub., Netherlands, pp. 75–90.
- 578 Titov, V.V., H.O. Mofjeld, F.I. Gonzalez and J.C. Newman (1999): Offshore forecasting  
579 of Virginia-Aleutian subduction zone tsunamis in Hawaii. NOAA Technical  
580 Memorandum. ERL PMEL-114, January 1999, 22 pp.
- 581 Titov, V.V. and C.S. Synolakis (1998): Numerical modeling of tidal wave runup. *Journal  
582 of Waterway, Port, Coastal and Ocean Engineering*, ASCE, 124(4), 157-171.
- 583 Titov, V.V. and F.I. Gonzalez (1997): Implementation and testing of the Method of  
584 Splitting Tsunami (MOST) model. NOAA Technical Memorandum. NOAA  
585 Pacific Marine Environmental Laboratory, ERL PMEL-112, Nov. 1997, 11 pp.
- 586 Tolkova, E. (2007): Compression of MOST Propagation Database. NOAA Tech. Memo.  
587 OAR PMEL-134, NTIS: PB2007-108218, 9 pp., Gov. Print. Off., Seattle, Wash.
- 588 USGS Fact Sheet 049-98, The Chesapeake Bay Bolide Impact: A New View of Coastal  
589 Plain Evolution, <http://pubs.usgs.gov/fs/fs49-98/index.html>.
- 590 Wei, Y., E. Bernard, L. Tang, R. Weiss, V. Titov, C. Moore, M. Spillane, M. Hopkins,  
591 and U. Kânoğlu (2008): Real-time experimental forecast of the Peruvian tsunami  
592 of August 2007 for U.S. coastlines. *Geophys. Res. Lett.*, 35, L04609, doi:  
593 10.1029/2007GL032250.

- 594 Wei, Y., and D. Arcas (2010): A tsunami forecast model for Kodiak, Alaska. NOAA  
595 OAR Spec. Rep./PMEL Tsunami Forecast Ser. 4, 96 pp., Gov. Print. Off., Seattle,  
596 Wash.
- 597 Wei, Y., C. Chamberlin, V.V. Titov, L. Tang, and E.N. Bernard (2012): Modeling of  
598 2011 Japan Tsunami - lessons for near-field forecast. *Pure Appl. Geophys.*, doi:  
599 10.1007/s00024-012-0519-z.
- 600 Whitmore, P.M. (2003): Tsunami amplitude prediction during events: A test based on  
601 previous tsunamis. In *Science of Tsunami Hazards*, 21, 135–143

## Tables

**Table 1** Tsunami source functions in the Pacific, Atlantic and Indian Oceans.

Source Zone			Tsunami source functions		Run time
No.	Abbr.	Name	Line/zone	Numbers	(hour)
1	ACSZ	Aleutian-Alaska-Canada-Cascadia	BAZYXW	184	24
2	CSSZ	Central-South American	BAZYX	382	30
3	EPSZ	East Philippines	BA	44	30
4	KISZ	Kamchatka-Kuril-Japan Trench-Izu Bonin-Marianas-Yap	BAZYXW	229	24
5	MOSZ	Manus Ocean Convergence Boundary	BA	34	24
6	NVSZ	New Britain-Solomons-Vanuatu	BA	74	24
7	NGSZ	North New Guinea	BA	30	30
8	NTSZ	New Zealand-Kermadec-Tonga	BA	81	24
9	NZSZ	South New Zealand	BA	14	30
10	RNSZ	New Ryukus-Kyushu-Nankai	BA	44	24
11	KBSZ	Kamchatskii-Bering Source Zone	BAZ	13	24
Subtotal:				<b>1129</b>	
12	ATSZ	Atlantic	BA	214	36
13	SSSZ	South Sandwich	BAZ	33	36
Subtotal:				<b>247</b>	
14	IOSZ	Adaman-Nicobar-Sumatra-Java	BAZY	307	24
15	MKSZ	Makran	BA	20	24
16	WPSZ	West Philippines	BA	22	24
Subtotal:				<b>349</b>	
Total:				<b>1725</b>	

**Table 2** MOST setups for the Virginia Beach reference and forecast models.

Grid	Region	Reference Model			Forecast model		
		Coverage Lon. (°E) Lat. (°N)	Cell Size (")	Time Step (sec)	Coverage Lon. (°E) Lat. (°N)	Cell Size (")	Time Step (sec)
A	Virginia	281.9241-289.6941	36 (778x886)	3.5	281.9224- 289.7057	60 (468x521)	5.2
		32.5007-41.3507			32.6774-41.344		
B	Virginia	282.8707-285.6541	12 (836x1466)	1.5	283.5391- 284.7141	18 (236x367)	5.2
		34.764-39.6474			36.1024-37.9324		
C	Virginia	283.9953-284.0796	1/3 (911x1441)	0.4	283.9686- 284.0791	2 (200x354)	2.6
	Beach	36.8143-36.9476			59.5064-59.6647		
Minimum offshore depth (m)			5		5		
Water depth for dry land (m)			0.1		0.1		
Friction coefficient (n <sup>2</sup> )			0.0001		0.0001		
Computational time for a 4-hr simulation			~ 2 hours using 8 processors		7.86 min using 1 processor		

**Table 3** Sources of the 9 simulated magnitude-9.3 tsunamis and the maximum computed wave crests at the Virginia Beach warning point.

No.	Subd. Zone	Source	alpha	Ref. model		Forecast Model		Error		Location
				etamax (m)	tmax (hour)	etamax (m)	tmax (hour)	(m)	(%)	
1	atsz AB	1-	10 25	0.45	15.774	0.45	31.487	-0.00	0	Panama
2	atsz AB	12-	21 25	0.53	16.641	0.49	16.680	-0.05	-9	Colombia
3	atsz AB	22-	31 25	0.96	17.801	0.86	17.805	-0.09	-10	Venezuela
4	atsz AB	38-	47 25	2.52	4.753	2.47	5.277	-0.05	-2	Dominica
5	atsz AB	48-	57 25	4.94	4.473	6.01	4.429	1.07	22	Puerto Rico
6	atsz AB	58-	67 25	1.06	4.663	1.09	4.704	0.03	3	Cayman
7	atsz AB	68-	77 25	0.23	26.085	0.23	26.002	0.01	0	Gulf of Honduras
8	atsz AB	82-	91 25	1.33	5.060	1.38	5.095	0.04	3	U.S. Virgin Is.
9	sssz AB	1-	10 25	0.63	28.460	0.58	28.471	-0.05	-7	South Sandwich Is.

## Appendix A.

Since the initial development of the forecast model for Virginia Beach, Virginia, the parameters for the input file for running the forecast and reference models have been changed to reflect changes to the MOST model code. The following appendix lists the new input files for Virginia Beach.

### A1. Reference model \*.in file for Virginia Beach, Virginia—updated for 2013

```
# ----- MOST Run 1 -----
# 0. Preparations
echo '#-----#'
echo '#          Preprocess MOST input          #'
echo '#-----#'
set main_dir="/home/tg23/data/tang/sims/virginiabeach/"
set np="8"
setenv OMP_NUM_THREADS $np
set path_w="$main_dir/virgv4_S03_at_ab22T31rb2_c1_05m_fp01_19h/"

set path_e="most4"
set path_src="/grid/tg23/data/tang/src_nc/src_sim_test/virg/S03_at_ab22T31_virg_"

if ( -d $path_w ) then
echo $path_w 'exist'
  cd $path_w
else
  echo Creating directory $path_w
  mkdir $path_w
  cd $path_w
endif
ln -sf /home/tg23/data/tang/bathy/virginiabeach/virg_rb2//*.nc .
# -----
# 1. Generate INPUT for MOST
# ~~~~~
# ~~~~~A~~~~~
cat > most3_facts_nc.inA<< EOF
0.005  Minimum amplitude of input offshore wave (m):
5      Input minimum depth for offshore (m)
0.1    Input "dry land" depth for inundation (m)
0.0001 Input friction coefficient (n**2)
2      Number of grids
2      Interpolation domain for outer boundary
2      inner boundary
RA_VirginiaBeach_36ss_20130211.nc
RB_VirginiaBeach_12s_20130211.nc
1      Runup flag
```

```

3.5  Input time step (sec)
19543 Input amount of steps
0      COntunue after input stops
9  Input number of steps between snapshots
1  saving inner boundaries every n-th timestep
1  ...Saving grid every n-th node, n=
0  1=initial deformation
EOF
cp most3_facts_nc.inA most3_facts_nc.in
#$path_e A $path_src most3_facts_nc.in
# ~~~~~
# ~~~~~B~~~~~
cat > most3_facts_nc.inB<< EOF
0.005  Minimum amplitude of input offshore wave (m):
5      Input minimum depth for offshore (m)
0.1    Input "dry land" depth for inundation (m)
0.0001 Input friction coefficient (n**2)
2      Number of grids
2      Interpolation domain for outer boundary
2      inner boundary
RB_VirginiaBeach_12s_20130211.nc
RC_Virginia_Beach_1_3s_c2_NGDC.nc
1      Runup flag
1.5    Input time step (sec)
45600  Input amount of steps
0      COntunue after input stops
20     Input number of steps between snapshots
1      saving inner boundaries every n-th timestep
1      ...Saving grid every n-th node, n=
0      1=initial deformation
EOF
cp most3_facts_nc.inB most3_facts_nc.in
$path_e B A most3_facts_nc.in
# ~~~~~
# ~~~~~C~~~~~
cat > most3_facts_nc.inC<< EOF
0.005  Minimum amplitude of input offshore wave (m):
-300   Input minimum depth for offshore (m)
0.1    Input "dry land" depth for inundation (m)
0.0001 Input friction coefficient (n**2)
1      Number of grids
2      Interpolation domain for outer boundary
2      inner boundary
RC_Virginia_Beach_1_3s_c2_NGDC.nc
2      Runup flag
0.38   Input time step (sec)
180000 Input amount of steps
0      COntunue after input stops
79     Input number of steps between snapshots
1      saving inner boundaries every n-th timestep
1      ...Saving grid every n-th node, n=
0      1=initial deformation
EOF
cp most3_facts_nc.inC most3_facts_nc.in
$path_e C B most3_facts_nc.in

```

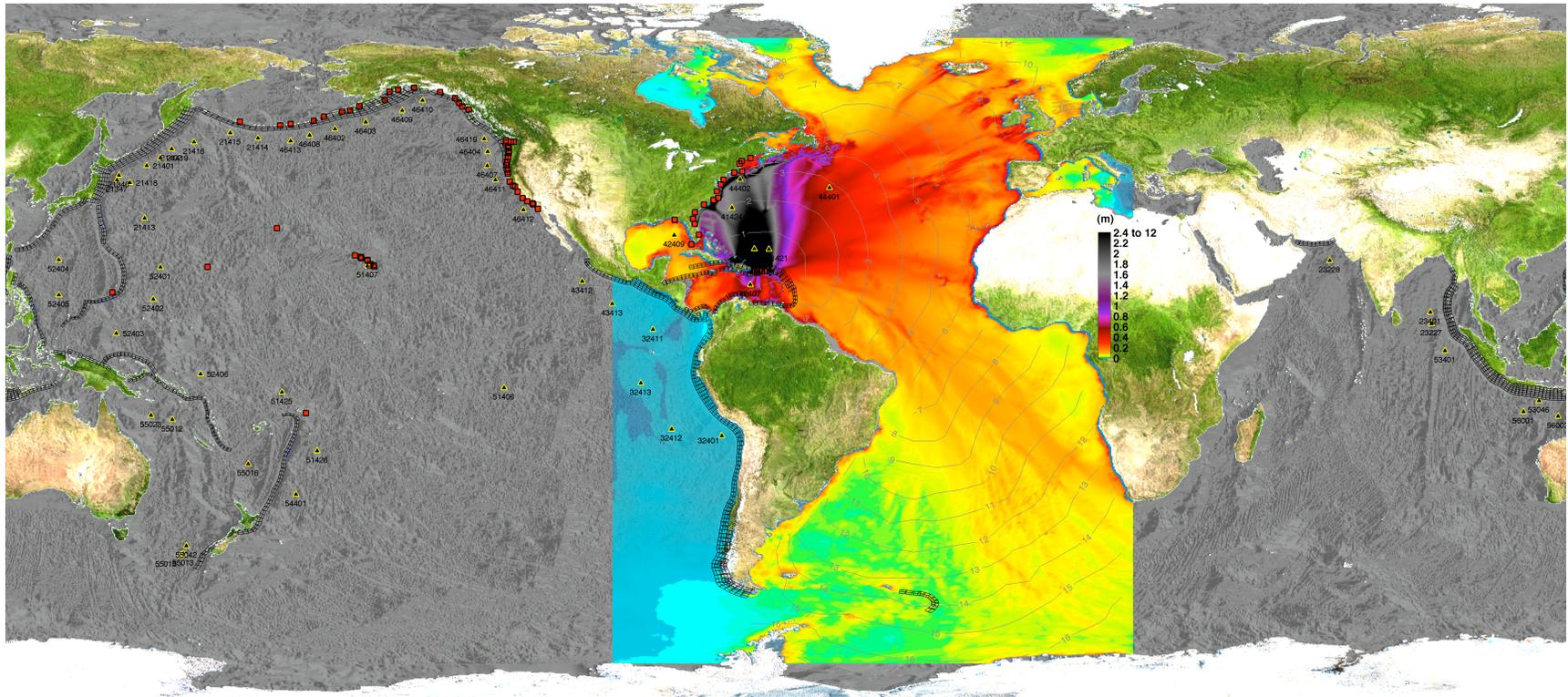
**A2. Forecast model \*.in file for Virginia Beach, Virginia—updated for 2013**

```
0.0001      Minimum amplitude of input offshore wave (m):
5           Input minimum depth for offshore (m)
0.1        Input "dry land" depth for inundation (m)
0.0001     Input friction coefficient (n**2)
1          runup flag for grids A and B (1=yes,0=no)
300.0     blowup limit
2.6       Input time step (sec)
16615     Input amount of steps
2         Compute "A" arrays every n-th time step, n=
2         Compute "B" arrays every n-th time step, n=
10        Input number of steps between snapshots
0         ...Starting from
1         ...Saving grid every n-th node, n=
FA_Virg_Beach_60s_20130211.ssl
FB_Virg_Beach_18s_20130211.ssl
FC_Virg_Beach_2s_c7_NGDC.ssl
/grid/tg23/data/tang/src_nc/src_sim_test/virg/
./
1 1 1 1    NetCDF output for A, B, C, SIFT
1         Timeseries locations:
3 109 223  Virginia Beach 284.0286E 36.8530N, 6 m depth
```

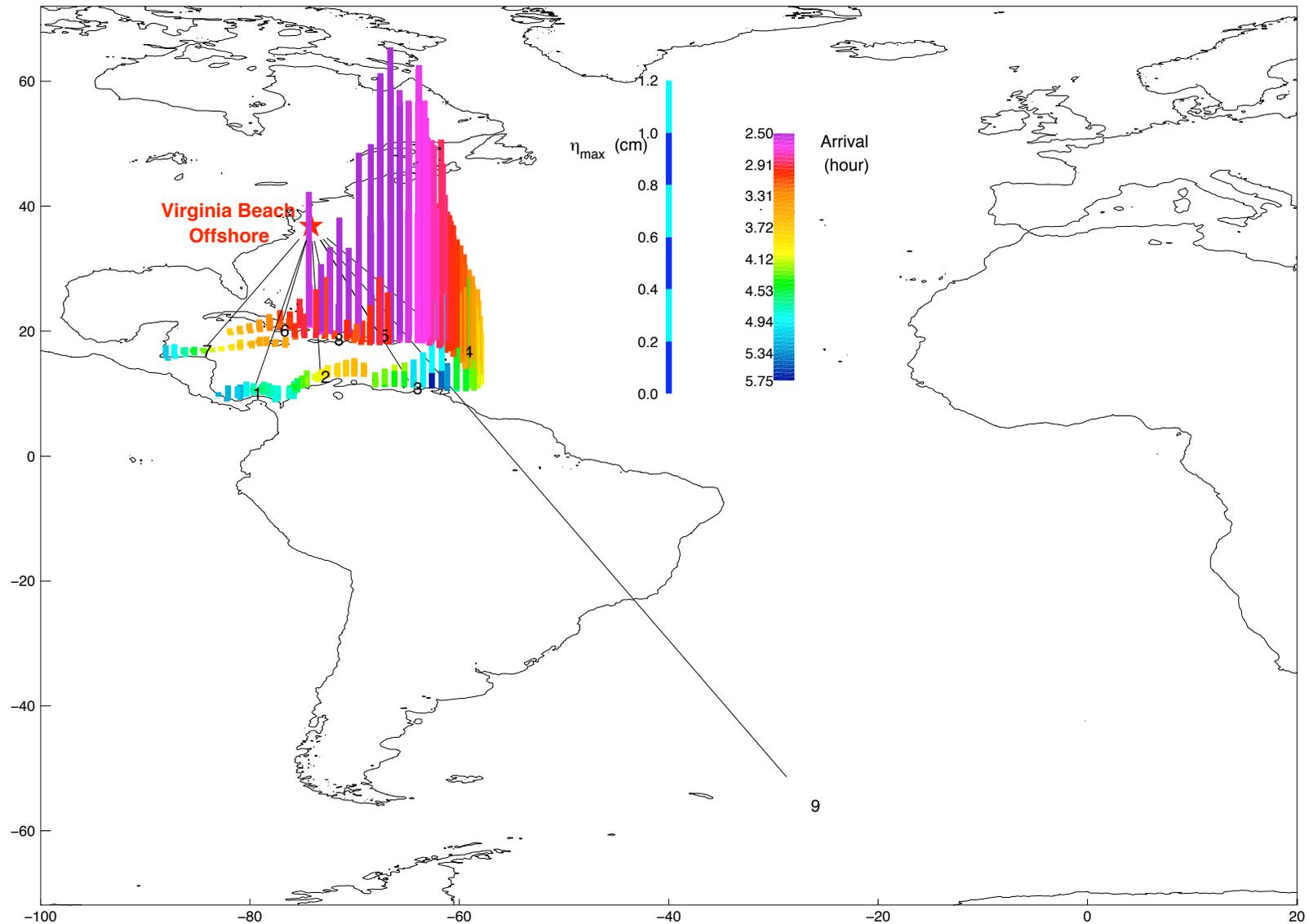
## **Figures**

<b>Figure 1</b> (a) Overview of the tsunami Forecast System. System components include tsunameter (DART) network (yellow triangles), pre-computed tsunami source function (unfilled black rectangles) and high-resolution forecast models (red squares). Filled color shows the computed offshore maximum sea surface elevation in m for a simulated magnitude-9.3 Caribbean tsunami (#5). Contours indicate the travel time in hours. ....	28
<b>Figure 2</b> Maximum sea surface elevation ( $\eta_{max}$ ) offshore Virginia Beach from 214 magnitude-7.5 earthquakes. Data were taken from NCTR's pre-computed propagation database for Atlantic Ocean. Heights and colors of the bars represent $\eta_{max}$ and the first arrival at the offshore point (74.1333°W, 36.9461°N; water depth = 2269 m) respectively. 1-9, locations for nine simulated magnitude-9.3 tsunamis.....	29
<b>Figure 3</b> Historical tsunamis in Atlantic Ocean and Caribbean Sea ( National Geographic Data Center's database).....	30
<b>Figure 4</b> NOAA charts, (a) 13003 and (b) 12208, show Virginia Beach Soundings in fathoms at Mean Lower Low Water. Contour and summit elevation values are in feet above Mean Sea Level.....	32
<b>Figure 4</b> Aerial photos of Virginia Beach.....	34
<b>Figure 6</b> Population density at Virginia Beach (2000 Census).....	35
<b>Figure 7</b> Bathymetric and topographic data source overview for the high-resolution Virginia Beach DEM. Image courtesy of Tayler <i>et al.</i> (2007).....	36
<b>Figure 8</b> Grid setup for the Virginia Beach reference model. Resolutions are (a) 36", (b) 12" and(c) 1/3" . Red boxes are boundaries of the telescoped grids for the reference model. ....	39
<b>Figure 9</b> Grid setup for the Virginia Beach forecast model. Grid resolutions are (a) 60 ", (b) 18", and (c) 2". Red boxes, boundaries of the telescoping grids. Red dot, Virginia Beach warning point (284.0286°E, 36.8530°N; water depth= 6m ). ....	42
<b>Figure 10</b> Sensitivity of $\eta$ to friction coefficients. Results were computed by a set of testing grids (Fig. 11) for a magnitude 9.3 Caribbean tsunami. ....	43
<b>Figure 11</b> Sensitivity of $\eta_{max}$ to friction coefficients. Results were computed by a set of testing grids for a magnitude-9.3 Caribbean tsunami.....	44
<b>Figure 12</b> Modeled $\eta$ time series by the Virginia Beach reference and forecast models for simulated magnitude-9.3 tsunamis.....	46
<b>Figure 13</b> Modeled $\eta$ time series computed by the Virginia Beach forecast model for a simulated micro tsunami. The tsunami was generated from a Magnitude 6.8 earthquake from South Sandwich Islands Subduction (0.1 × B11).....	47

- Figure 14** (a) Modeled  $\eta$  time series at Virginia Beach warning point for the nine simulated magnitude-9.3 tsunamis. (b) Wavelet-derived amplitude spectrogram for the reference model. (c and d) Real part of the spectrograms computed by the reference and forecast models. ....52
- Figure 15** (a) Forecast uncertainty in the  $\eta_{\max}$  at the Virginia Beach warning point. (b) Uncertainty v.s. peak period.  $\eta_{\max 1}$  and  $T_{p1}$ , maximum water elevation and peak period at the warning point from the reference model.  $\eta_{\max 2}$  and  $T_{p2}$ , maximum water surface elevation and peak period at the warning point computed by the forecast model.....53
- Figure 16** Maximum water elevation and current computed by the Virginia Beach reference and forecast models for the simulated magnitude-9.3 tsunamis.....62



**Figure 1** (a) Overview of the tsunami Forecast System. System components include tsunameter (DART) network (yellow triangles), pre-computed tsunami source function (unfilled black rectangles) and high-resolution forecast models (red squares). Filled color shows the computed offshore maximum sea surface elevation in m for a simulated magnitude-9.3 Caribbean tsunami (#5). Contours indicate the travel time in hours.



**Figure 2** Maximum sea surface elevation ( $\eta_{\max}$ ) offshore Virginia Beach from 214 magnitude-7.5 earthquakes. Data were taken from NCTR's pre-computed propagation database for Atlantic Ocean. Heights and colors of the bars represent  $\eta_{\max}$  and the first arrival at the offshore point (74.1333°W, 36.9461°N; water depth = 2269 m) respectively. 1-9, locations for nine simulated magnitude-9.3 tsunamis.

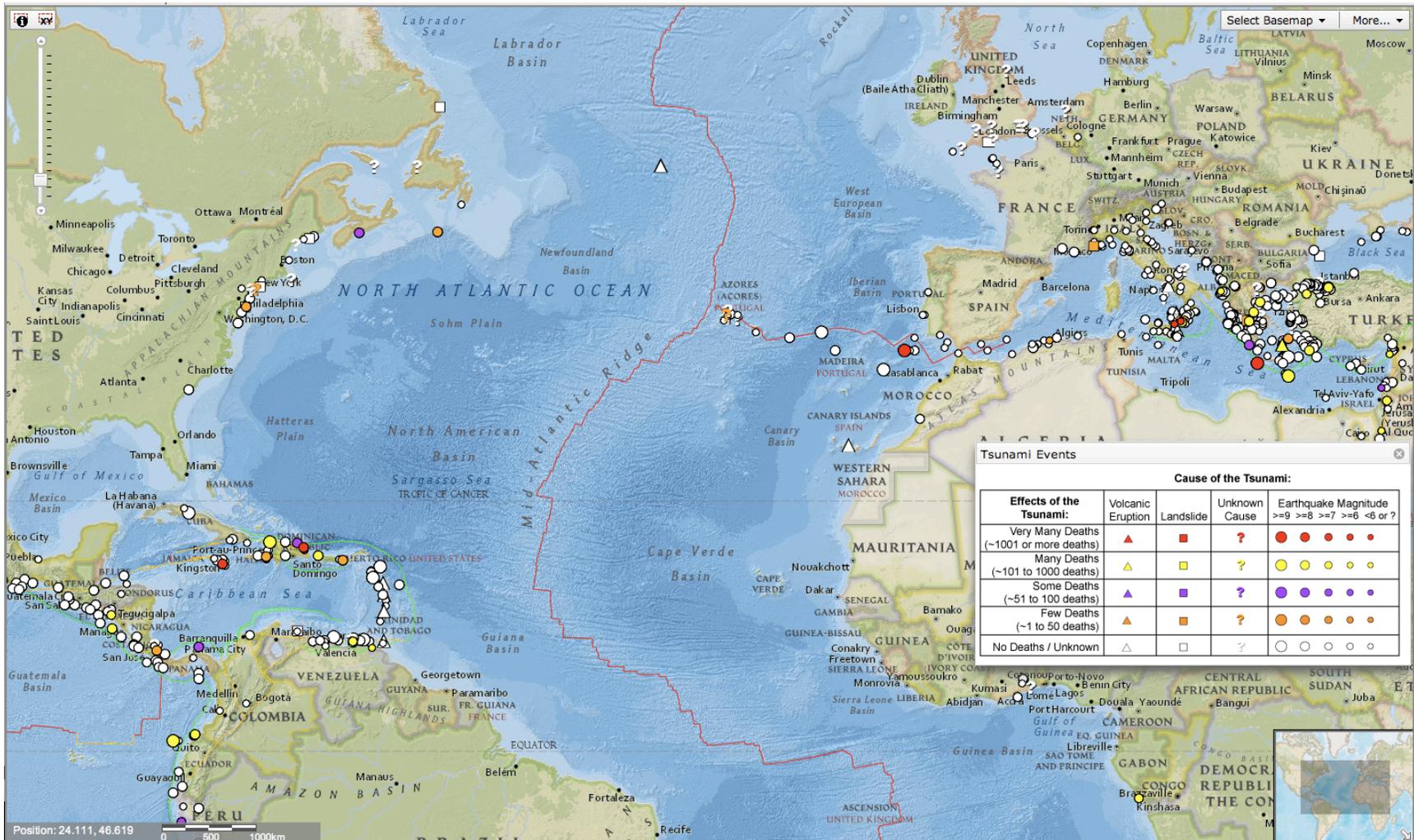
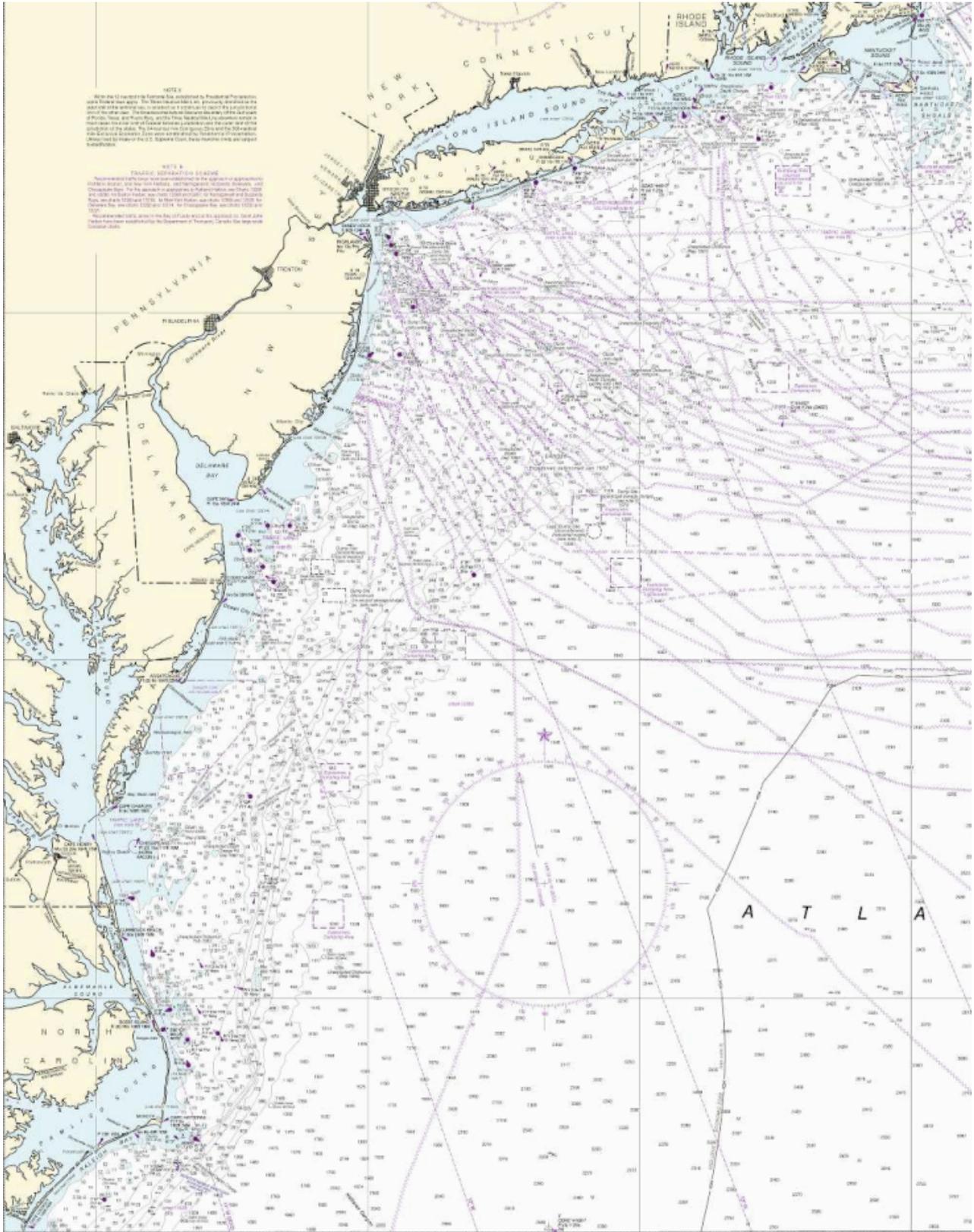
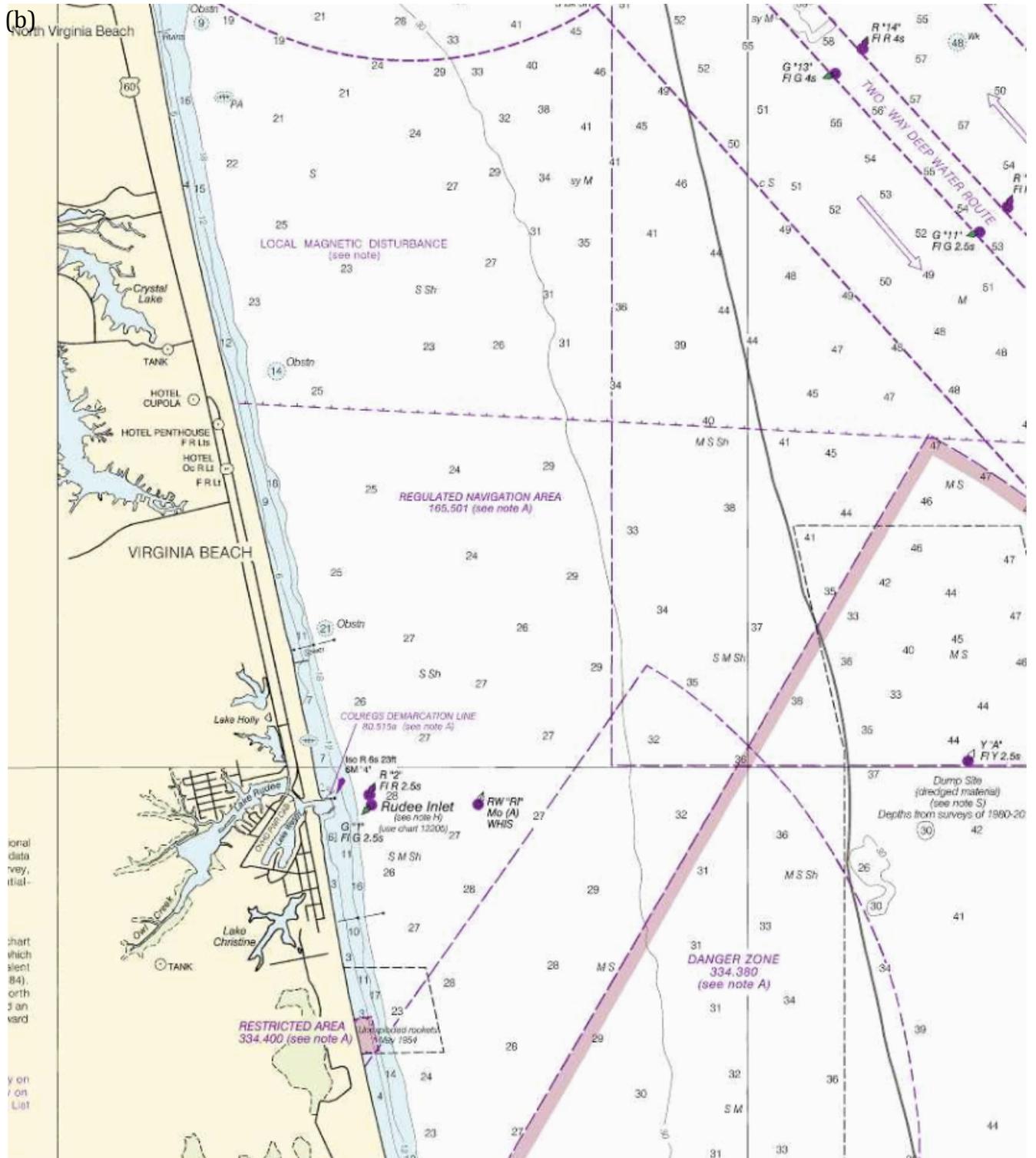


Figure 3 Historical tsunamis in Atlantic Ocean and Caribbean Sea ( National Geographic Data Center’s database).

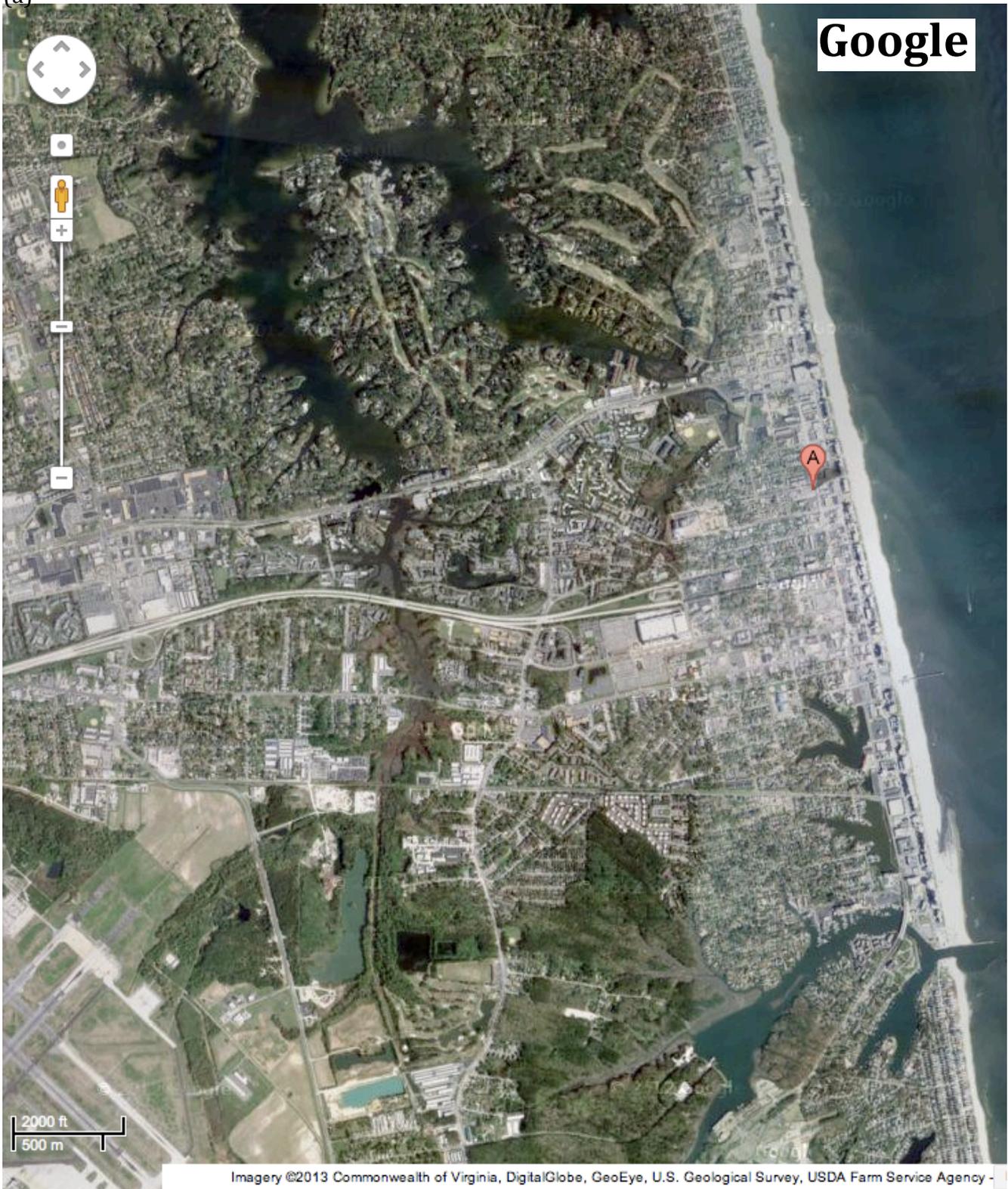


(a)



**Figure 4** NOAA charts, (a) 13003 and (b) 12208, show Virginia Beach Soundings in fathoms at Mean Lower Low Water. Contour and summit elevation values are in feet above Mean Sea Level.

(a)

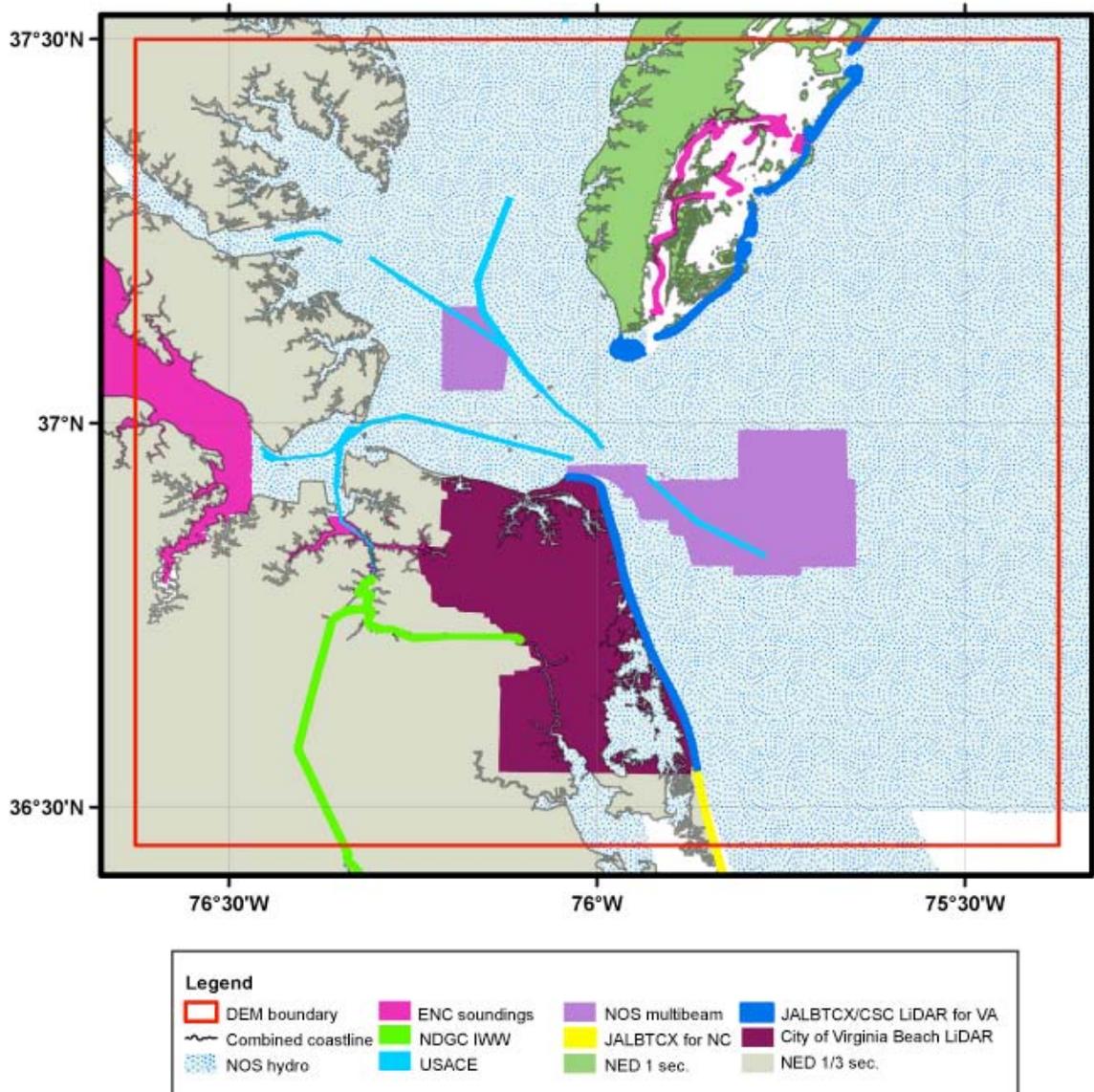




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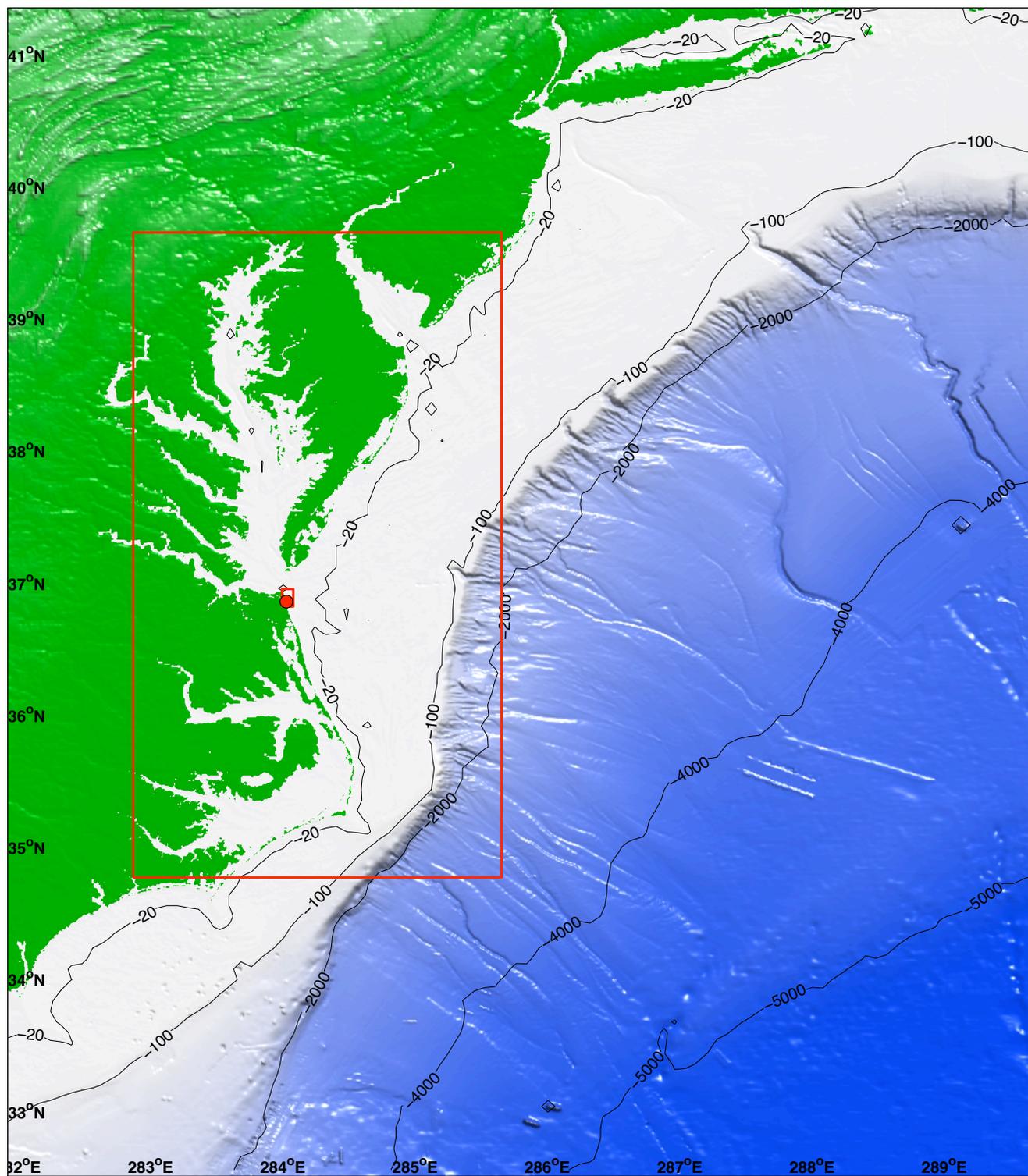
**Figure 5** Aerial photos of Virginia Beach.

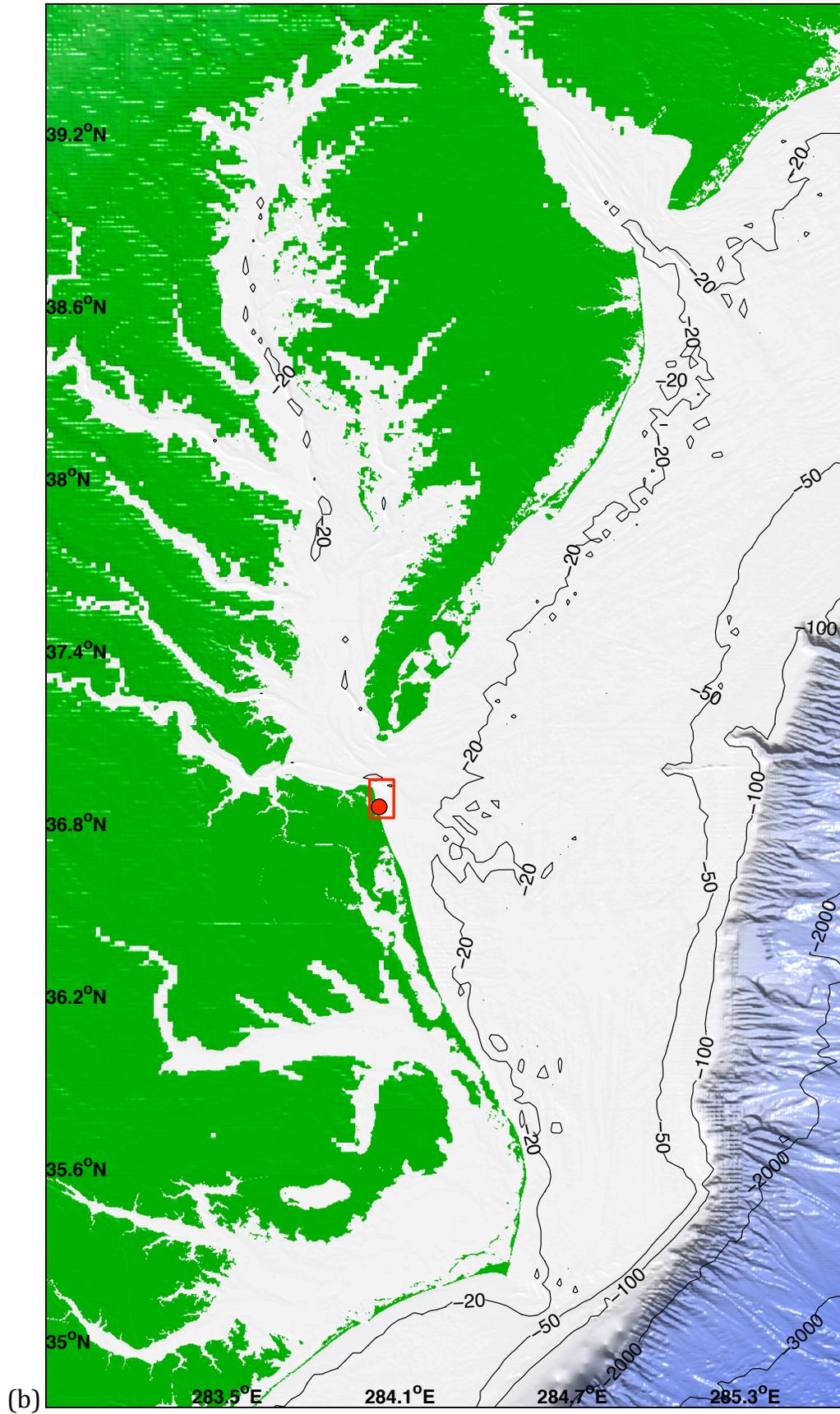


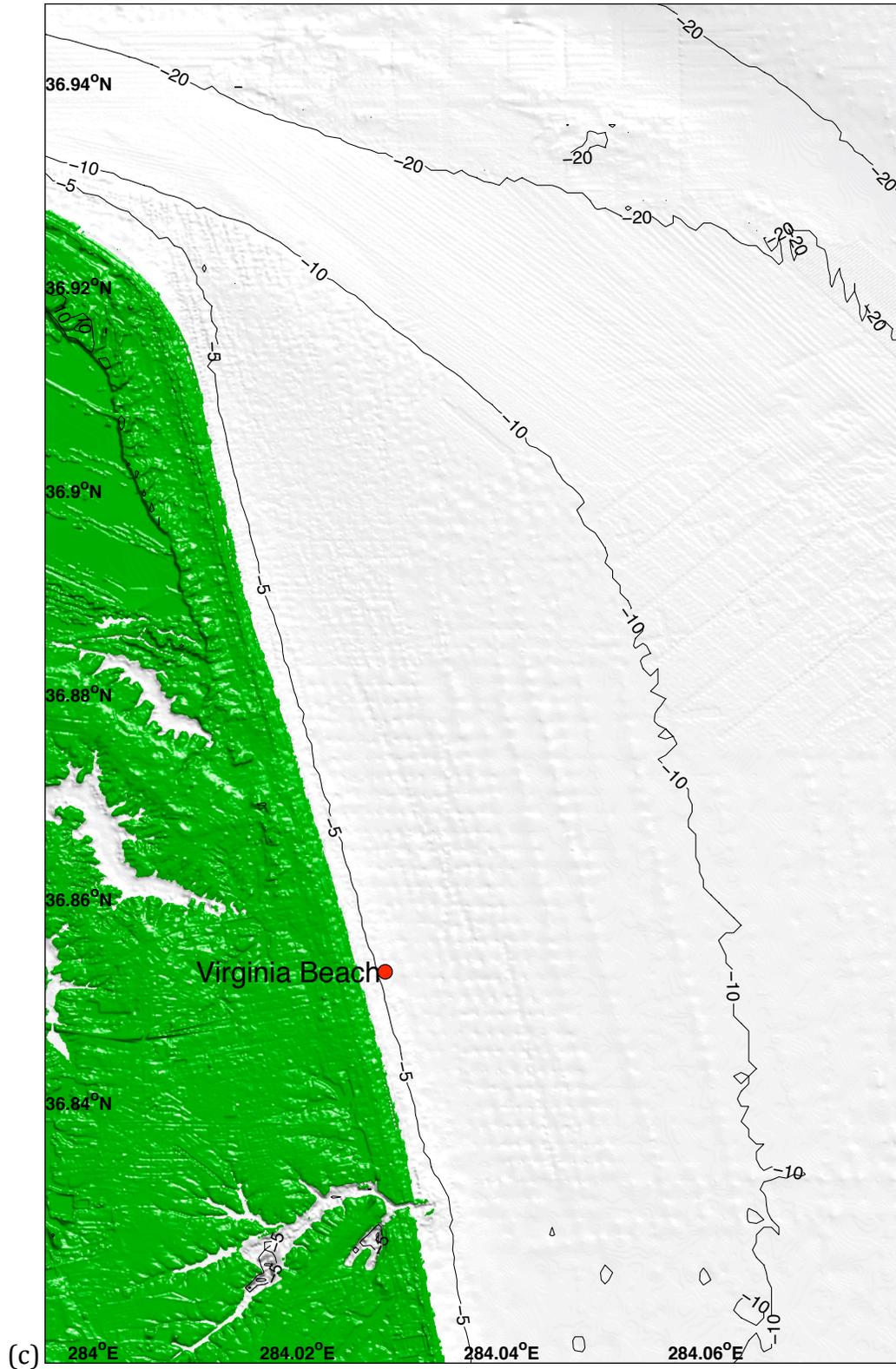


**Figure 7** Bathymetric and topographic data source overview for the high-resolution Virginia Beach DEM. Image courtesy of Tayler *et al.* (2007).

(a)

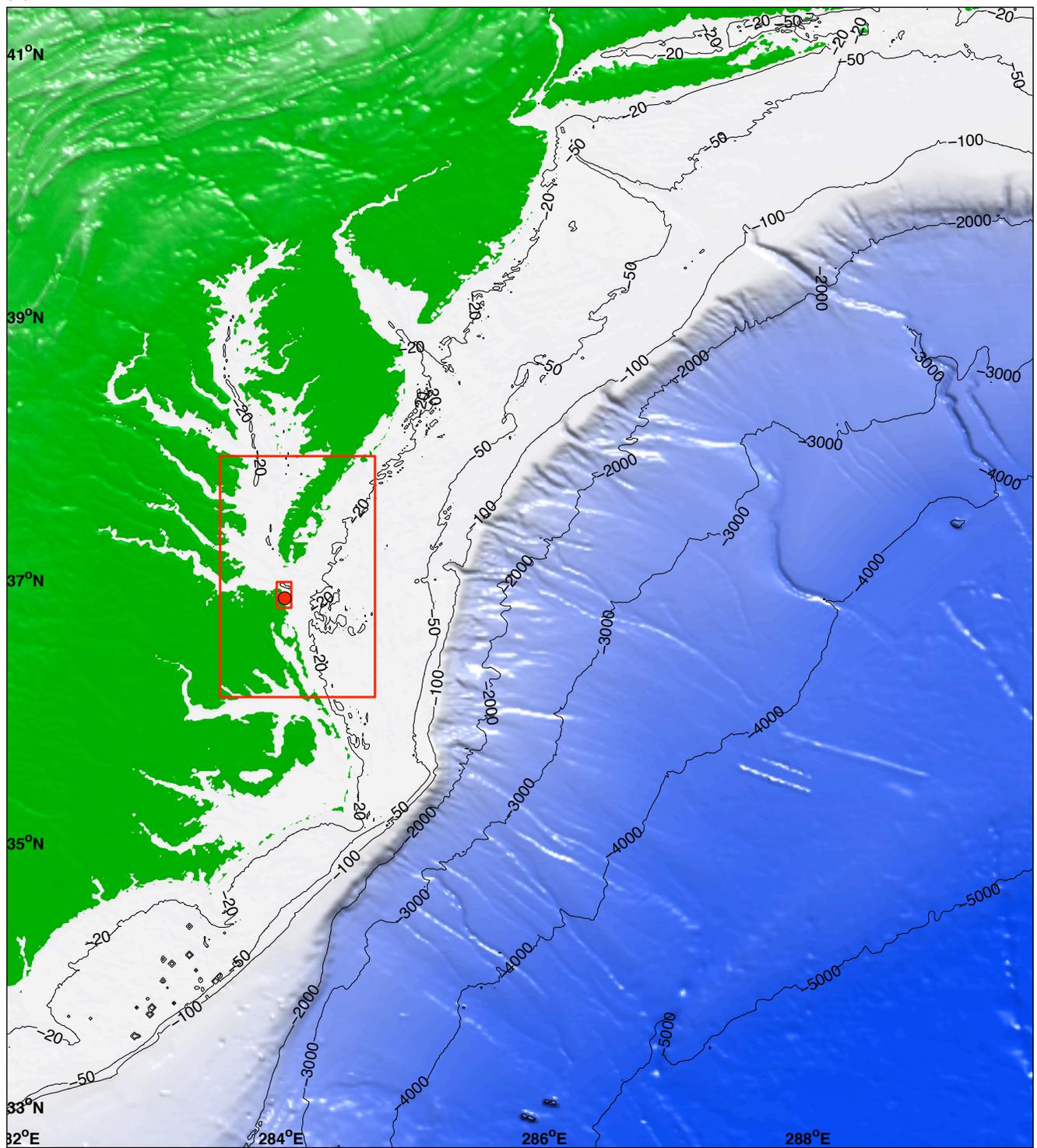


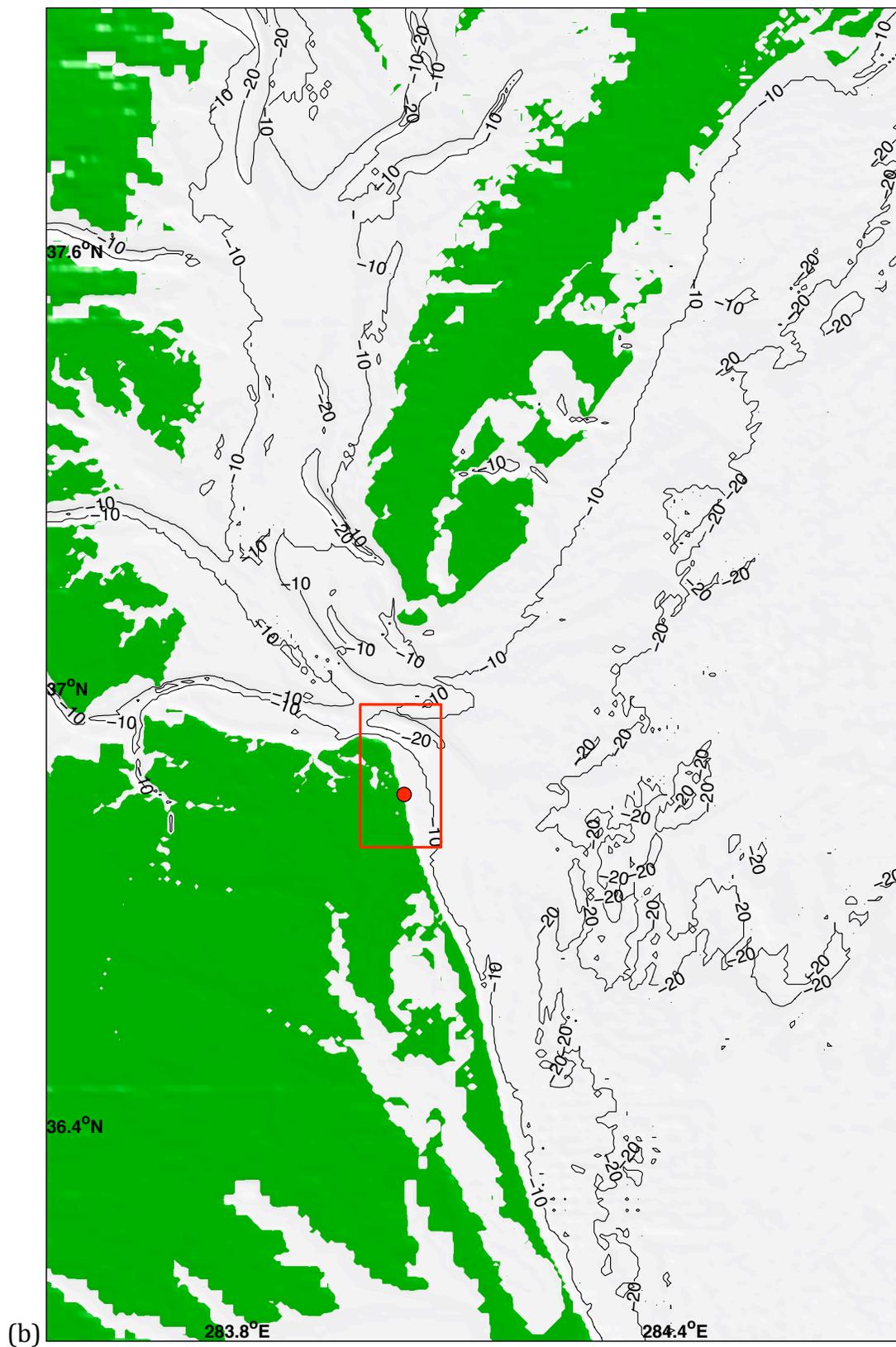




**Figure 8** Grid setup for the Virginia Beach reference model. Resolutions are (a) 36", (b) 12" and (c) 1/3". Red boxes are boundaries of the telescoped grids for the reference model.

(a)







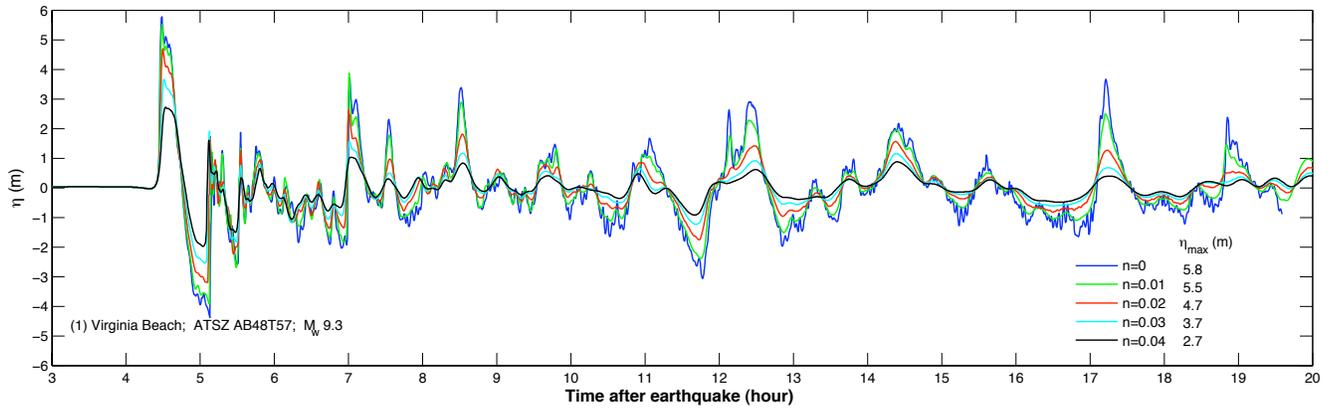
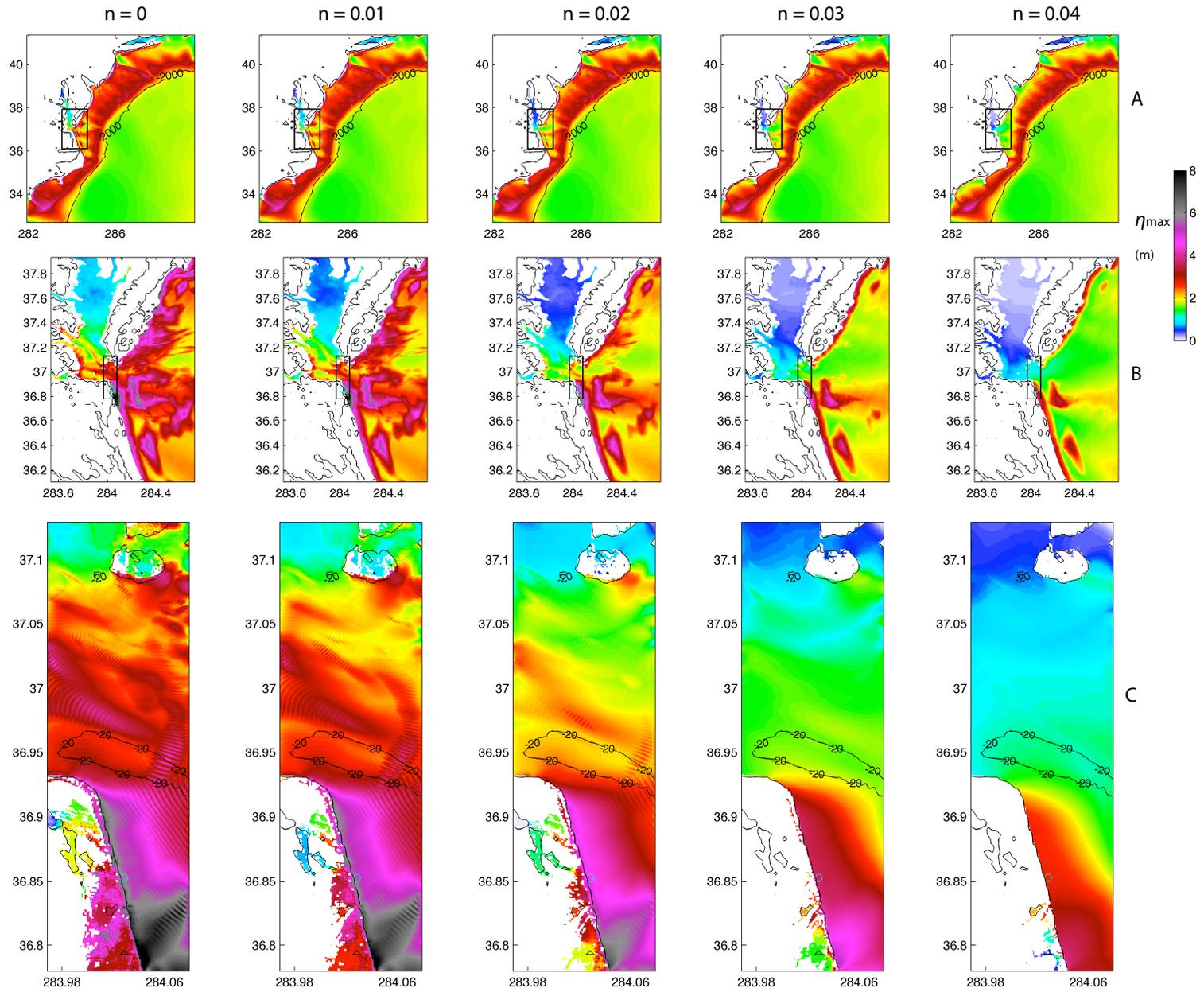
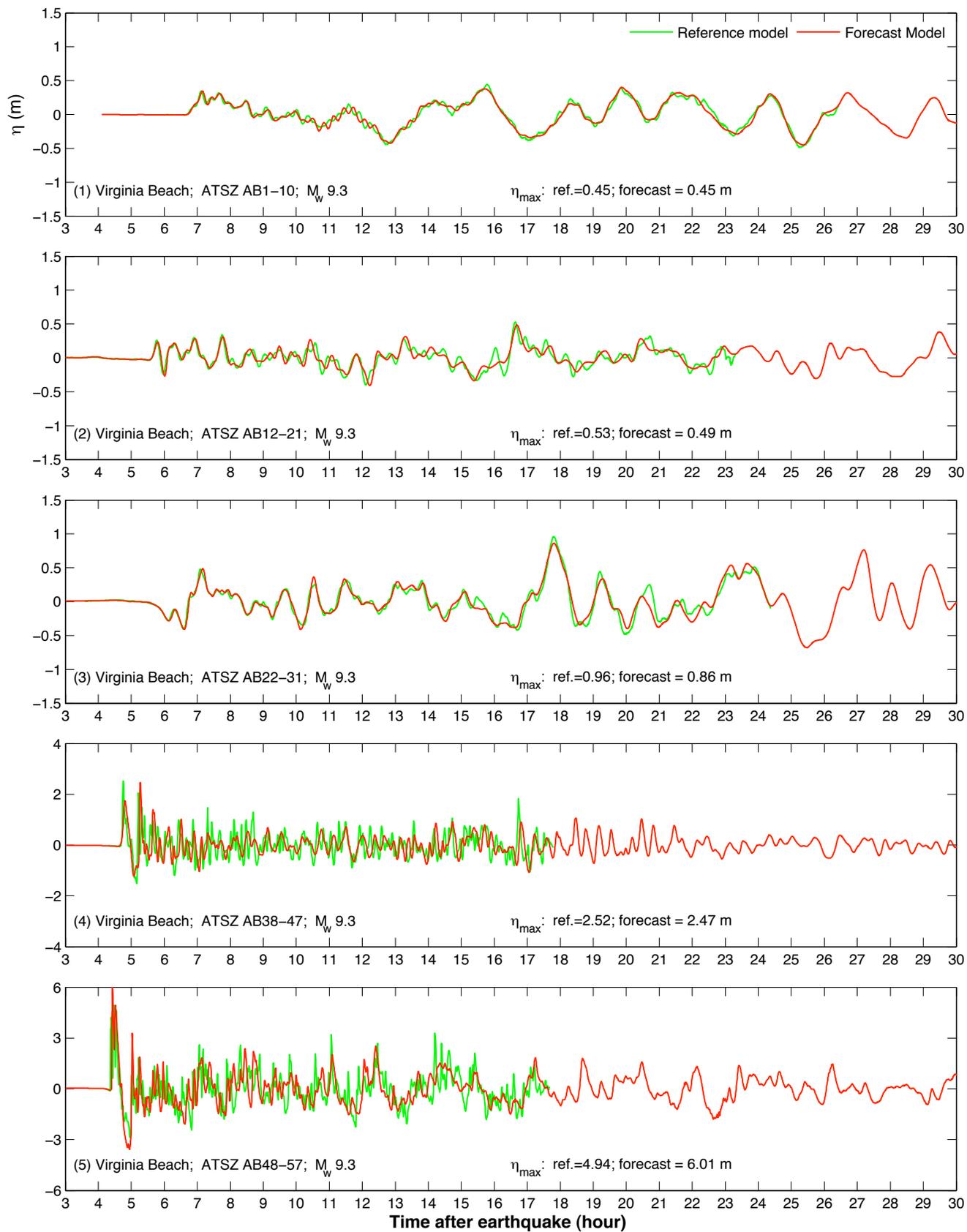
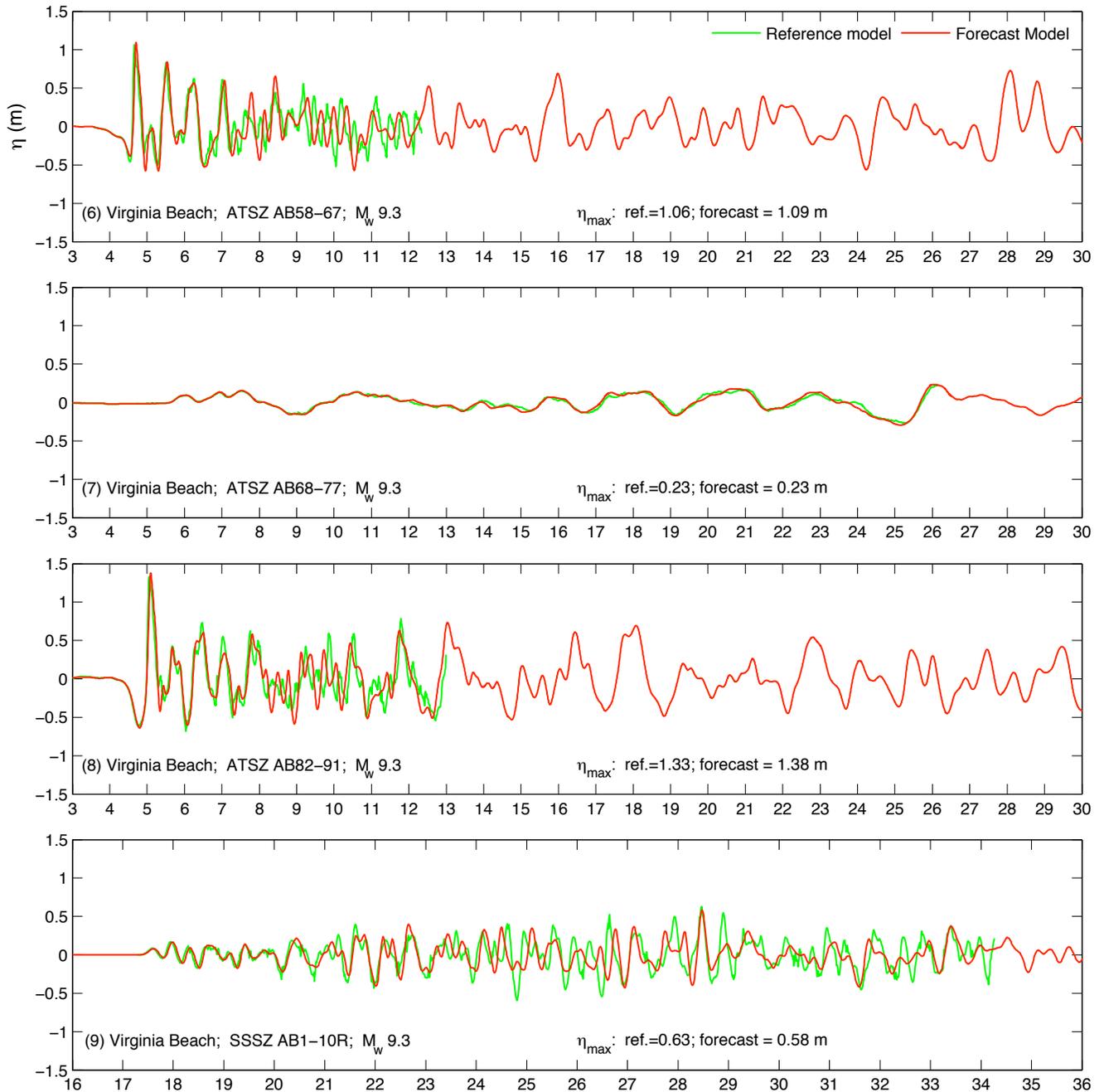


Figure 10 Sensitivity of  $\eta$  to friction coefficients. Results were computed by a set of testing grids (Fig. 11) for a magnitude 9.3 Caribbean tsunami.

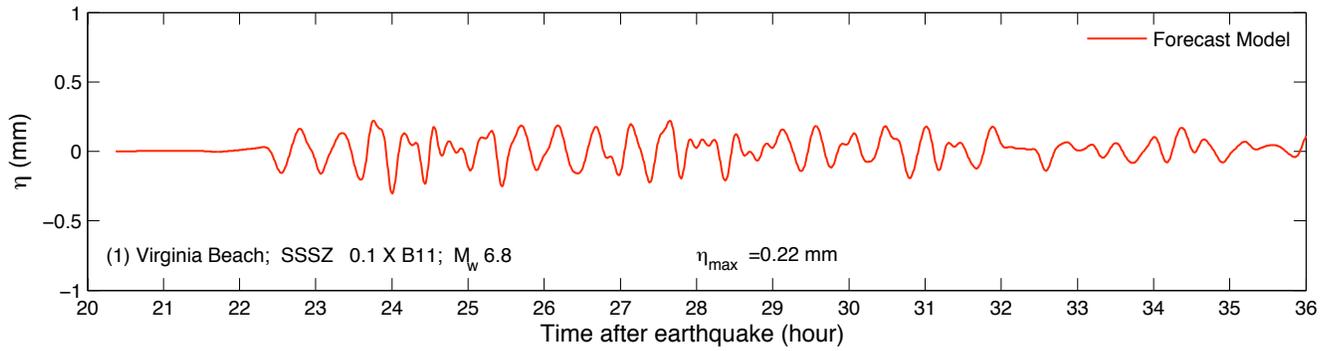


**Figure 11** Sensitivity of  $\eta_{max}$  to friction coefficients. Results were computed by a set of testing grids for a magnitude-9.3 Caribbean tsunami.

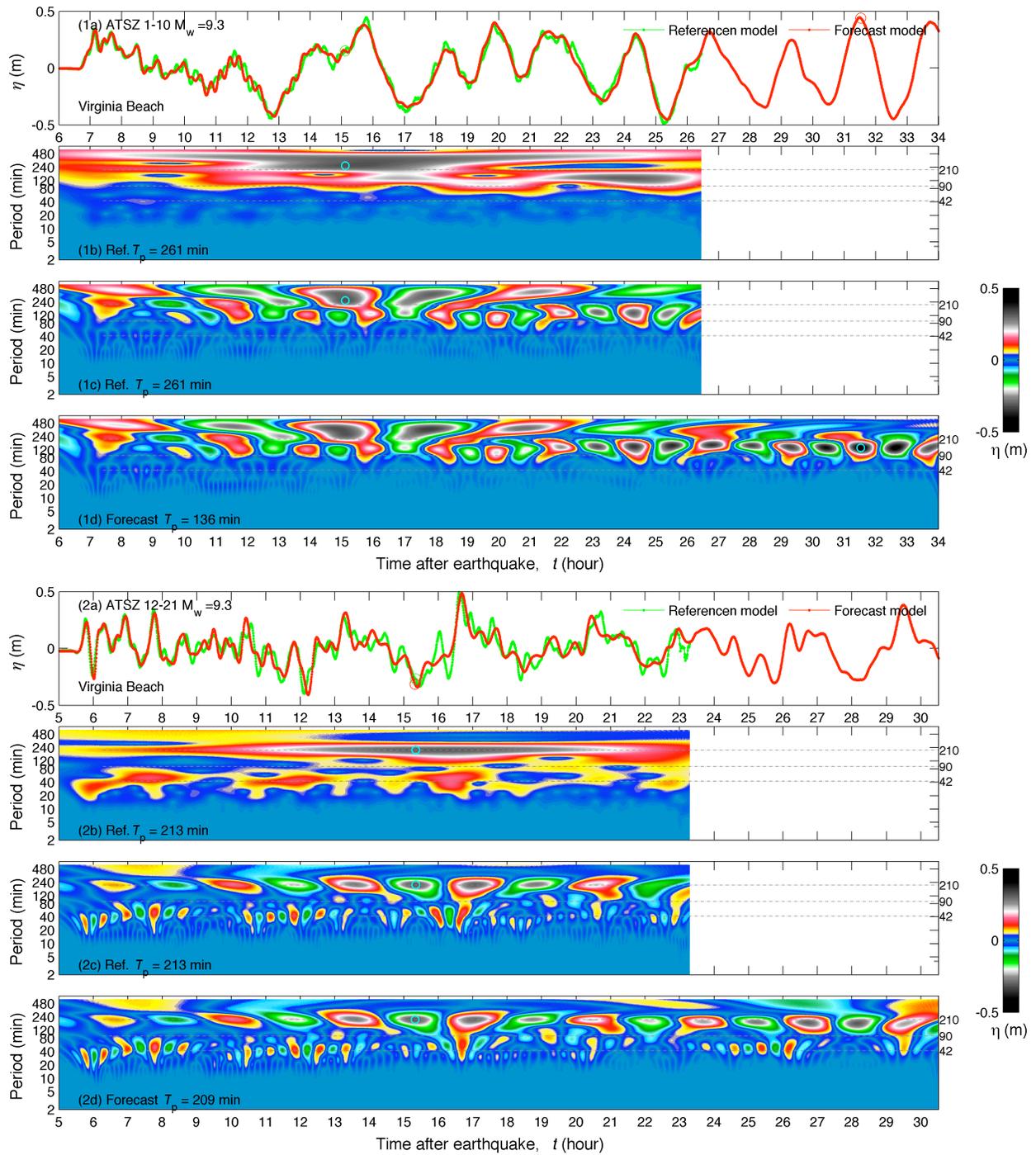


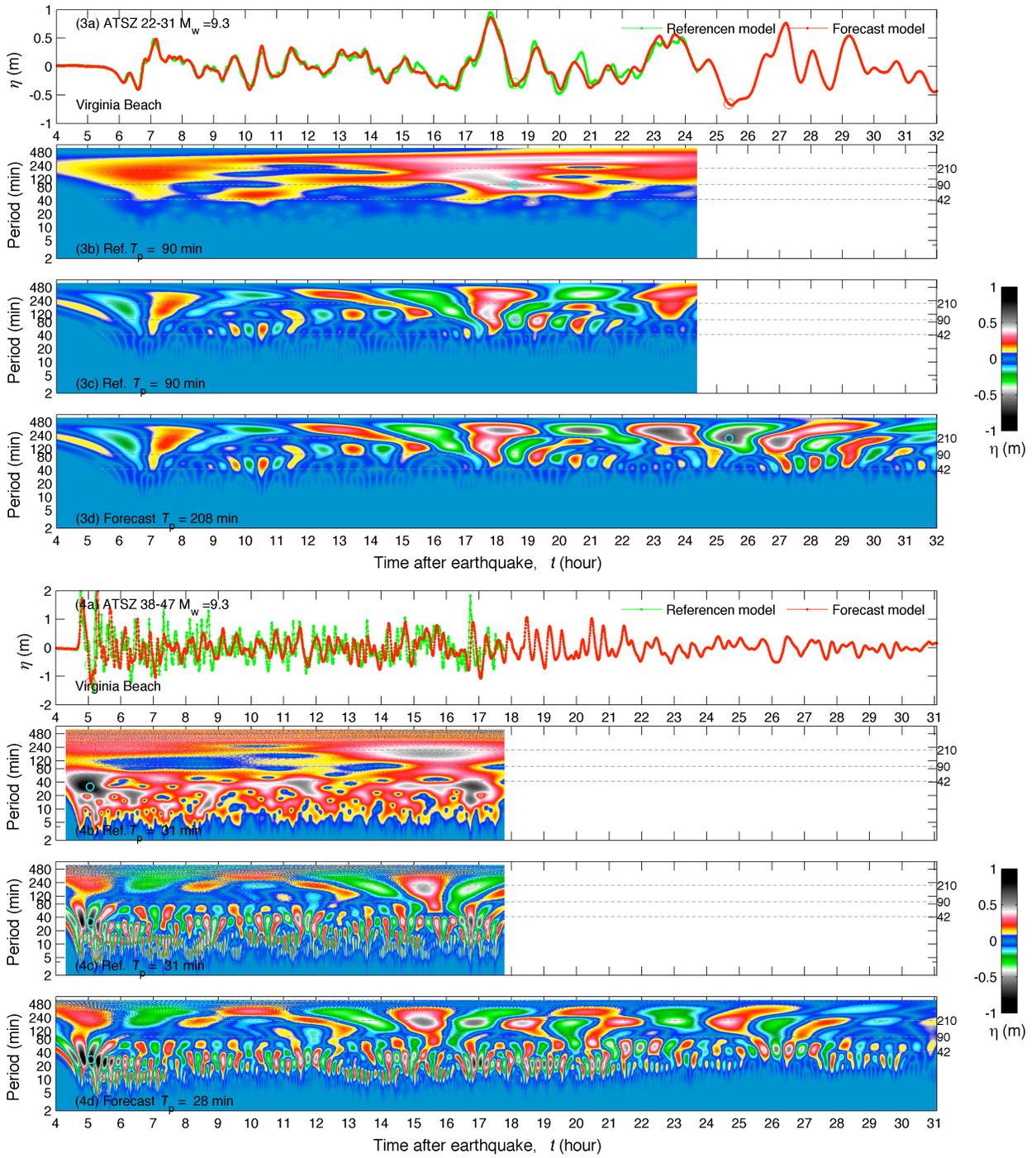


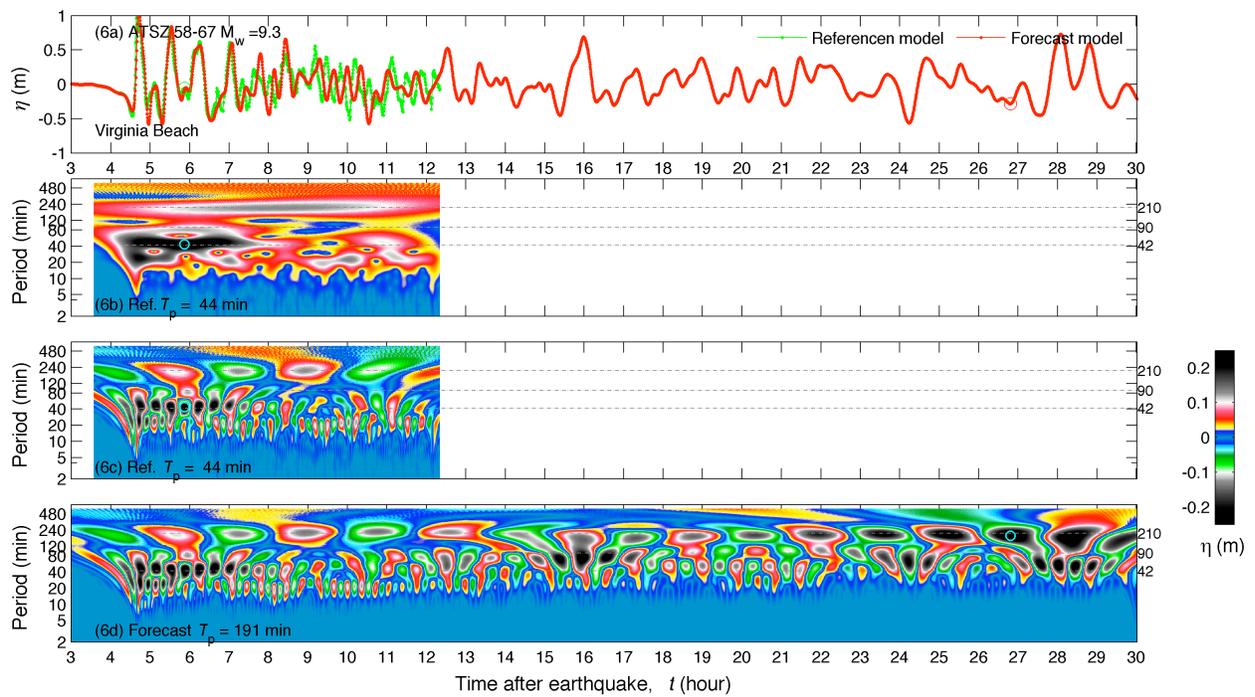
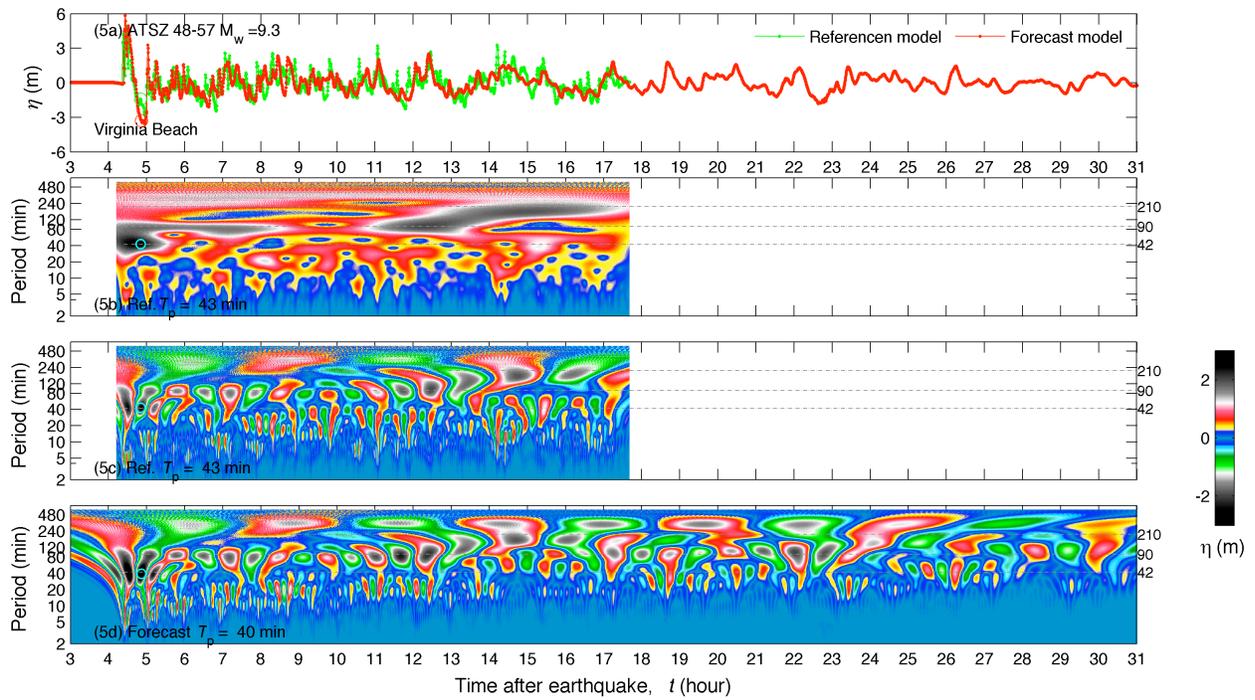
**Figure 12** Modeled  $\eta$  time series by the Virginia Beach reference and forecast models for simulated magnitude-9.3 tsunamis.

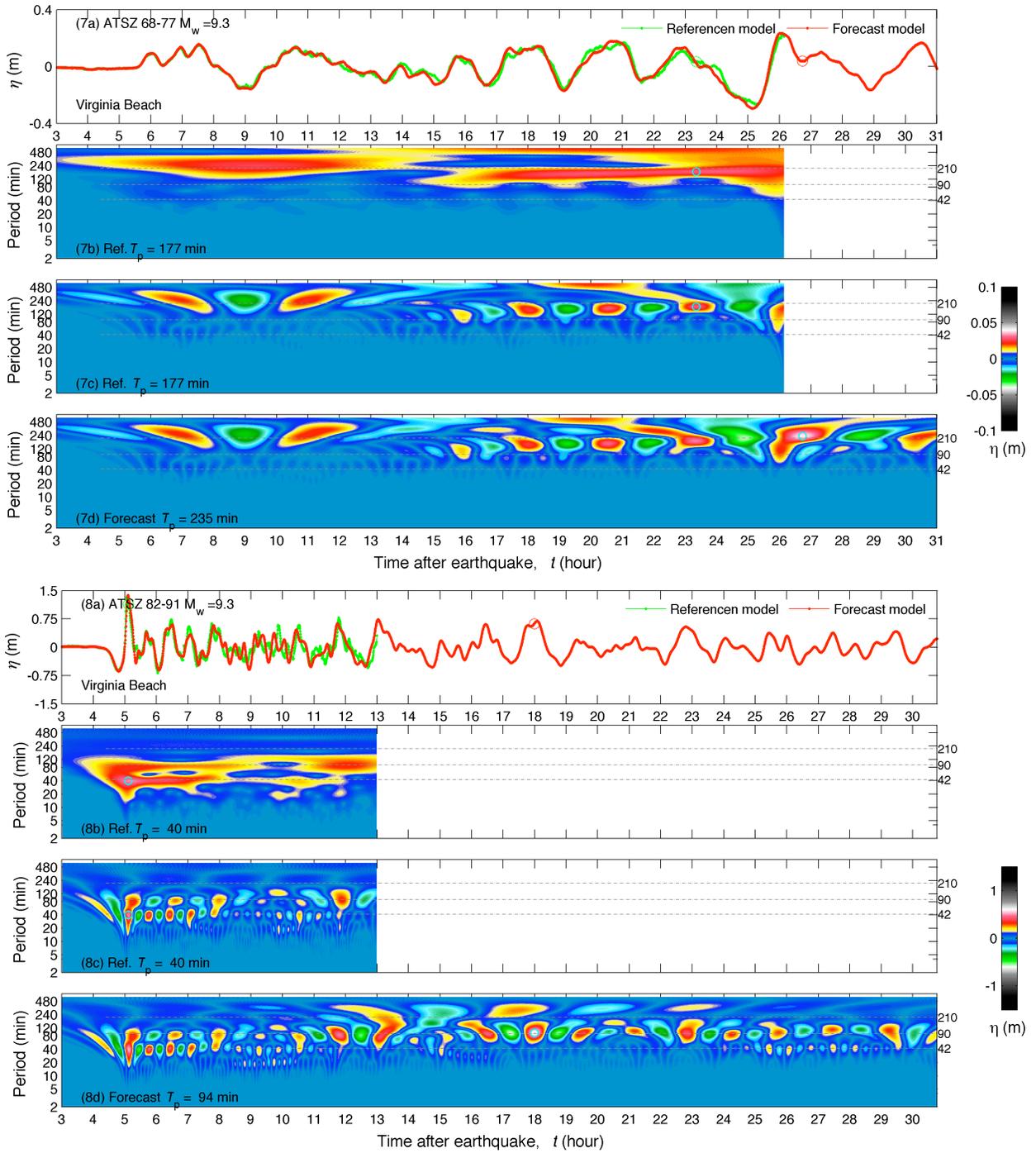


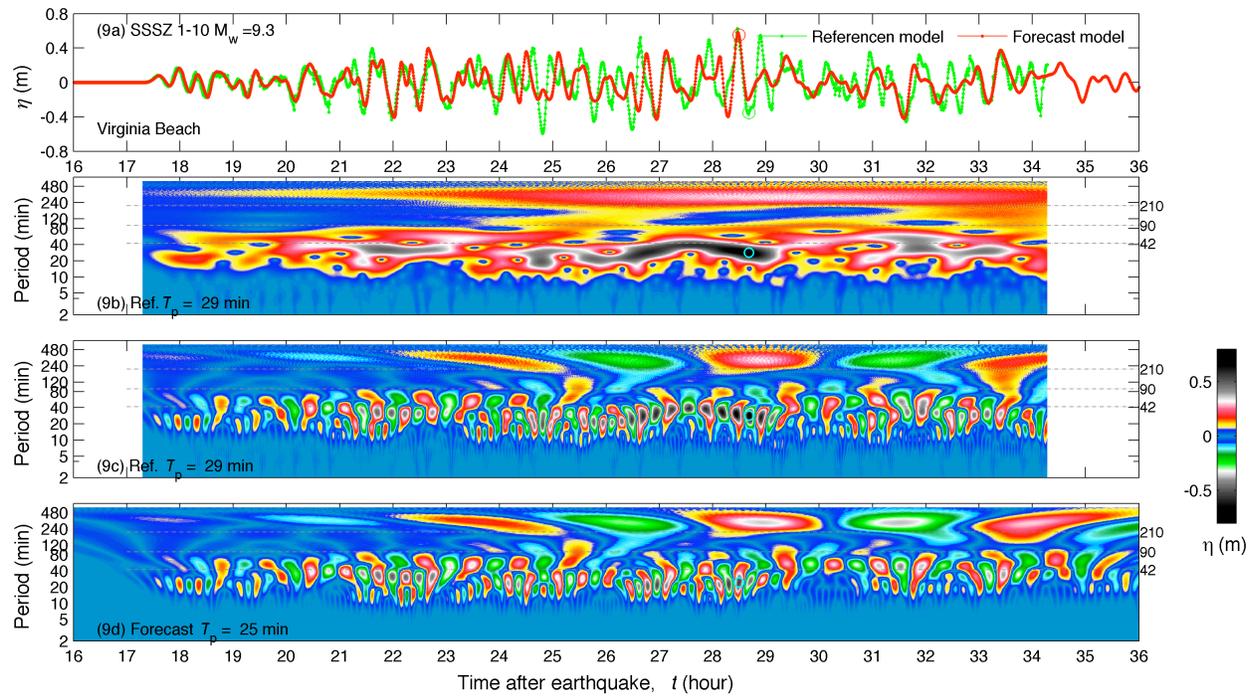
**Figure 13** Modeled  $\eta$  time series computed by the Virginia Beach forecast model for a simulated micro tsunami. The tsunami was generated from a Magnitude 6.8 earthquake from South Sandwich Islands Subduction ( $0.1 \times B11$ ).



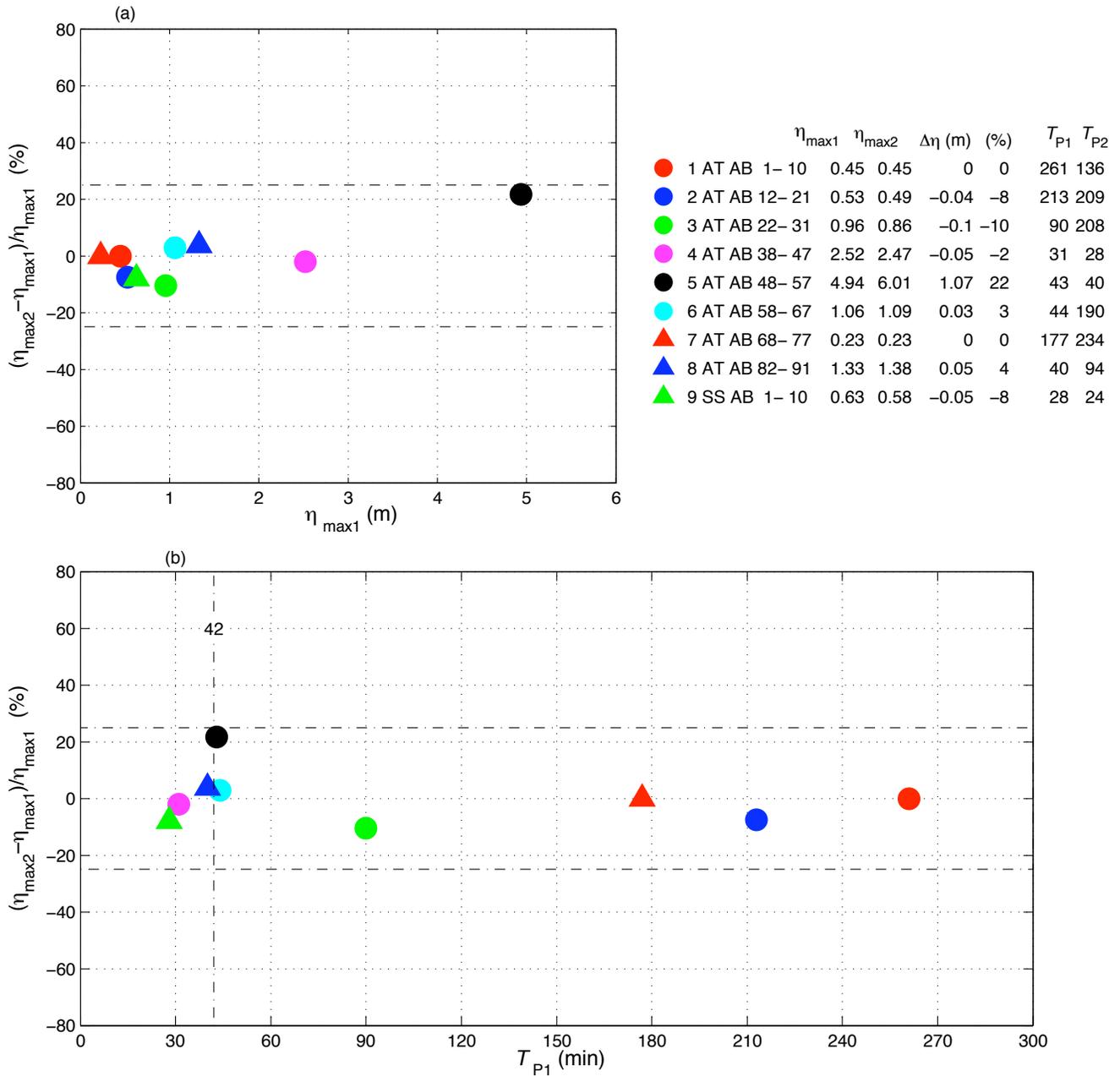




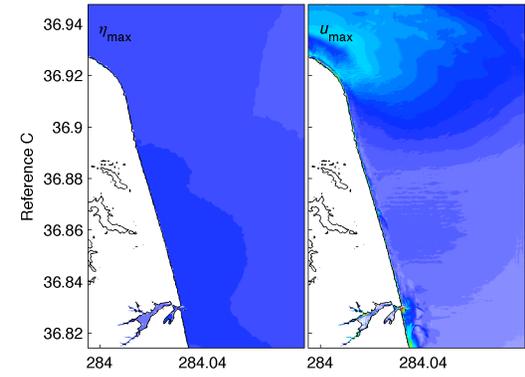
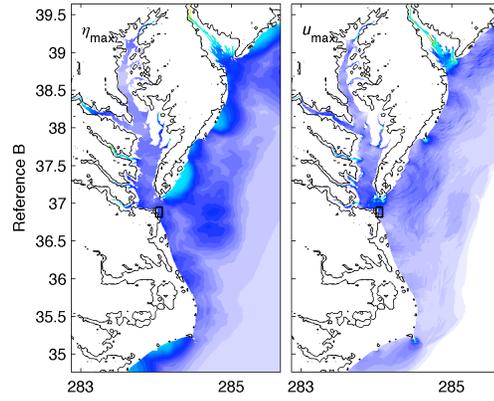
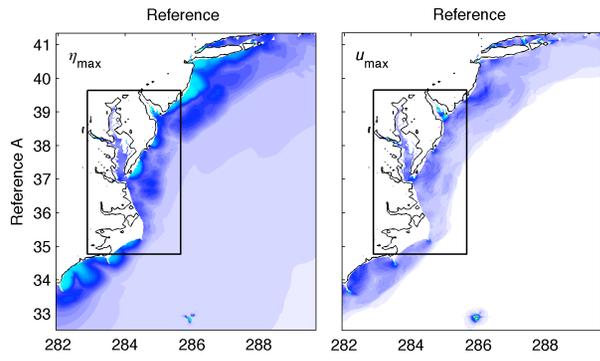




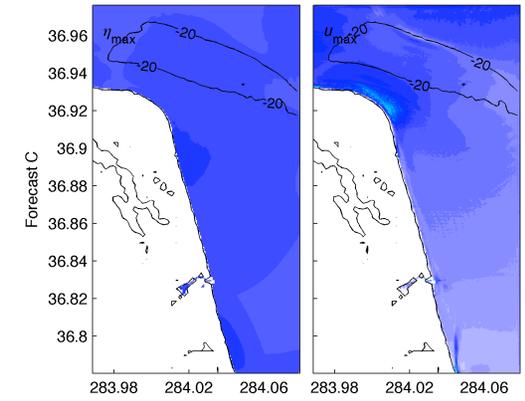
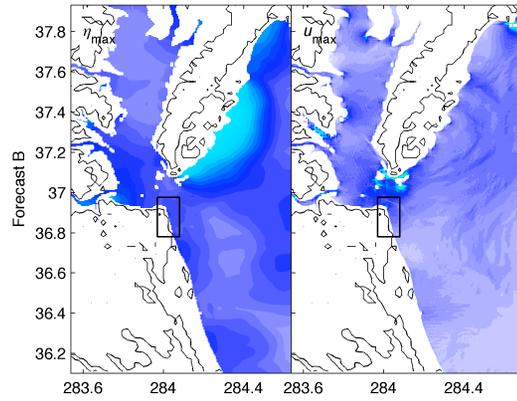
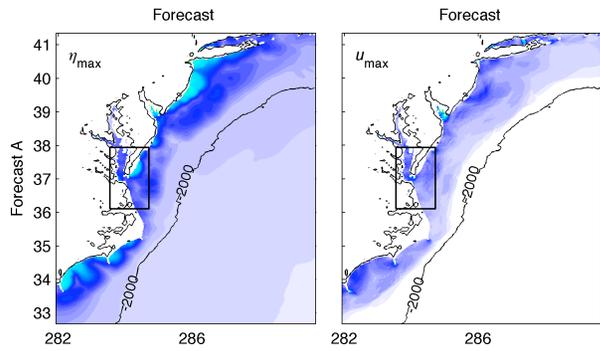
**Figure 14** (a) Modeled  $\eta$  time series at Virginia Beach warning point for the nine simulated magnitude-9.3 tsunamis. (b) Wavelet-derived amplitude spectrogram for the reference model. (c and d) Real part of the spectrograms computed by the reference and forecast models.

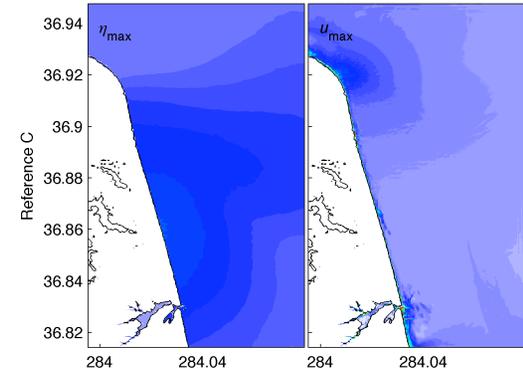
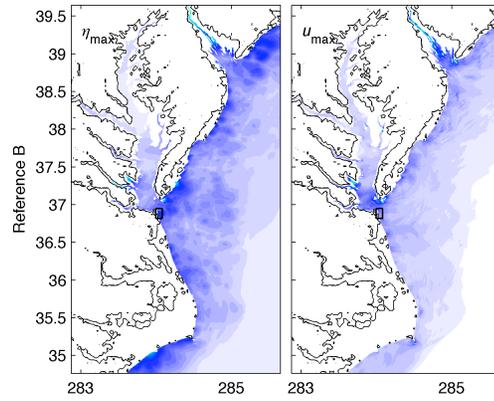
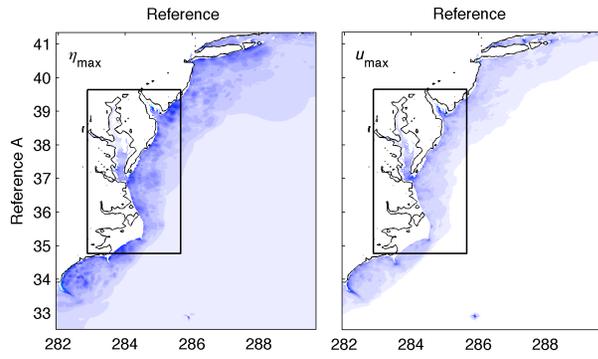


**Figure 15** (a) Forecast uncertainty in the  $\eta_{\max}$  at the Virginia Beach warning point. (b) Uncertainty v.s. peak period.  $\eta_{\max 1}$  and  $T_{p1}$ , maximum water elevation and peak period at the warning point from the reference model.  $\eta_{\max 2}$  and  $T_{p2}$ , maximum water surface elevation and peak period at the warning point computed by the forecast model.

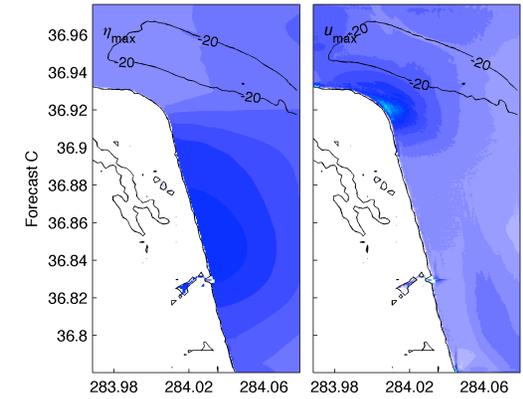
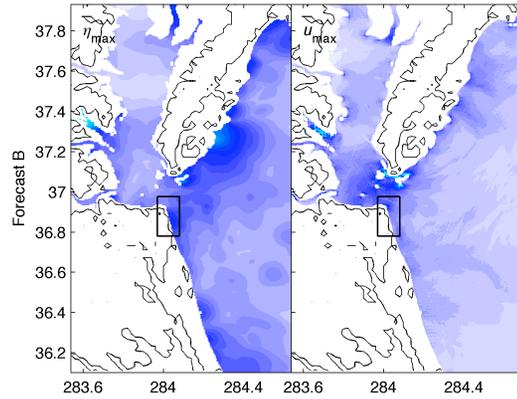
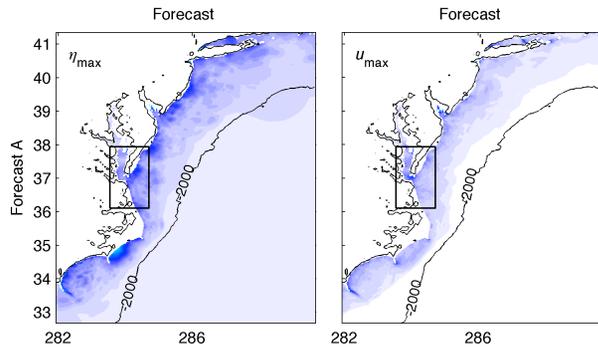


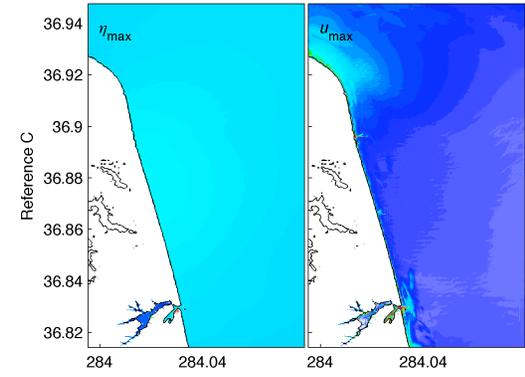
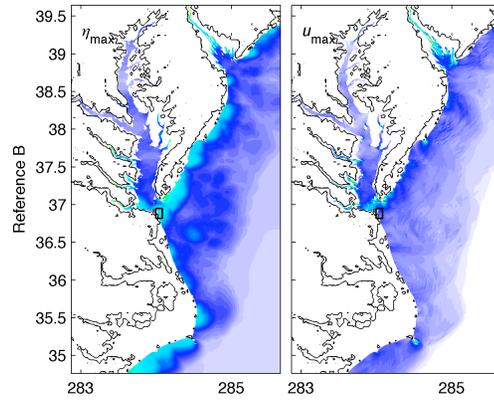
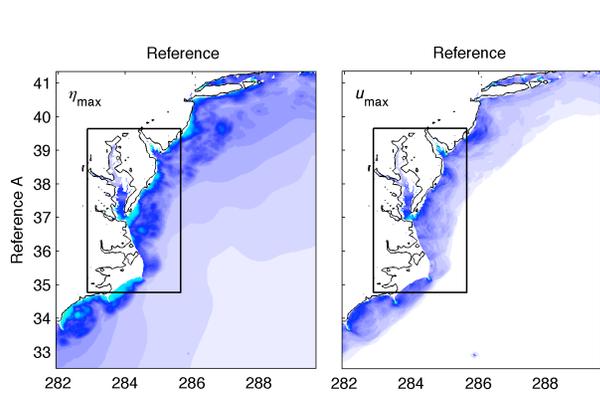
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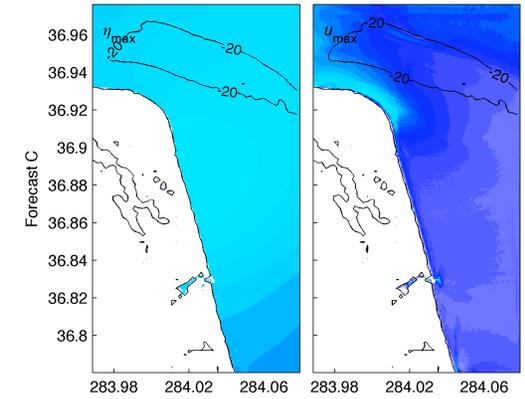
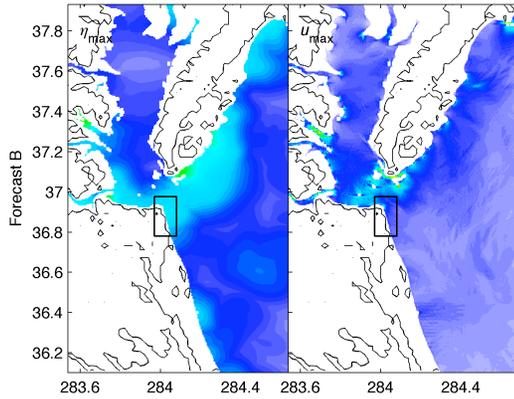
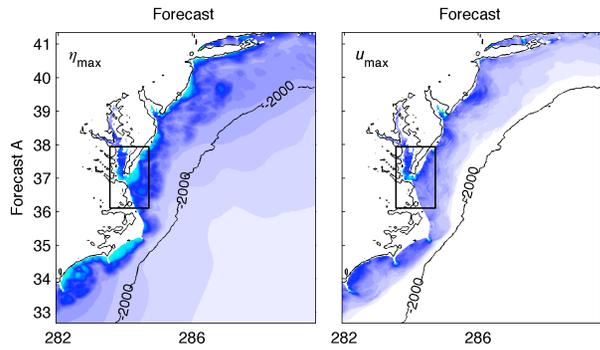


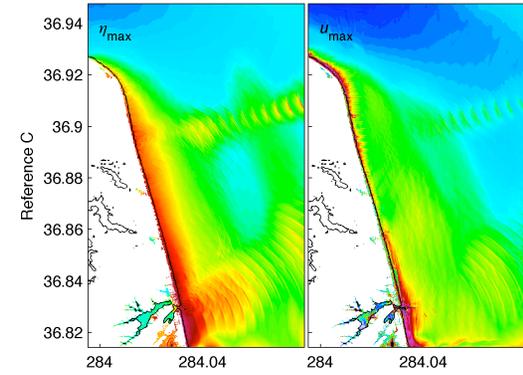
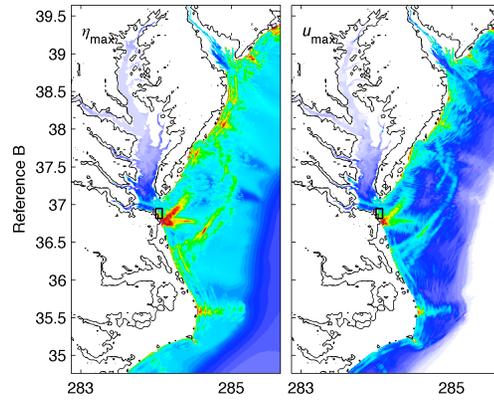
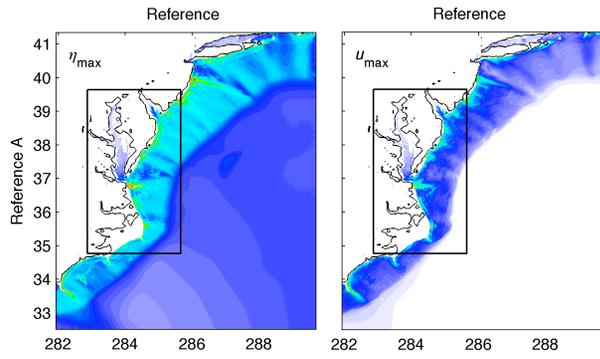
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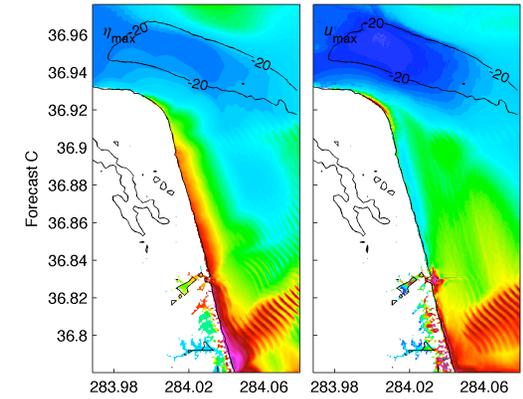
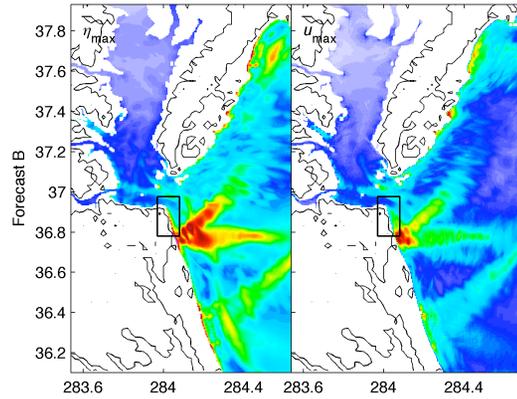
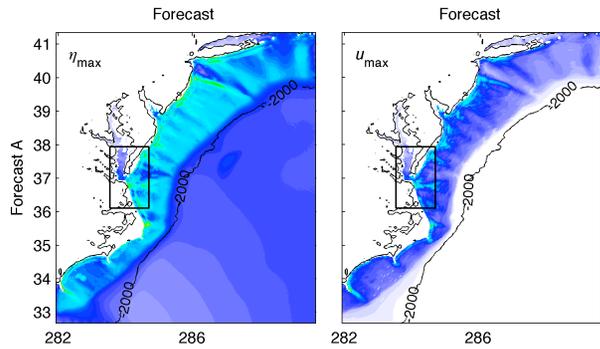


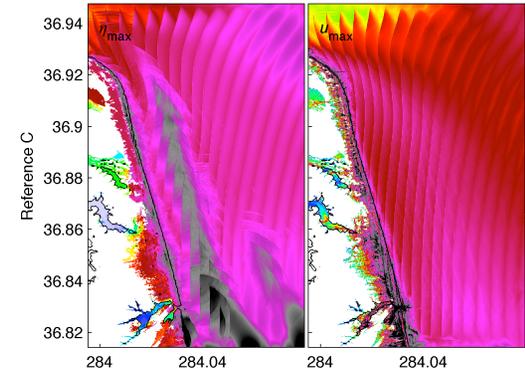
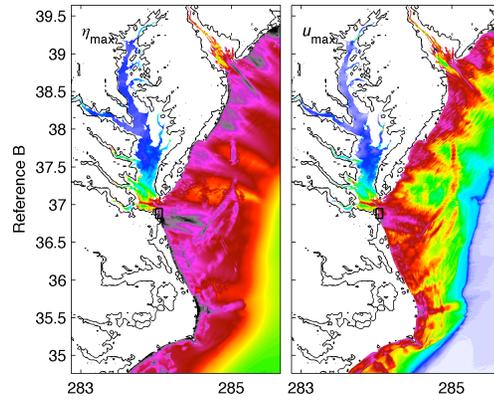
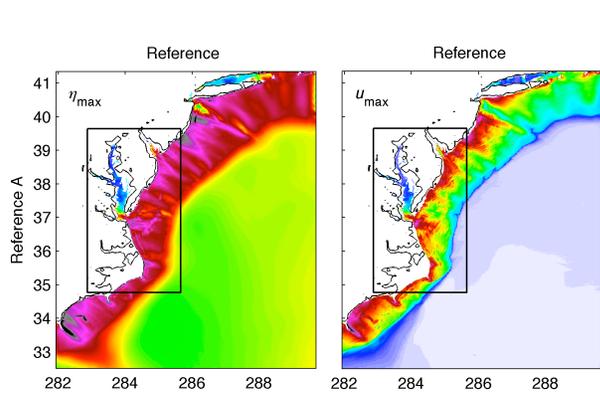
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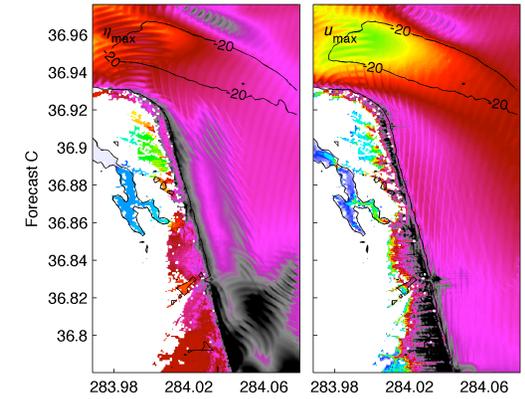
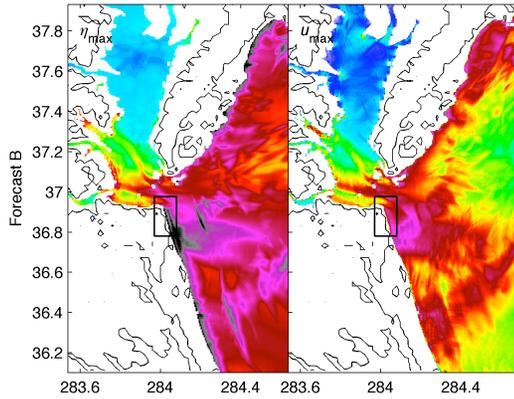
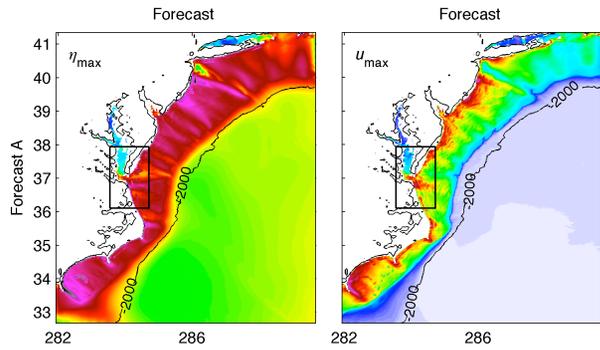


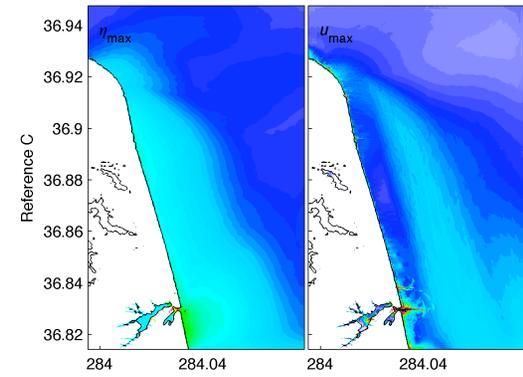
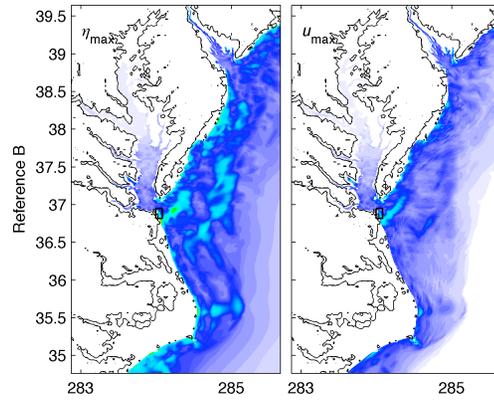
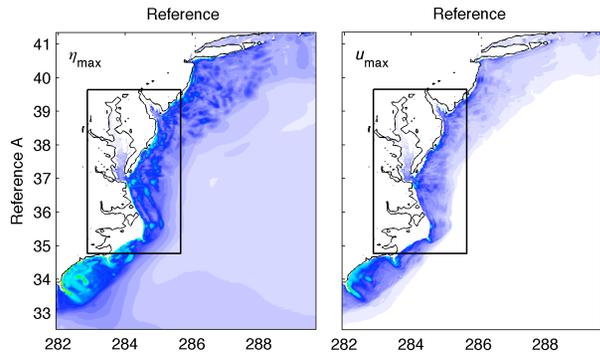
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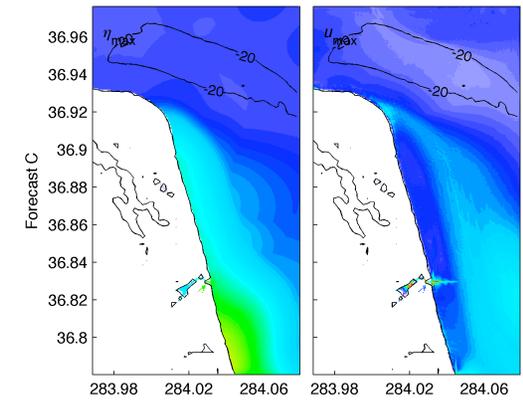
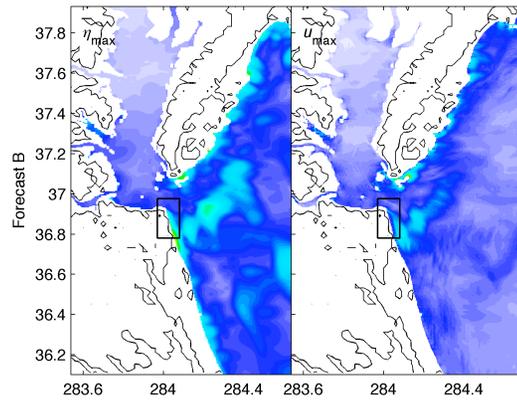
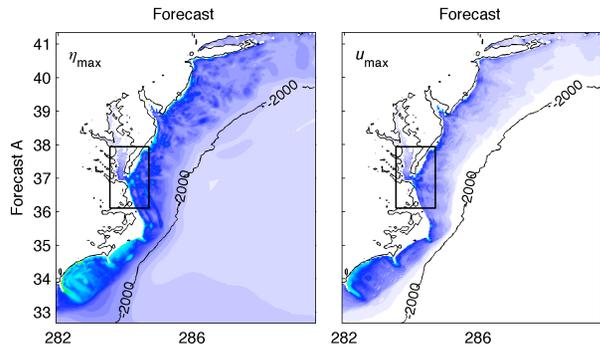


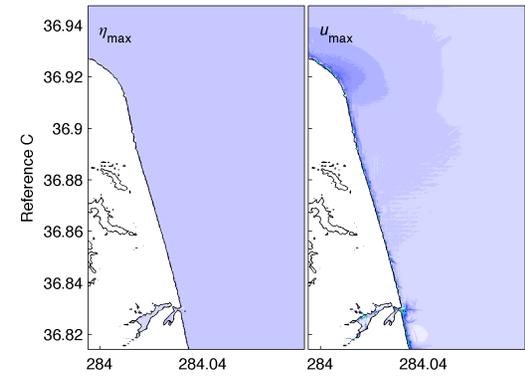
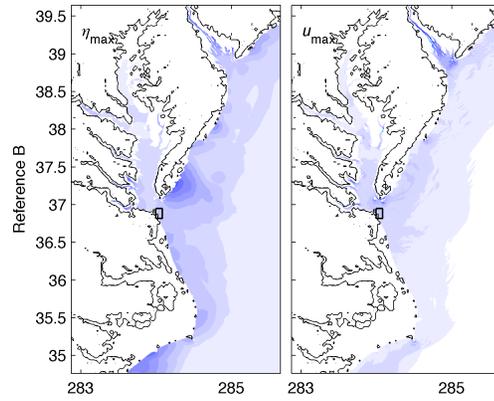
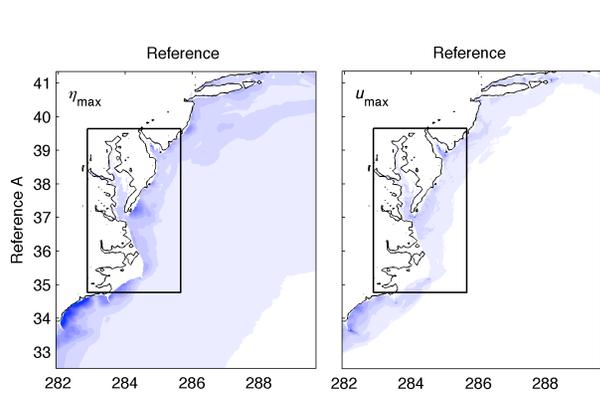
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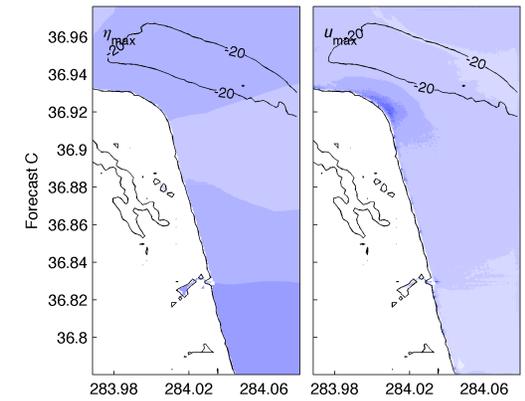
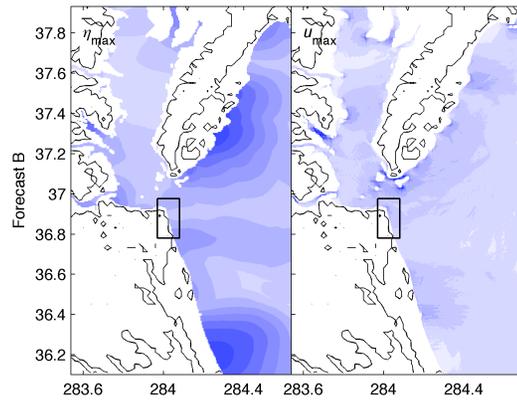
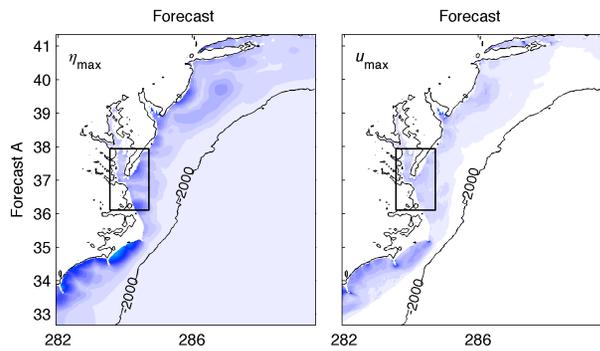


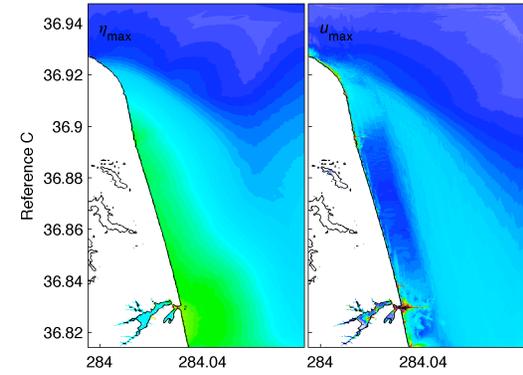
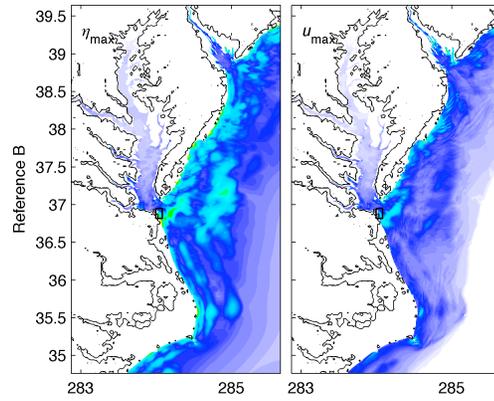
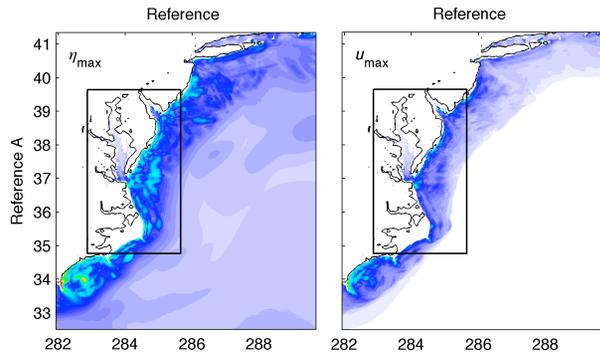
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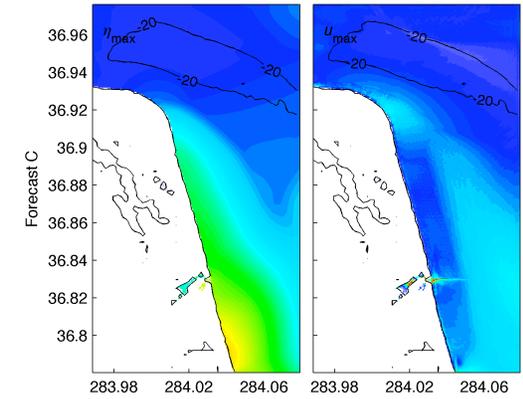
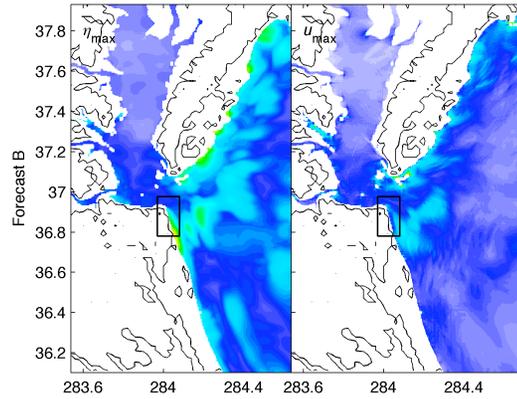
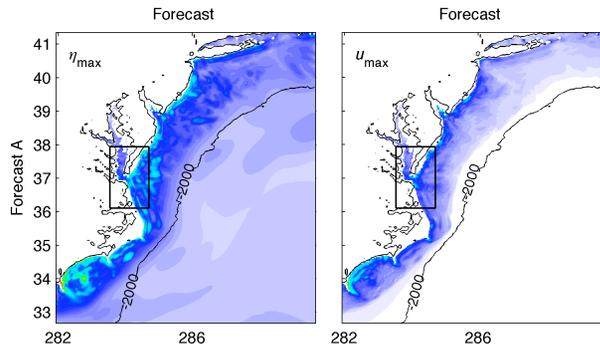


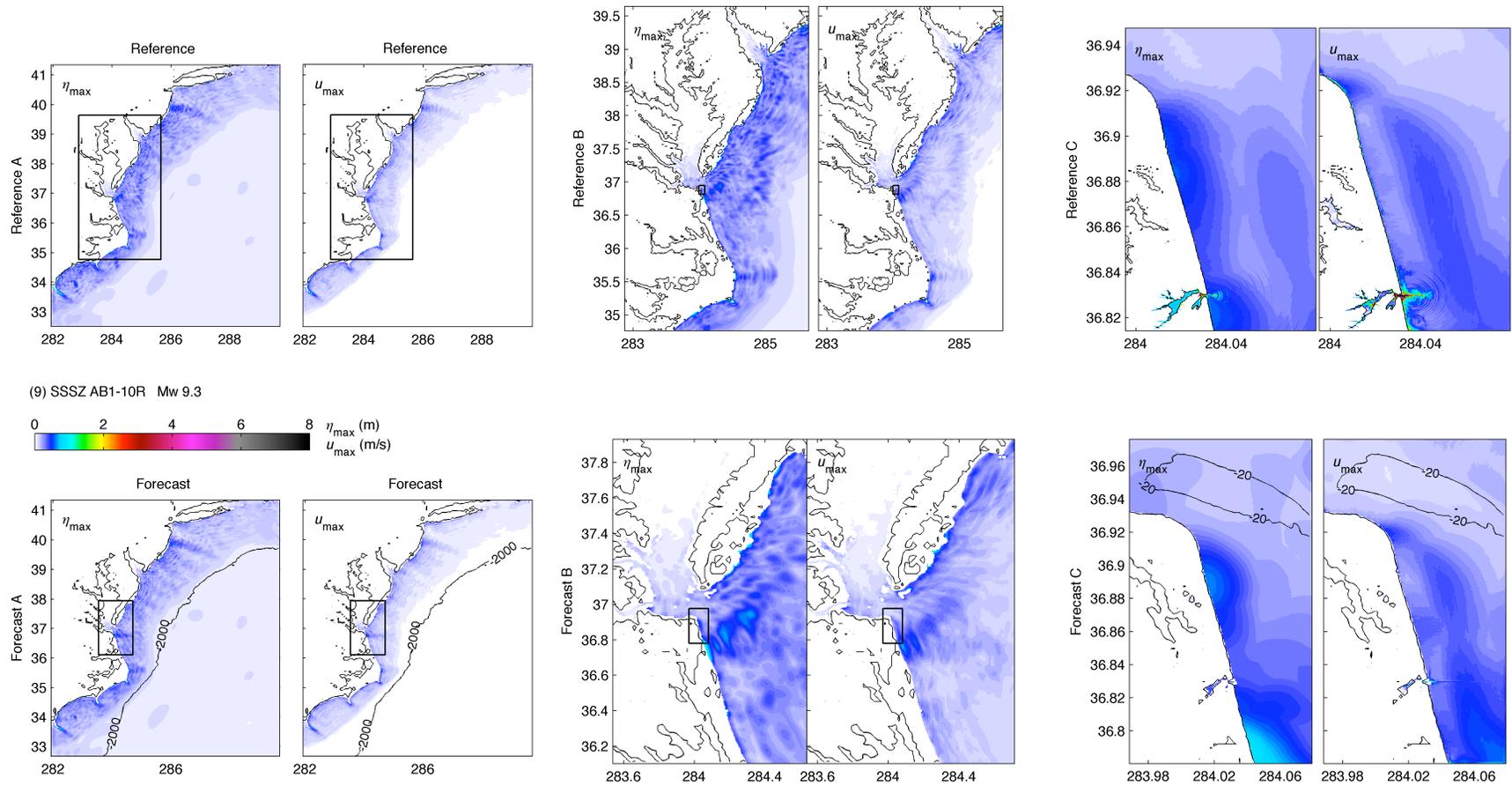
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(8) ATSZ AB82-91 Mw 9.3





**Figure 16** Maximum water elevation and current computed by the Virginia Beach reference and forecast models for the simulated magnitude-9.3 tsunamis.

## Appendix B

### Propagation Database: Atlantic Ocean Unit Sources



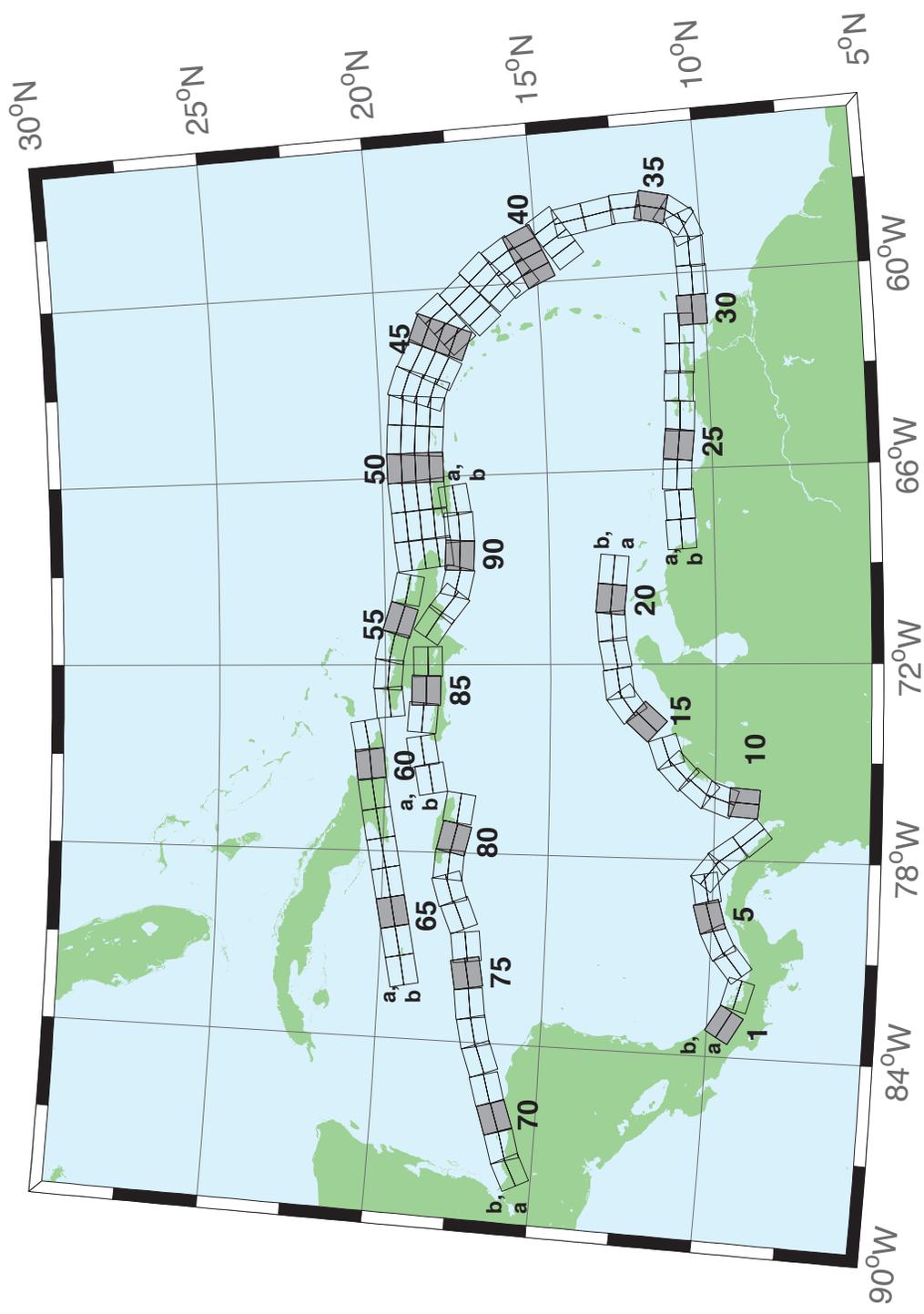


Figure B.1: Atlantic Source Zone unit sources.

Table B.1: Earthquake parameters for Atlantic Source Zone unit sources.

Segment	Description	Longitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz-1a	Atlantic Source Zone	-83.2020	9.1449	120	27.5	28.09
atsz-1b	Atlantic Source Zone	-83.0000	9.4899	120	27.5	5
atsz-2a	Atlantic Source Zone	-82.1932	8.7408	105.1	27.5	28.09
atsz-2b	Atlantic Source Zone	-82.0880	9.1254	105.1	27.5	5
atsz-3a	Atlantic Source Zone	-80.9172	9.0103	51.31	30	30
atsz-3b	Atlantic Source Zone	-81.1636	9.3139	51.31	30	5
atsz-4a	Atlantic Source Zone	-80.3265	9.4308	63.49	30	30
atsz-4b	Atlantic Source Zone	-80.5027	9.7789	63.49	30	5
atsz-5a	Atlantic Source Zone	-79.6247	9.6961	74.44	30	30
atsz-5b	Atlantic Source Zone	-79.7307	10.0708	74.44	30	5
atsz-6a	Atlantic Source Zone	-78.8069	9.8083	79.71	30	30
atsz-6b	Atlantic Source Zone	-78.8775	10.1910	79.71	30	5
atsz-7a	Atlantic Source Zone	-78.6237	9.7963	127.2	30	30
atsz-7b	Atlantic Source Zone	-78.3845	10.1059	127.2	30	5
atsz-8a	Atlantic Source Zone	-78.1693	9.3544	143.8	30	30
atsz-8b	Atlantic Source Zone	-77.8511	9.5844	143.8	30	5
atsz-9a	Atlantic Source Zone	-77.5913	8.5989	139.9	30	30
atsz-9b	Atlantic Source Zone	-77.2900	8.8493	139.9	30	5
atsz-10a	Atlantic Source Zone	-75.8109	9.0881	4.67	17	19.62
atsz-10b	Atlantic Source Zone	-76.2445	9.1231	4.67	17	5
atsz-11a	Atlantic Source Zone	-75.7406	9.6929	19.67	17	19.62
atsz-11b	Atlantic Source Zone	-76.1511	9.8375	19.67	17	5
atsz-12a	Atlantic Source Zone	-75.4763	10.2042	40.4	17	19.62
atsz-12b	Atlantic Source Zone	-75.8089	10.4826	40.4	17	5
atsz-13a	Atlantic Source Zone	-74.9914	10.7914	47.17	17	19.62
atsz-13b	Atlantic Source Zone	-75.2890	11.1064	47.17	17	5
atsz-14a	Atlantic Source Zone	-74.5666	11.0708	71.68	17	19.62
atsz-14b	Atlantic Source Zone	-74.7043	11.4786	71.68	17	5
atsz-15a	Atlantic Source Zone	-73.4576	11.8012	42.69	17	19.62
atsz-15b	Atlantic Source Zone	-73.7805	12.0924	42.69	17	5
atsz-16a	Atlantic Source Zone	-72.9788	12.3365	54.75	17	19.62
atsz-16b	Atlantic Source Zone	-73.2329	12.6873	54.75	17	5
atsz-17a	Atlantic Source Zone	-72.5454	12.5061	81.96	17	19.62
atsz-17b	Atlantic Source Zone	-72.6071	12.9314	81.96	17	5
atsz-18a	Atlantic Source Zone	-71.6045	12.6174	79.63	17	19.62
atsz-18b	Atlantic Source Zone	-71.6839	13.0399	79.63	17	5
atsz-19a	Atlantic Source Zone	-70.7970	12.7078	86.32	17	19.62
atsz-19b	Atlantic Source Zone	-70.8253	13.1364	86.32	17	5
atsz-20a	Atlantic Source Zone	-70.0246	12.7185	95.94	17	19.62
atsz-20b	Atlantic Source Zone	-69.9789	13.1457	95.94	17	5
atsz-21a	Atlantic Source Zone	-69.1244	12.6320	95.94	17	19.62
atsz-21b	Atlantic Source Zone	-69.0788	13.0592	95.94	17	5
atsz-22a	Atlantic Source Zone	-68.0338	11.4286	266.9	15	17.94
atsz-22b	Atlantic Source Zone	-68.0102	10.9954	266.9	15	5
atsz-23a	Atlantic Source Zone	-67.1246	11.4487	266.9	15	17.94
atsz-23b	Atlantic Source Zone	-67.1010	11.0155	266.9	15	5
atsz-24a	Atlantic Source Zone	-66.1656	11.5055	273.3	15	17.94
atsz-24b	Atlantic Source Zone	-66.1911	11.0724	273.3	15	5
atsz-25a	Atlantic Source Zone	-65.2126	11.4246	276.4	15	17.94
atsz-25b	Atlantic Source Zone	-65.2616	10.9934	276.4	15	5
atsz-26a	Atlantic Source Zone	-64.3641	11.3516	272.9	15	17.94
atsz-26b	Atlantic Source Zone	-64.3862	10.9183	272.9	15	5
atsz-27a	Atlantic Source Zone	-63.4472	11.3516	272.9	15	17.94

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**Table B.1 – continued from previous page**

Segment	Description	Longitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz-27b	Atlantic Source Zone	-63.4698	10.9183	272.9	15	5
atsz-28a	Atlantic Source Zone	-62.6104	11.2831	271.1	15	17.94
atsz-28b	Atlantic Source Zone	-62.6189	10.8493	271.1	15	5
atsz-29a	Atlantic Source Zone	-61.6826	11.2518	271.6	15	17.94
atsz-29b	Atlantic Source Zone	-61.6947	10.8181	271.6	15	5
atsz-30a	Atlantic Source Zone	-61.1569	10.8303	269	15	17.94
atsz-30b	Atlantic Source Zone	-61.1493	10.3965	269	15	5
atsz-31a	Atlantic Source Zone	-60.2529	10.7739	269	15	17.94
atsz-31b	Atlantic Source Zone	-60.2453	10.3401	269	15	5
atsz-32a	Atlantic Source Zone	-59.3510	10.8123	269	15	17.94
atsz-32b	Atlantic Source Zone	-59.3734	10.3785	269	15	5
atsz-33a	Atlantic Source Zone	-58.7592	10.8785	248.6	15	17.94
atsz-33b	Atlantic Source Zone	-58.5984	10.4745	248.6	15	5
atsz-34a	Atlantic Source Zone	-58.5699	11.0330	217.2	15	17.94
atsz-34b	Atlantic Source Zone	-58.2179	10.7710	217.2	15	5
atsz-35a	Atlantic Source Zone	-58.3549	11.5300	193.7	15	17.94
atsz-35b	Atlantic Source Zone	-57.9248	11.4274	193.7	15	5
atsz-36a	Atlantic Source Zone	-58.3432	12.1858	177.7	15	17.94
atsz-36b	Atlantic Source Zone	-57.8997	12.2036	177.7	15	5
atsz-37a	Atlantic Source Zone	-58.4490	12.9725	170.7	15	17.94
atsz-37b	Atlantic Source Zone	-58.0095	13.0424	170.7	15	5
atsz-38a	Atlantic Source Zone	-58.6079	13.8503	170.2	15	17.94
atsz-38b	Atlantic Source Zone	-58.1674	13.9240	170.2	15	5
atsz-39a	Atlantic Source Zone	-58.6667	14.3915	146.8	15	17.94
atsz-39b	Atlantic Source Zone	-58.2913	14.6287	146.8	15	5
atsz-39y	Atlantic Source Zone	-59.4168	13.9171	146.8	15	43.82
atsz-39z	Atlantic Source Zone	-59.0415	14.1543	146.8	15	30.88
atsz-40a	Atlantic Source Zone	-59.1899	15.2143	156.2	15	17.94
atsz-40b	Atlantic Source Zone	-58.7781	15.3892	156.2	15	5
atsz-40y	Atlantic Source Zone	-60.0131	14.8646	156.2	15	43.82
atsz-40z	Atlantic Source Zone	-59.6012	15.0395	156.2	15	30.88
atsz-41a	Atlantic Source Zone	-59.4723	15.7987	146.3	15	17.94
atsz-41b	Atlantic Source Zone	-59.0966	16.0392	146.3	15	5
atsz-41y	Atlantic Source Zone	-60.2229	15.3177	146.3	15	43.82
atsz-41z	Atlantic Source Zone	-59.8473	15.5582	146.3	15	30.88
atsz-42a	Atlantic Source Zone	-59.9029	16.4535	137	15	17.94
atsz-42b	Atlantic Source Zone	-59.5716	16.7494	137	15	5
atsz-42y	Atlantic Source Zone	-60.5645	15.8616	137	15	43.82
atsz-42z	Atlantic Source Zone	-60.2334	16.1575	137	15	30.88
atsz-43a	Atlantic Source Zone	-60.5996	17.0903	138.7	15	17.94
atsz-43b	Atlantic Source Zone	-60.2580	17.3766	138.7	15	5
atsz-43y	Atlantic Source Zone	-61.2818	16.5177	138.7	15	43.82
atsz-43z	Atlantic Source Zone	-60.9404	16.8040	138.7	15	30.88
atsz-44a	Atlantic Source Zone	-61.1559	17.8560	141.1	15	17.94
atsz-44b	Atlantic Source Zone	-60.8008	18.1286	141.1	15	5
atsz-44y	Atlantic Source Zone	-61.8651	17.3108	141.1	15	43.82
atsz-44z	Atlantic Source Zone	-61.5102	17.5834	141.1	15	30.88
atsz-45a	Atlantic Source Zone	-61.5491	18.0566	112.8	15	17.94
atsz-45b	Atlantic Source Zone	-61.3716	18.4564	112.8	15	5
atsz-45y	Atlantic Source Zone	-61.9037	17.2569	112.8	15	43.82
atsz-45z	Atlantic Source Zone	-61.7260	17.6567	112.8	15	30.88
atsz-46a	Atlantic Source Zone	-62.4217	18.4149	117.9	15	17.94
atsz-46b	Atlantic Source Zone	-62.2075	18.7985	117.9	15	5
atsz-46y	Atlantic Source Zone	-62.8493	17.6477	117.9	15	43.82
atsz-46z	Atlantic Source Zone	-62.6352	18.0313	117.9	15	30.88

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**Table B.1 – continued from previous page**

Segment	Description	Longitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz-47a	Atlantic Source Zone	-63.1649	18.7844	110.5	20	22.1
atsz-47b	Atlantic Source Zone	-63.0087	19.1798	110.5	20	5
atsz-47y	Atlantic Source Zone	-63.4770	17.9936	110.5	20	56.3
atsz-47z	Atlantic Source Zone	-63.3205	18.3890	110.5	20	39.2
atsz-48a	Atlantic Source Zone	-63.8800	18.8870	95.37	20	22.1
atsz-48b	Atlantic Source Zone	-63.8382	19.3072	95.37	20	5
atsz-48y	Atlantic Source Zone	-63.9643	18.0465	95.37	20	56.3
atsz-48z	Atlantic Source Zone	-63.9216	18.4667	95.37	20	39.2
atsz-49a	Atlantic Source Zone	-64.8153	18.9650	94.34	20	22.1
atsz-49b	Atlantic Source Zone	-64.7814	19.3859	94.34	20	5
atsz-49y	Atlantic Source Zone	-64.8840	18.1233	94.34	20	56.3
atsz-49z	Atlantic Source Zone	-64.8492	18.5442	94.34	20	39.2
atsz-50a	Atlantic Source Zone	-65.6921	18.9848	89.59	20	22.1
atsz-50b	Atlantic Source Zone	-65.6953	19.4069	89.59	20	5
atsz-50y	Atlantic Source Zone	-65.6874	18.1407	89.59	20	56.3
atsz-50z	Atlantic Source Zone	-65.6887	18.5628	89.59	20	39.2
atsz-51a	Atlantic Source Zone	-66.5742	18.9484	84.98	20	22.1
atsz-51b	Atlantic Source Zone	-66.6133	19.3688	84.98	20	5
atsz-51y	Atlantic Source Zone	-66.4977	18.1076	84.98	20	56.3
atsz-51z	Atlantic Source Zone	-66.5353	18.5280	84.98	20	39.2
atsz-52a	Atlantic Source Zone	-67.5412	18.8738	85.87	20	22.1
atsz-52b	Atlantic Source Zone	-67.5734	19.2948	85.87	20	5
atsz-52y	Atlantic Source Zone	-67.4781	18.0319	85.87	20	56.3
atsz-52z	Atlantic Source Zone	-67.5090	18.4529	85.87	20	39.2
atsz-53a	Atlantic Source Zone	-68.4547	18.7853	83.64	20	22.1
atsz-53b	Atlantic Source Zone	-68.5042	19.2048	83.64	20	5
atsz-53y	Atlantic Source Zone	-68.3575	17.9463	83.64	20	56.3
atsz-53z	Atlantic Source Zone	-68.4055	18.3658	83.64	20	39.2
atsz-54a	Atlantic Source Zone	-69.6740	18.8841	101.5	20	22.1
atsz-54b	Atlantic Source Zone	-69.5846	19.2976	101.5	20	5
atsz-55a	Atlantic Source Zone	-70.7045	19.1376	108.2	20	22.1
atsz-55b	Atlantic Source Zone	-70.5647	19.5386	108.2	20	5
atsz-56a	Atlantic Source Zone	-71.5368	19.3853	102.6	20	22.1
atsz-56b	Atlantic Source Zone	-71.4386	19.7971	102.6	20	5
atsz-57a	Atlantic Source Zone	-72.3535	19.4838	94.2	20	22.1
atsz-57b	Atlantic Source Zone	-72.3206	19.9047	94.2	20	5
atsz-58a	Atlantic Source Zone	-73.1580	19.4498	84.34	20	22.1
atsz-58b	Atlantic Source Zone	-73.2022	19.8698	84.34	20	5
atsz-59a	Atlantic Source Zone	-74.3567	20.9620	259.7	20	22.1
atsz-59b	Atlantic Source Zone	-74.2764	20.5467	259.7	20	5
atsz-60a	Atlantic Source Zone	-75.2386	20.8622	264.2	15	17.94
atsz-60b	Atlantic Source Zone	-75.1917	20.4306	264.2	15	5
atsz-61a	Atlantic Source Zone	-76.2383	20.7425	260.7	15	17.94
atsz-61b	Atlantic Source Zone	-76.1635	20.3144	260.7	15	5
atsz-62a	Atlantic Source Zone	-77.2021	20.5910	259.9	15	17.94
atsz-62b	Atlantic Source Zone	-77.1214	20.1638	259.9	15	5
atsz-63a	Atlantic Source Zone	-78.1540	20.4189	259	15	17.94
atsz-63b	Atlantic Source Zone	-78.0661	19.9930	259	15	5
atsz-64a	Atlantic Source Zone	-79.0959	20.2498	259.2	15	17.94
atsz-64b	Atlantic Source Zone	-79.0098	19.8236	259.2	15	5
atsz-65a	Atlantic Source Zone	-80.0393	20.0773	258.9	15	17.94
atsz-65b	Atlantic Source Zone	-79.9502	19.6516	258.9	15	5
atsz-66a	Atlantic Source Zone	-80.9675	19.8993	258.6	15	17.94
atsz-66b	Atlantic Source Zone	-80.8766	19.4740	258.6	15	5
atsz-67a	Atlantic Source Zone	-81.9065	19.7214	258.5	15	17.94

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**Table B.1 – continued from previous page**

Segment	Description	Longitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz-67b	Atlantic Source Zone	-81.8149	19.2962	258.5	15	5
atsz-68a	Atlantic Source Zone	-87.8003	15.2509	62.69	15	17.94
atsz-68b	Atlantic Source Zone	-88.0070	15.6364	62.69	15	5
atsz-69a	Atlantic Source Zone	-87.0824	15.5331	72.73	15	17.94
atsz-69b	Atlantic Source Zone	-87.2163	15.9474	72.73	15	5
atsz-70a	Atlantic Source Zone	-86.1622	15.8274	70.64	15	17.94
atsz-70b	Atlantic Source Zone	-86.3120	16.2367	70.64	15	5
atsz-71a	Atlantic Source Zone	-85.3117	16.1052	73.7	15	17.94
atsz-71b	Atlantic Source Zone	-85.4387	16.5216	73.7	15	5
atsz-72a	Atlantic Source Zone	-84.3470	16.3820	69.66	15	17.94
atsz-72b	Atlantic Source Zone	-84.5045	16.7888	69.66	15	5
atsz-73a	Atlantic Source Zone	-83.5657	16.6196	77.36	15	17.94
atsz-73b	Atlantic Source Zone	-83.6650	17.0429	77.36	15	5
atsz-74a	Atlantic Source Zone	-82.7104	16.7695	82.35	15	17.94
atsz-74b	Atlantic Source Zone	-82.7709	17.1995	82.35	15	5
atsz-75a	Atlantic Source Zone	-81.7297	16.9003	79.86	15	17.94
atsz-75b	Atlantic Source Zone	-81.8097	17.3274	79.86	15	5
atsz-76a	Atlantic Source Zone	-80.9196	16.9495	82.95	15	17.94
atsz-76b	Atlantic Source Zone	-80.9754	17.3801	82.95	15	5
atsz-77a	Atlantic Source Zone	-79.8086	17.2357	67.95	15	17.94
atsz-77b	Atlantic Source Zone	-79.9795	17.6378	67.95	15	5
atsz-78a	Atlantic Source Zone	-79.0245	17.5415	73.61	15	17.94
atsz-78b	Atlantic Source Zone	-79.1532	17.9577	73.61	15	5
atsz-79a	Atlantic Source Zone	-78.4122	17.5689	94.07	15	17.94
atsz-79b	Atlantic Source Zone	-78.3798	18.0017	94.07	15	5
atsz-80a	Atlantic Source Zone	-77.6403	17.4391	103.3	15	17.94
atsz-80b	Atlantic Source Zone	-77.5352	17.8613	103.3	15	5
atsz-81a	Atlantic Source Zone	-76.6376	17.2984	98.21	15	17.94
atsz-81b	Atlantic Source Zone	-76.5726	17.7278	98.21	15	5
atsz-82a	Atlantic Source Zone	-75.7299	19.0217	260.1	15	17.94
atsz-82b	Atlantic Source Zone	-75.6516	18.5942	260.1	15	5
atsz-83a	Atlantic Source Zone	-74.8351	19.2911	260.8	15	17.94
atsz-83b	Atlantic Source Zone	-74.7621	18.8628	260.8	15	5
atsz-84a	Atlantic Source Zone	-73.6639	19.2991	274.8	15	17.94
atsz-84b	Atlantic Source Zone	-73.7026	18.8668	274.8	15	5
atsz-85a	Atlantic Source Zone	-72.8198	19.2019	270.6	15	17.94
atsz-85b	Atlantic Source Zone	-72.8246	18.7681	270.6	15	5
atsz-86a	Atlantic Source Zone	-71.9143	19.1477	269.1	15	17.94
atsz-86b	Atlantic Source Zone	-71.9068	18.7139	269.1	15	5
atsz-87a	Atlantic Source Zone	-70.4738	18.8821	304.5	15	17.94
atsz-87b	Atlantic Source Zone	-70.7329	18.5245	304.5	15	5
atsz-88a	Atlantic Source Zone	-69.7710	18.3902	308.9	15	17.94
atsz-88b	Atlantic Source Zone	-70.0547	18.0504	308.4	15	5
atsz-89a	Atlantic Source Zone	-69.2635	18.2099	283.9	15	17.94
atsz-89b	Atlantic Source Zone	-69.3728	17.7887	283.9	15	5
atsz-90a	Atlantic Source Zone	-68.5059	18.1443	272.9	15	17.94
atsz-90b	Atlantic Source Zone	-68.5284	17.7110	272.9	15	5
atsz-91a	Atlantic Source Zone	-67.6428	18.1438	267.8	15	17.94
atsz-91b	Atlantic Source Zone	-67.6256	17.7103	267.8	15	5
atsz-92a	Atlantic Source Zone	-66.8261	18.2536	262	15	17.94
atsz-92b	Atlantic Source Zone	-66.7627	17.8240	262	15	5



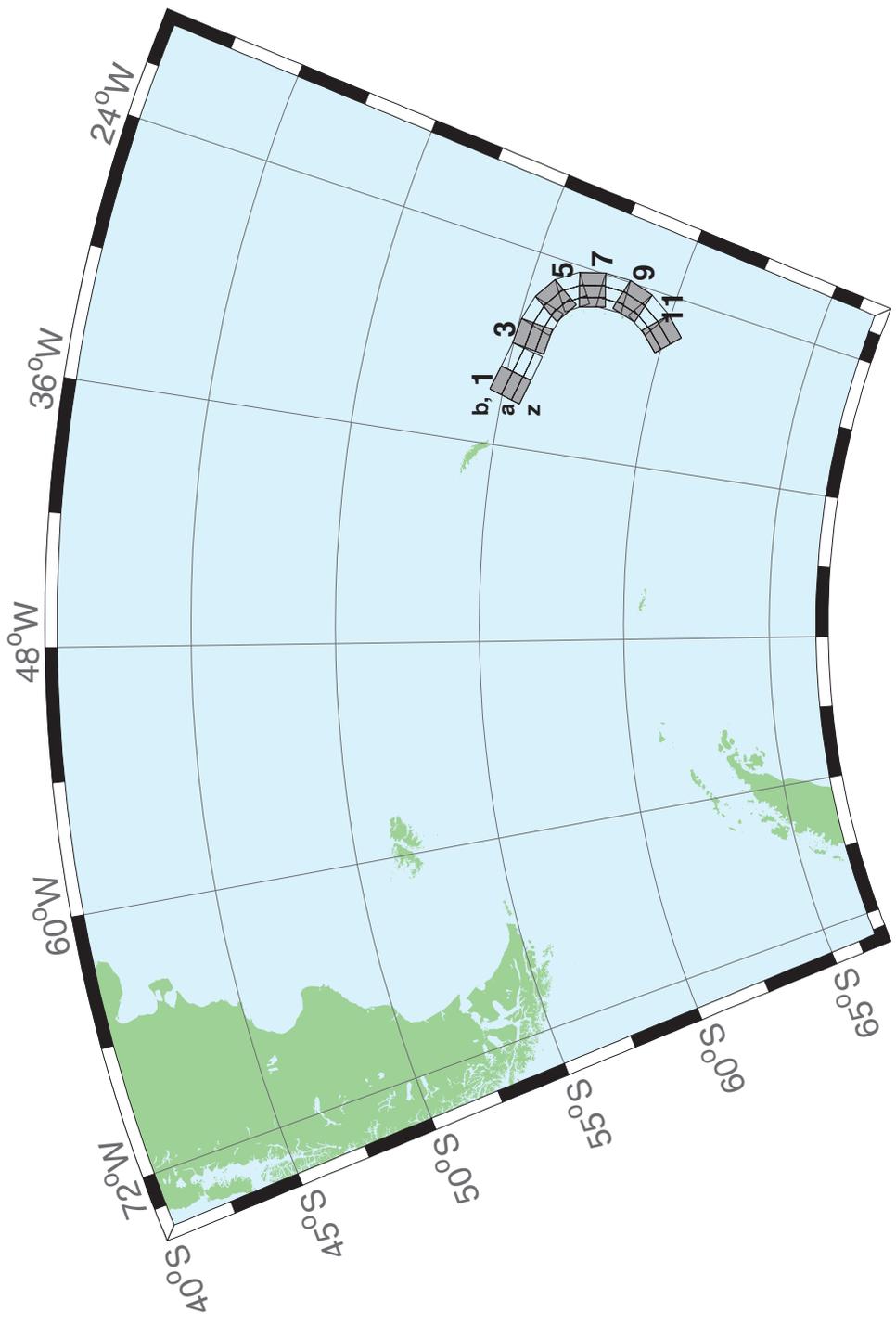


Figure B.2: South Sandwich Islands Subduction Zone.

Table B.2: Earthquake parameters for South Sandwich Islands Subduction Zone unit sources.

Segment	Description	Longitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)	
sssz-1a	South Sandwich Islands Subduction Zone	-32.3713	-55.4655	104.7	28.53	17.51	
sssz-1b	South Sandwich Islands Subduction Zone	-32.1953	-55.0832	104.7	9.957	8.866	
sssz-1z	South Sandwich Islands Subduction Zone	-32.5091	-55.7624	104.7	46.99	41.39	
sssz-2a	South Sandwich Islands Subduction Zone	-30.8028	-55.6842	102.4	28.53	17.51	
sssz-2b	South Sandwich Islands Subduction Zone	-30.6524	-55.2982	102.4	9.957	8.866	
sssz-2z	South Sandwich Islands Subduction Zone	-30.9206	-55.9839	102.4	46.99	41.39	
sssz-3a	South Sandwich Islands Subduction Zone	-29.0824	-55.8403	95.53	28.53	17.51	
sssz-3b	South Sandwich Islands Subduction Zone	-29.0149	-55.4468	95.53	9.957	8.866	
sssz-3z	South Sandwich Islands Subduction Zone	-29.1353	-56.1458	95.53	46.99	41.39	
sssz-4a	South Sandwich Islands Subduction Zone	-27.8128	-55.9796	106.1	28.53	17.51	
sssz-4b	South Sandwich Islands Subduction Zone	-27.6174	-55.5999	106.1	9.957	8.866	
sssz-4z	South Sandwich Islands Subduction Zone	-27.9659	-56.2744	106.1	46.99	41.39	
sssz-5a	South Sandwich Islands Subduction Zone	-26.7928	-56.2481	123.1	28.53	17.51	
sssz-5b	South Sandwich Islands Subduction Zone	-26.4059	-55.9170	123.1	9.957	8.866	
sssz-5z	South Sandwich Islands Subduction Zone	-27.0955	-56.5052	123.1	46.99	41.39	
sssz-6a	South Sandwich Islands Subduction Zone	-26.1317	-56.6466	145.6	23.28	16.11	
sssz-6b	South Sandwich Islands Subduction Zone	-25.5131	-56.4133	145.6	9.09	8.228	
sssz-6z	South Sandwich Islands Subduction Zone	-26.5920	-56.8194	145.6	47.15	35.87	
sssz-7a	South Sandwich Islands Subduction Zone	-25.6787	-57.2162	162.9	21.21	14.23	
sssz-7b	South Sandwich Islands Subduction Zone	-24.9394	-57.0932	162.9	7.596	7.626	
sssz-7z	South Sandwich Islands Subduction Zone	-26.2493	-57.3109	162.9	44.16	32.32	
sssz-8a	South Sandwich Islands Subduction Zone	-25.5161	-57.8712	178.2	20.33	15.91	
sssz-8b	South Sandwich Islands Subduction Zone	-24.7233	-57.8580	178.2	8.449	8.562	
sssz-8z	South Sandwich Islands Subduction Zone	-26.1280	-57.8813	178.2	43.65	33.28	
sssz-9a	South Sandwich Islands Subduction Zone	-25.6657	-58.5053	195.4	25.76	15.71	
sssz-9b	South Sandwich Islands Subduction Zone	-24.9168	-58.6127	195.4	8.254	8.537	
sssz-9z	South Sandwich Islands Subduction Zone	-26.1799	-58.4313	195.4	51.69	37.44	
sssz-10a	South Sandwich Islands Subduction Zone	-26.1563	-59.1048	212.5	32.82	15.65	
sssz-10b	South Sandwich Islands Subduction Zone	-25.5335	-59.3080	212.5	10.45	6.581	
sssz-10z	South Sandwich Islands Subduction Zone	-26.5817	-58.9653	212.5	54.77	42.75	
sssz-11a	South Sandwich Islands Subduction Zone	-27.0794	-59.6799	224.2	33.67	15.75	
sssz-11b	South Sandwich Islands Subduction Zone	-26.5460	-59.9412	224.2	11.32	5.927	
sssz-11z	South Sandwich Islands Subduction Zone	-27.4245	-59.5098	224.2	57.19	43.46	

## **Appendix C SIFT Testing Report**

## **Appendix C**

### **SIFT Testing Report**

Authors: Lindsey Wright, Liujuan Tang

#### **1.0 PURPOSE**

Forecast models are tested with synthetic tsunami events covering a range of tsunami source locations and magnitudes. Testing is also done with selected historical tsunami events when available.

The testing of a forecast model has three objectives. The first objective is to assure that the results obtained with the NOAA's tsunami forecast system software, which has been released to the Tsunami Warning Centers for operational use are consistent with those obtained by the researcher during the development of the forecast model. The second objective is to test the forecast model for consistency, accuracy, time efficiency, and quality of results over a range of possible tsunami locations and magnitudes. The third objective is to identify bugs and issues in need of resolution by the researcher who developed the Forecast Model or by the forecast system software development team before the next version release to NOAA's two Tsunami Warning Centers.

Local hardware and software applications, and tools familiar to the researcher(s), are used to run the Method of Splitting Tsunamis (MOST) model during the forecast model development. The test results presented in this report lend confidence that the model performs as developed and produces the same results when initiated within the forecast system application in an operational setting as those produced by the researcher during the forecast model development. The test results assure those who rely on the Virginia Beach tsunami forecast model that consistent results are produced irrespective of system.

## 2.0 TESTING PROCEDURE

The general procedure for forecast model testing is to run a set of synthetic tsunami scenarios and a selected set of historical tsunami events through the forecast system application and compare the results with those obtained by the researcher during the forecast model development and presented in the Tsunami Forecast Model Report. Specific steps taken to test the model include:

1. Identification of testing scenarios, including the standard set of synthetic events, appropriate historical events, and customized synthetic scenarios that may have been used by the researcher(s) in developing the forecast model.
2. Creation of new events to represent customized synthetic scenarios used by the researcher(s) in developing the forecast model, if any.
3. Submission of test model runs with the forecast system, and export of the results from A, B, and C grids, along with time series.
4. Recording applicable metadata, including the specific forecast system version used for testing.
5. Examination of forecast model results for instabilities in both time series and plot results.
6. Comparison of forecast model results obtained through the forecast system with those obtained during the forecast model development.
7. Summarization of results with specific mention of quality, consistency, and time efficiency.
8. Reporting of issues identified to modeler and forecast system software development team.
9. Retesting the forecast models in the forecast system when reported issues have been addressed or explained.

Synthetic model runs were tested on a DELL PowerEdge R510 computer equipped with two Xeon E5670 processors at 2.93 Ghz, each with 12 MBytes of cache and 32GB memory. The processors are hex core and support hyperthreading, resulting in the computer performing as a 24 processor core machine. Additionally, the testing computer supports 10 Gigabit Ethernet for fast network connections. This computer configuration is similar or the same as the configurations of the

computers installed at the Tsunami Warning Centers so the compute times should only vary slightly.

## Results

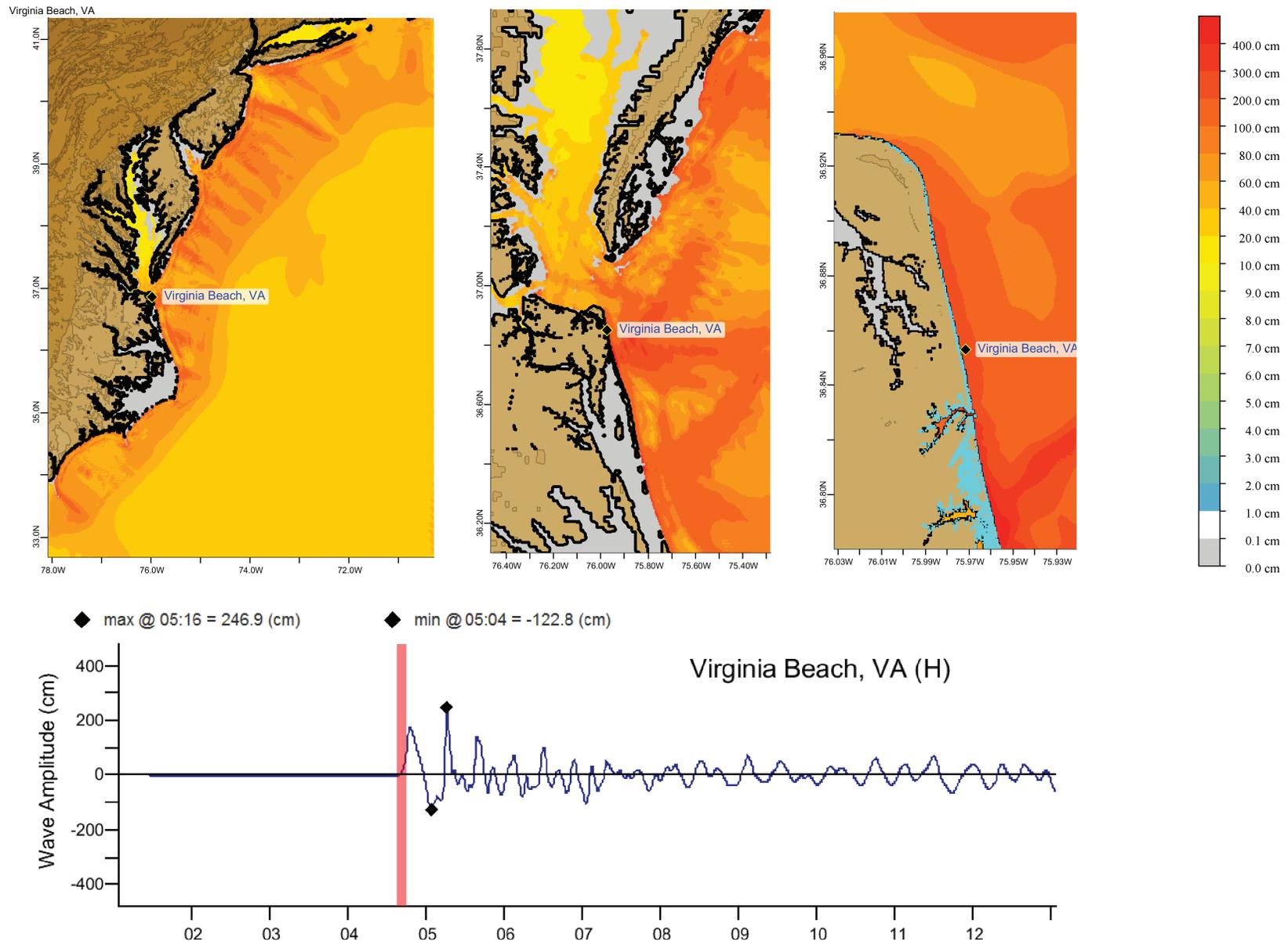
The Virginia Beach forecast model was tested with SIFT version 3.2. The same version of propagation database was used during the model development.

The Virginia Beach, Virginia forecast model was tested with three synthetic scenarios. Test results from the forecast system and comparisons with the results obtained during the forecast model development are shown numerically in Table C1 and graphically in Figures C1 to C3. The results show that the minimum and maximum amplitudes and time series obtained from the forecast system agree with those obtained during the forecast model development, and that the forecast model is stable and robust, with consistent and high quality results across geographically distributed tsunami sources. The model run time (wall clock time) was 24.75 minutes for 11.99 hours of simulation time, and 8.24 minutes for 4.0 hours. This run time is well within the 10 minute run time for 4 hours of simulation time.

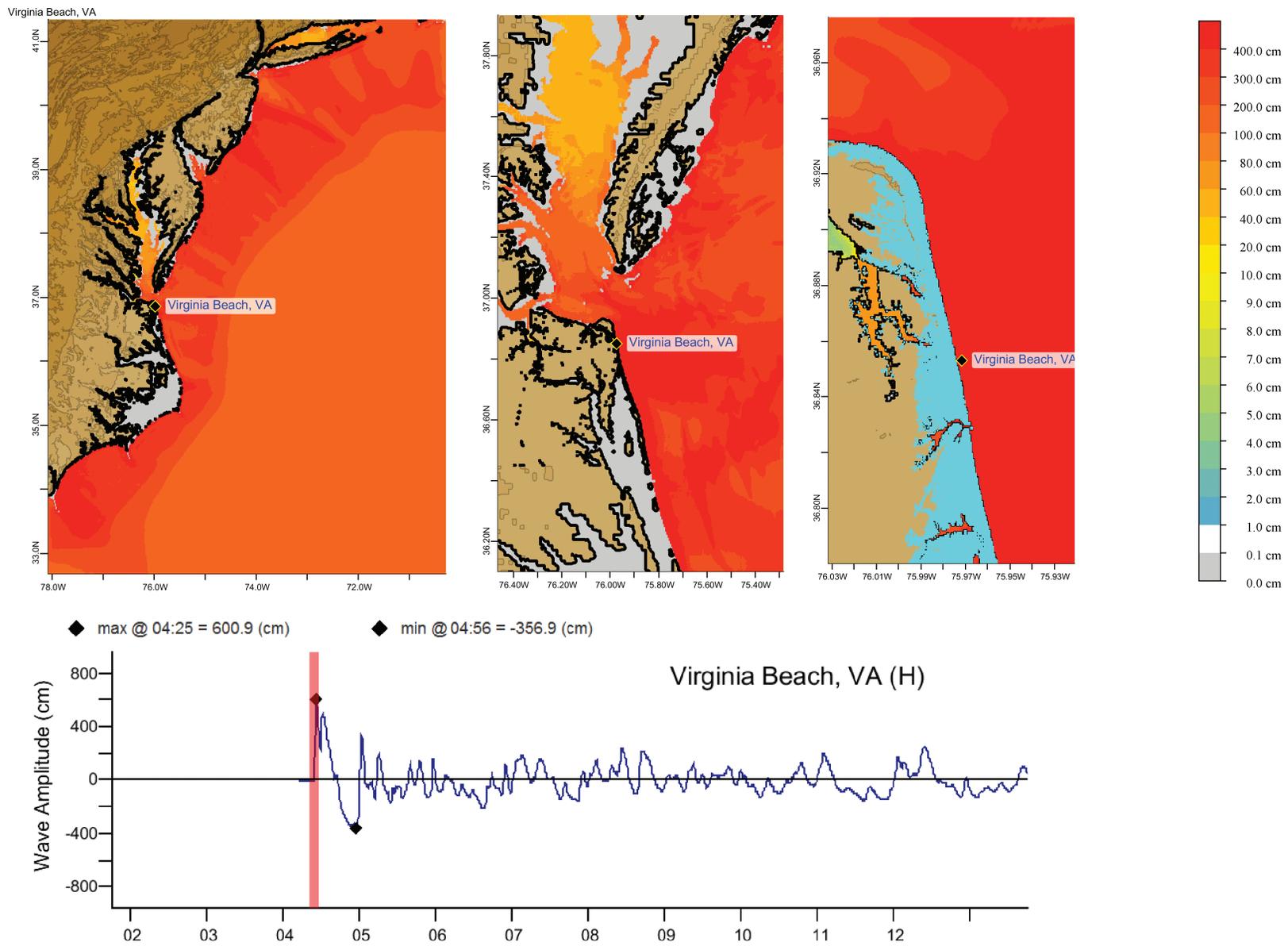
A suite of three synthetic events was run on the Virginia Beach forecast model. The modeled scenarios were stable for all cases run. The largest modeled height was 601 centimeters (cm) from the Atlantic (ATSZ 48–57) source zone. The smallest signal of 40 cm was recorded at the South Sandwich (SSSZ 1–10) source zone. Maximum values for the SSSZ 1–10 differed slightly. This abnormality resulted from the development model being run for a longer window of time than the SIFT output and therefore an additional wave with a slightly higher amplitude was recorded at approximately 28 hours after the event. Visual comparisons between the development cases and the forecast system output were nearly identical in shape and amplitude for all cases. The Virginia Beach reference point used for the forecast model development is the same as what is deployed in the forecast system, so the results can be considered valid for the three cases studied.

**Table C1.** Table of maximum and minimum amplitudes (cm) at the Virginia Beach, Virginia warning point for synthetic and historical events tested using SIFT 3.2 and obtained during development.

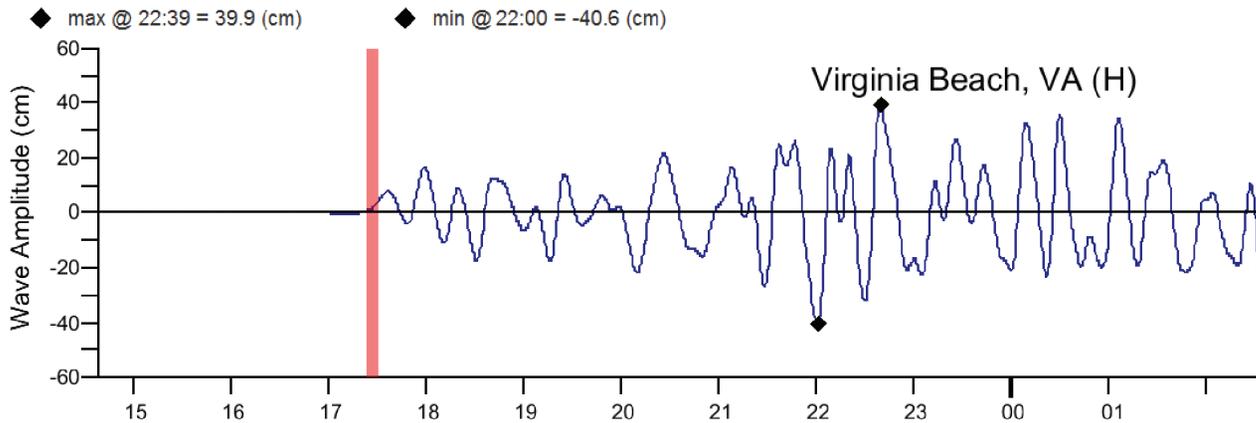
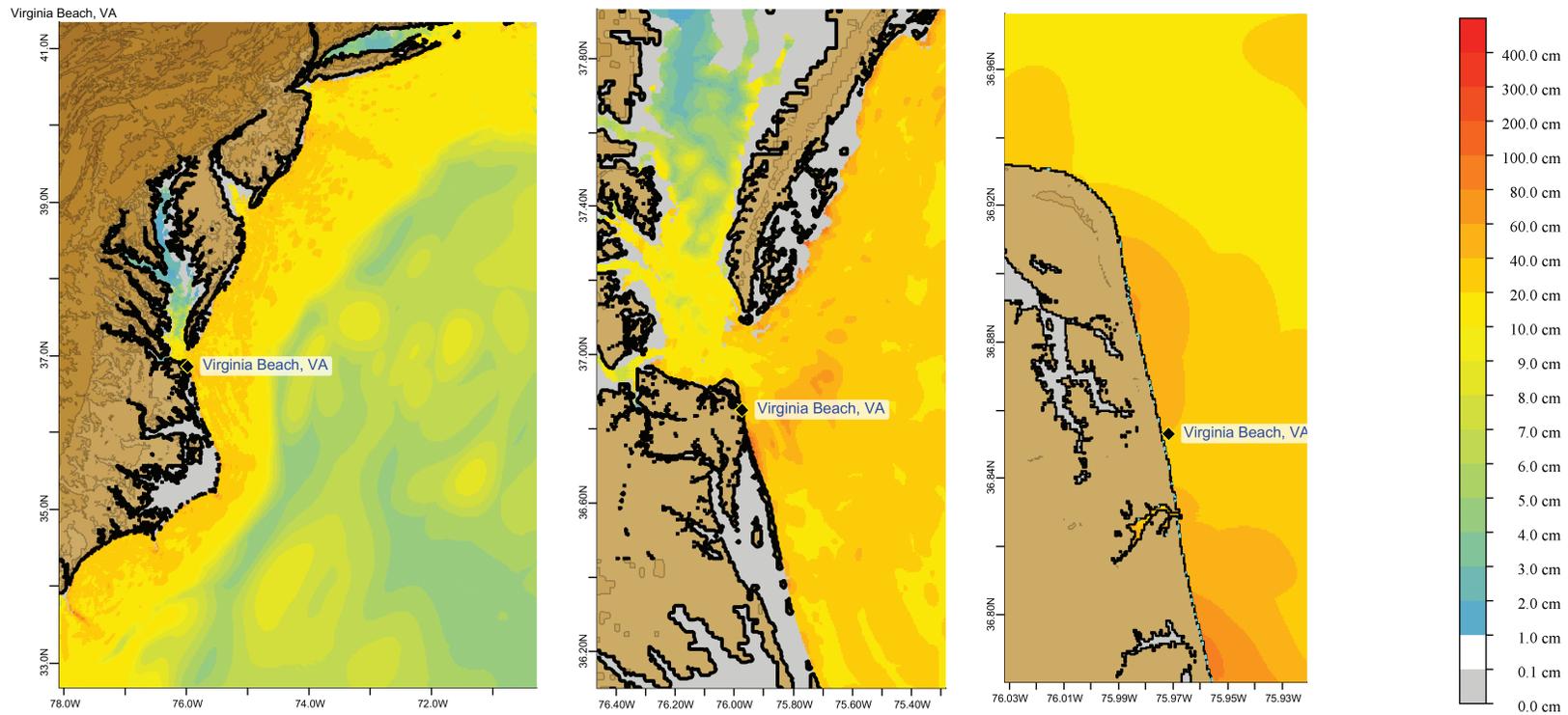
Scenario Name	Source Zone	Tsunami Source	$\alpha$ [m]	SIFT Max (cm)	Development Max (cm)	SIFT Min (cm)	Development Min (cm)
<b>Mega-tsunami Scenarios</b>							
ATSZ 38-47	Atlantic	A38-A47, B38-B47	25	246.9	247	-122.8	-123
ATSZ 48-57	Atlantic	A48-A57, B48-B57	25	600.9	601	-356.9	-358
SSSZ 1-10	South Sandwich	A1-A10, B1-B10	25	39.9	58(40 for first 12 hours)	-40.6	-43



**Figure C1** Response of the Virginia Beach forecast model to synthetic scenario ATSZ 38-47. (a, b, and c) Maximum sea surface elevation for A-, B- and C-grids. (d) Sea surface elevation time series at the C-grid warning point.



**Figure C2** Response of the Virginia Beach forecast model to synthetic scenario ATSZ 48-57. (a, b, and c) Maximum sea surface elevation for A-, B- and C-grids. (d) Sea surface elevation time series at the C-grid warning point.



**Figure C3** Response of the Virginia Beach forecast model to synthetic scenario SSSZ 1-10. (a, b, and c) Maximum sea surface elevation for A-, B- and C-grids. (d) Sea surface elevation time series at the C-grid warning point.